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Age-related changes in mouse bone permeability

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1 **ABSTRACT**

2 The determination of lacunar-canalicular permeability is essential for understanding local
3 fluid flow in bone, which may indicate how bone senses changes in the mechanical
4 environment to regulate mechano-adaptation. The estimates of lacunar-canalicular
5 permeability found in the literature vary by up to eight orders of magnitude, and age-related
6 permeability changes have not been measured in non-osteonal mouse bone. The objective of
7 this study is to use a poroelastic approach based on nanoindentation data to characterize
8 lacunar-canalicular permeability in murine bone as a function of age. Nine wild type
9 C57BL/6 mice of different ages (2, 7 and 12 months) were used. Three tibiae from each age
10 group were embedded in epoxy resin, cut in half and indented in the longitudinal direction in
11 the mid-cortex using two spherical fluid indenter tips ($R = 238 \mu\text{m}$ and $500 \mu\text{m}$). Results
12 suggest that the lacunar-canalicular intrinsic permeability of mouse bone decreases from 2 to
13 7 months, with no significant changes from 7 to 12 months. The large indenter tip imposed
14 larger contact sizes and sampled larger ranges of permeabilities, particularly for the old bone.
15 This age-related difference in the distribution was not seen for indents with the smaller radius
16 tip. We conclude that the small tip effectively measured lacunar-canalicular permeability,
17 while larger tip indents were influenced by vascular permeability. Exploring the age-related
18 changes in permeability of bone measured by nanoindentation will lead to a better
19 understanding of the role of fluid flow in mechano-transduction. This understanding may
20 help indicate alterations in bone adaptation and remodelling.

21

22 1. INTRODUCTION

23 It is well known that bone continuously adapts to its mechanical environment. Previous
24 studies have established that this adaptive response is most likely coordinated by osteocytes,
25 the mechanosensor cells in bone (Burger et al. 1999, Cowin et al. 1995, Han et al. 2004).
26 Osteocyte bodies lie in spaces called lacunae in the mineralized bone matrix and they are
27 connected through small channels termed canaliculi. The mechanical stimulus that drives
28 osteocytes to respond has not been established yet but evidence suggests that fluid flow might
29 perform a major role in cellular excitation. The primary loading-induced fluid motion appears
30 to be through the lacunar-canalicular network, where osteocyte cells sense shear stress due to
31 interstitial fluid movement (Anderson and Knothe Tate 2008, Fritton and Weinbaum 2009,
32 Gardinier et al. 2010, Jacobs et al. 2010, Knothe-Tate 2003). Characterizing lacunar-
33 canalicular network permeability is vital to understand the role of fluid flow in the mechano-
34 transduction mechanism of bone (Anderson et al. 2008, Burger et al. 1999, Lemaire et al.
35 2012, Price et al. 2011).

36 Experimentally measuring lacunar-canalicular permeability is challenging due to the
37 heterogeneity of bone and small size of the pores, which is why the first calculations were
38 mainly theoretical. Theoretical estimates based on Biot's poroelasticity theory have given
39 values ranging from 10^{-22} to 10^{-19} m^2 (Gururaja et al. 2005, Wang et al. 1999, Zhou et al.
40 2008). Finite element models predicted values of 10^{-22} to 10^{-18} m^2 (Lemaire et al. 2012, Smit
41 et al. 2002). Beno et al. (2006) reported values of 10^{-23} - 10^{-19} m^2 with microstructural models
42 of lacunar-canalicular porosity based on geometric data. Stress-relaxation measurements of
43 single osteons measured 10^{-25} - 10^{-24} m^2 (Gailani et al. 2009) and compaction of bone gave
44 values of 10^{-23} m^2 (Gardinier et al. 2010). Nanoindentation studies measured values between
45 10^{-24} to 10^{-21} m^2 for the lacunar-canalicular permeability of equine cortical bone (Galli and
46 Oyen 2009, Oyen 2008, Oyen et al. 2012). Overall, these estimations of lacunar-canalicular

47 permeability range from 10^{-25} to 10^{-18} m². This wide range is mainly a result of the fact that
48 vascular and lacunar-canalicular network are interconnected (Fig. 1), making it difficult to
49 separate the contribution of each one to the permeability of bone (Benalla et al. 2012, Jast and
50 Jasiuk 2013, Knothe Tate et al. 2009). In order to isolate effects of lacunar-canalicular
51 permeability independent of vascular permeability, we used nanoindentation.
52 Nanoindentation is a non-destructive way to measure tissue properties of bone and it has
53 recently been used to measure the permeability of hydrated biological tissues (Galli and Oyen
54 2009, Oyen 2008, Oyen et al. 2012). Oyen et al. (2012) found that the values of bone
55 permeability are dependent on the indentation contact size and reported nanoindentation-
56 measured permeability values approximately three orders of magnitude smaller than those
57 given by microindentation. Results from porosity studies also suggest that the probability of
58 measuring specific porosity-ranges in a sample is affected by the inherent structure or density
59 of the interconnected porous network (Jast and Jasiuk 2013, Knothe Tate et al. 2009).
60 Overall, these findings suggest that different indentation contact sizes might measure
61 different hierarchies of bone permeability. In order to investigate this further, spherical
62 indenters of two different radii were used in the current study.

63 The objective of this research was to characterize lacunar-canalicular permeability in young
64 and aged B6 murine bone using a poroelastic approach based on nanoindentation data.
65 Despite the differences between murine and human bone, C57BL/6J (B6) mice are often
66 utilized to explore aspects of age-related bone loss in humans (Halloran et al. 2002, Jilka
67 2013). Unlike human bone, murine bone does not have osteons or Haversian systems, which
68 is why values of porosity and permeability of human or other animal bone cannot directly be
69 transferred to murine bone. Analyzing age-related changes in mouse bone permeability will
70 provide a better insight into the complex nature of bone permeability and its influence in
71 mechanotransduction.

72 **2. METHODS**

73 *Sample preparation*

74 Nine C57BL/6 (B6) female mice of 2, 7 and 12 months, which correspond to young,
75 skeletally mature and old mice respectively, were used for this study. Three right tibiae from
76 each age-group were cleaned of surrounding soft tissue, dried in air for an hour and
77 embedded in epoxy resin (EPOTHIN; Buehler, Lake Bluff, IL, USA). The resin and hardener
78 were mixed and let cool for 15 minutes to increase the viscosity and avoid the infiltration of
79 the resin into the pores. Tibiae were cut at the mid-diaphysis using a low speed diamond saw
80 (Isomet, Buehler GmbH, Germany). The distal sections were cut in cubes and polished using
81 increasing grades of carbide papers (from P800 to P4000).

82 *Nanoindentation*

83 Figure 2 shows the outline of the experimental setup for nanoindentation. Tests were carried
84 out using a TI700 UBI (Hysitron, MN, USA) nanoindenter in load control. The distal halves
85 of the tibiae were glued to a metallic container that covered the stage and indents were done
86 in the longitudinal direction on the tibia mid-diaphyseal cross-sections. Tests were conducted
87 after submerging the specimens in distilled water for at least 15 minutes to fill the pores with
88 fluid. Spherical fluid cell indenter tips of two sizes were used: radius of 238 μm and 500 μm .
89 A trapezoidal loading profile was applied with a rising time of 10 s to a maximum load of 6
90 mN and a holding time of 30 s. A minimum of ten indents were made on each sample in the
91 mid-cortex around the circumference of the bone. The indents that fell in pores were
92 excluded.

93 Experimental data from all tests was exported as load-displacement-time (P-h-t) for analysis
94 in MATLAB (The MathWorks, Natick, MA, USA).

95 3. ANALYSIS

96 *Poroelastic Analysis*

97 The poroelastic analysis proposed by Oyen (2008) and further developed by Galli and Oyen
98 (2009) examines spherical indentation creep responses of hydrated biological materials.
99 During the indentation, the spherical indenter is brought into contact with the surface, pushed
100 into the fully saturated material and retracted, while the applied load, resulting displacement
101 and time are recorded. The rapid local deformation from the indenter causes fluid to be forced
102 out of the material, resulting in pore pressure, which supports part of the applied load. As the
103 fluid leaves the material, pore pressure decreases, resulting in a time-dependent deformation
104 response, which is measured by the nanoindenter. The poroelastic framework assumes that
105 the material has linear isotropic poroelastic behaviour and is fully saturated. Five parameters
106 are required to characterize a poroelastic response: the shear modulus G [N/m²]; the drained
107 Poisson's ratio ν ; the undrained Poisson's ratio ν_u [ν , 0.5]; the Biot effective stress coefficient
108 α [0, 1]; and the Darcy hydraulic permeability κ [m⁴/Ns]. The elastic properties (G and ν)
109 correspond to the porous medium considered as a homogeneous linear elastic material. The
110 undrained and drained cases of a fluid-infiltrated porous material represent its limiting
111 behaviors. The undrained response characterizes the condition where the fluid is trapped in
112 the porous solid; while the drained response is related to zero pore pressure (or the pressure
113 corresponding to empty pores).

114 For an ideal isotropic poroelastic material, the Biot effective stress coefficient α is defined as:

$$\alpha = 1 - \frac{K}{K_s} \quad [1]$$

115 where K [N/m²] is the bulk modulus of the drained material (bone with pores) and K_s [N/m²]
116 refers to the bulk modulus of the material of the solid skeleton (bone material). The stress

117 coefficient represents the variation of the fluid volume in a material unit volume due to the
118 volumetric change of the element when loaded under the drained condition.

119 Darcy hydraulic permeability κ characterizes the flow through the porous elastic skeleton. It
120 is defined as the ratio of the intrinsic permeability k [m^2] to the fluid dynamic viscosity μ (for
121 water $\mu = 0.001$ Pa-s is assumed):

$$\kappa = k/\mu \quad [2]$$

122 The intrinsic permeability k is related to the porous bone structure only (the connectedness of
123 the porosity and the size and spatial arrangement of the pores), not the fluid in the pores. This
124 is the parameter that will be reported in the current study.

125 Galli and Oyen (2009) proposed and validated an algorithm to identify these constitutive
126 parameters using a master curve library. The master curves were obtained solving the
127 poroelastic indentation problem utilizing Finite Element modeling for several materials and
128 normalizing their time-displacement indentation response. The non-dimensional displacement
129 h^* is defined as:

$$h^* = \frac{h(t) - h_0(t)}{h_\infty(t) - h_0(t)} \quad [3]$$

130 where $h(t)$ is the time-dependent displacement of the indenter, h_0 is the indentation depth that
131 corresponds to step-loading conditions, and h_∞ is the indentation depth at $t = \infty$ when the
132 pore pressure field vanishes. These two values can be computed from the elastic solutions
133 (Oyen et al. 2011):

$$h_0(t) = \left(\frac{3P(t)(1 - \nu_u)}{8GR^{1/2}} \right)^{2/3} \quad [4]$$

$$h_{\infty}(t) = \left(\frac{3P(t)(1-\nu)}{8GR^{1/2}} \right)^{2/3} \quad [5]$$

134 where $P(t)$ represents the indentation load and R is the indenter tip radius. The normalized
 135 time t^* is given by:

$$t^* = \sqrt{\frac{ct}{Rh(t)}} \quad [6]$$

136 $\sqrt{Rh(t)}$ represents the contact radius of the indentation. The diffusivity coefficient c is a
 137 function of the five constitutive parameters:

$$c = \frac{2\kappa G(1-\nu)(\nu_u - \nu)}{\alpha^2(1-2\nu)^2(1-\nu_u)} \quad [7]$$

138 Only three constitutive parameters can be identified from spherical indentation data. G , ν , and
 139 κ were considered unknown, while the values for α and ν_u were set to 1 (Oyen 2008) and 0.5
 140 (Galli and Oyen 2009, Oyen et al. 2012) respectively. The indenter tip was considered to be
 141 impermeable. The percentage of loading ramp analyzed ranged between 1-4%. The
 142 poroelastic analysis framework consisted of two optimization steps (Gali and Oyen 2009).
 143 The first one occurred in the normalized domain (h^*-t^*), where based on initial guesses, the
 144 normalized curves were fitted to the master curves in the database. By normalizing the
 145 response (eq. 3, 6), the noise of the experimental data can have a greater influence. Hence,
 146 the second optimization routine was used to verify that the non-dimensional solution (x^*)
 147 gave also the best fit in the dimensional domain. The second routine used the solution from
 148 the normalized domain (x^*) as initial guess to fit the curves in the time-displacement domain
 149 ($h-t$) and compute a new dimensional solution (x^d). Both curve fittings were carried out
 150 following the non-linear least-squares optimization routine from MATLAB Optimization
 151 Toolbox™ as described by Galli and Oyen (2009). Convergence was achieved when the

152 difference between the parameters identified in each domain was negligible ($x^* \sim x^d$). The final
153 solution (x) contained the values of G , ν , and κ .

154 *Statistical Analysis*

155 The number of indents per age group ranged between 30 and 55 and therefore, unequal
156 sample sizes had to be considered for statistical analysis. Hochberger's GT2 test (post-hoc
157 test) was utilized to compare the means between the three age groups when Levene's test
158 proved homogeneity of variances. If the variances were inhomogeneous, Games-Howell test
159 was used. In order to compare the means of the same bones when indenting with different
160 tips, the Wilcoxon signed-rank test was used. The significant level assumed was 0.05.
161 Statistical analysis was performed using SPSS (v.21, SPSS Inc., Chicago, IL).

162 **4. RESULTS**

163 *Elastic properties*

164 The average values and standard deviations of the elastic properties are summarized in Fig. 3.
165 The shear modulus increased significantly from 2 to 7 months for both indenter tips ($p <$
166 0.001) and then decreased again ($p < 0.001$) in the oldest bones. The $238 \mu\text{m}$ radius tip
167 measured larger shear modulus for the three ages, but this was significant only for the 7
168 month-old bones ($p = 0.002$). No statistical difference was found in Poisson's ratios between
169 the age groups when indenting the bone with the largest tip. The $238 \mu\text{m}$ measured smaller
170 Poisson's ratio values for the youngest bones compared to the 7 and 12 months ($p < 0.001$).
171 There were no significant differences between the two tip sizes.

172 *Permeability*

173 Measurements with the small tip revealed that the youngest bones had a larger permeability
174 value ($p < 0.01$) than the older ones but no statistical difference was found between the 7 and

175 12 month-old bones (Fig. 4). The permeability distribution captured with the two tips is
176 shown in Fig. 5. For the larger radius indents young bones had a narrower range of
177 permeability values (10^{-24} to 5×10^{-23} m²) while old bones exhibited a broader range (5×10^{-25}
178 to 10^{-21} m²). An example of the wide range of permeability values captured with the larger tip
179 can be observed in Fig. 6, where displacement-time (h-t) curves of two indents on the same
180 12 month-old bone result in permeability values that vary three orders of magnitude. This
181 difference in distribution of permeability values was not seen for indents with the smaller tip.

182 5. DISCUSSION

183 We used nanoindentation to determine the poroelastic properties of wild type murine tibia as
184 a function of age. The indentations with the small tip revealed a decrease in the lacunar-
185 canalicular permeability from young to skeletally matured tibiae. The 500 μ m tip imposed
186 larger contact sizes, which captured both lacunar-canalicular and vascular permeability of
187 bone.

188 The 238 μ m tip showed that lacunar-canalicular permeability decreased from 2 to 7 months
189 with no significant changes from 7 to 12 months (Fig. 4). In vivo tracer transport experiments
190 through the lacunar-canalicular network of rat bone showed that transport becomes more
191 restricted in aged bone due to a more compact mineralized tissue (Knothe Tate et al. 1998). In
192 human cortical bone, porosity of lacunae decreases slightly in older (Wang and Ni, 2003).
193 These findings on osteonal bone seem to follow the same trend of a decrease of lacunar-
194 canalicular permeability with age.

195 The permeability values we measured (5×10^{-25} to 10^{-21} m²) are within the range of previous
196 measurements using other experimental methods. Curve fitting of stress-relaxation of single
197 osteons gave lacunar-cannalicular permeability values of 10^{-25} - 10^{-24} m² for bovine femoral
198 bone (Gailani et al. 2009). This technique cannot be directly employed in murine bone, which

199 does not have osteons. Compaction of intact bone by Gardinier et al. (2010) measured values
200 of 10^{-23} m^2 for lacunar-canalicular permeability of canine metacarpal in situ. Oyen (2008)
201 measured permeability of equine bone using spherical nanoindentation assuming
202 incompressible constituents ($\alpha = 1$ and $\nu_u = 0.5$) and found values of 10^{-24} m^2 . In further
203 analysis on different equine bone specimens and using the master curve library together with
204 the poroelastic framework, nanoindentation experiments measured permeability values of 10^{-21} -
205 10^{-23} m^2 (Galli and Oyen 2009, Oyen et al. 2012). In our study, the majority of indents (60-
206 80%) indicated permeability values between 10^{-24} and $5 \times 10^{-24} \text{ m}^2$ for both tips for the three
207 ages evaluated.

208 Though our permeability values are within the range of other studies, quantitative values
209 depend on the testing and analysis methods. The epoxy-embedded bones were dry and then
210 rehydrated before testing, which may have caused changes to the cellular structures inside the
211 lacunae. Anderson et al. (2008) found that permeability decreased at two orders of magnitude
212 when the cellular structure was taken into account in a computational model. This model did
213 not include the effects of lipids and collagen matrix, which decreases permeability a further
214 three orders of magnitude (Wen et al. 2010). Nevertheless, all the samples in the current
215 study underwent the same preparation and testing protocol, and therefore, the effects of
216 freshness are assumed to have affected all the bones in the same manner. The assumptions
217 made in the analysis also influences the values obtained. In our poroelastic approach the
218 values of ν_u and α were assigned a priori. The undrained bone was considered incompressible
219 ($\nu_u = 0.5$), which does not influence the permeability value significantly when compared to ν_u
220 < 0.5 (Oyen et al. 2012). The value of $\alpha = 1$ does not influence the elastic properties but since
221 the algorithm identifies k/α^2 from the diffusivity coefficient (eq. 7) the assumed value affects
222 the quantitative value of permeability. Theoretical studies have estimated values of 0.14
223 (Cowin 1999) and 0.15 (Smit et al. 2002) for α in osteonal bone and it has been shown that its

224 value increases with increasing microporosity or decreasing mineral content (Hellmich and
225 Ulm 2005). The value $\alpha = 1$ was chosen in this study because there are no estimates of what it
226 should be for non-osteonal bone, nor how it changes with age. If $\alpha \neq 1$ was used, all the
227 reported permeability values would differ by a constant value α^2 , and thus the age-related
228 trends would not be altered. Overall, the measured values give a first experimental estimate
229 of the lacunar-canalicular permeability of non-osteonal bone.

230 In order to investigate the influence of the contact size in the measured permeability level,
231 indents made with the 238 μm and 500 μm radius tip were compared. The larger tip imposed
232 larger contact sizes and revealed a wider distribution for the 7 and 12 month-old bones,
233 reaching permeability values as large as $9 \times 10^{-22} \text{ m}^2$ (Fig. 5). These large values were not
234 captured when indenting old bone with the small tip. This difference can be explained by
235 looking at the lacunar and vascular pores of cortical bone (Fig. 7). The indentation contact
236 radius is defined as $a = \sqrt{Rh(t)}$; therefore for an average displacement of $\sim 250 \text{ nm}$ the
237 imposed contact diameter was $\sim 15 \mu\text{m}$ for the small tip and $\sim 22 \mu\text{m}$ for the larger tip. The
238 long radius of elliptical lacunae in murine bone measures 1-10 μm with a spacing of $\sim 30 \mu\text{m}$
239 between lacunae; while the diameter of vascular canals is $>10 \mu\text{m}$ with a vascular spacing of
240 $\sim 100 \mu\text{m}$ (Carriero et al. 2011, Wang et al. 2005, Schneider et al. 2007, Schneider et al. 2010,
241 Voide et al. 2011). Fig. 7 shows a nano-CT image of a 12 month-old tibia where the long
242 radius of a lacuna is 7.0 μm and the diameter of a vascular canal is 14.2 μm . This suggests
243 that with a larger contact area there is a higher likelihood of indenting a hole or part of a hole.
244 When the indent fell into a pore, the time-displacement curve was either distorted or the
245 displacement limit was exceeded before making contact with the surface. In both cases, this
246 data was excluded from the analysis.

247 In the current study, the 500 μm tip was able to identify both lacunar-canalicular and vascular
248 permeability, showing a continuum distribution of permeability over three orders of
249 magnitude. These differences in permeability are in accordance with the multi-scale
250 permeability response of equine bone obtained with varying contact sizes: when the contact
251 diameter increased from 6-14 μm to 18 μm , permeability increased almost two orders of
252 magnitude; and it increased three orders of magnitude further when the contact radius
253 reached 200-300 μm (Oyen et al. 2012). In these studies, nanoindentation measured different
254 levels of permeability in a discrete manner; the transition across length scales was not
255 explored further. In the current study, the indents with the 500 μm tip captured this transition
256 and revealed that the permeability distribution was narrower in the youngest bones. This may
257 be a result of the increasing intracortical and cortical porosity with advancing age found in
258 B6 mice femora (Ferguson et al. 2003, Courtland et al. 2013), similar to the increased size of
259 vascular Haversian canals seen in human bone (Wang and Ni 2003).

260 The elastic properties derived from the poroelastic analysis did not show such dependence on
261 the indentation contact size and their values were in agreement with published data. Shear
262 modulus increased from young to skeletally mature (2 to 7 months) bone and then decreased
263 in aged mice (12 months). Previous nanoindentation tests on hydrated bone have reported
264 shear moduli of 430-500 MPa (Bembey et al. 2006, Oyen 2008, Oyen et. al 2012). Some
265 studies have measured larger values of shear modulus in dry bone (Bushby et al. 2004, Chang
266 et al. 2011, Lopez-Franco et al. 2011); however, it has been shown that the shear modulus
267 measured by nanoindentation decreases almost an order of magnitude when spherical
268 indentation is used on hydrated bone, in contrast to sharp indentation in dry bone (Rodriguez-
269 Florez et al. 2013). Previous studies have also shown similar age-related changes in elastic
270 properties of B6 murine bone with different measurement techniques at the whole-bone
271 (Brodt et al. 1999, Ferguson et al. 2003, Sommerville et al. 2004) and tissue (Raghavan et al.

272 2012) level. The drained Poisson's ratios measured in this study are similar to the values
273 obtained by Oyen et al. (2012) and close to the $\nu = 0.3$ often assumed for bone.

274 This study provides an insight into the changes of lacunar-canalicular permeability of bone
275 with age, as well as a first experimental approximation of lacunar-canalicular permeability of
276 mouse bone. Our results suggest that nanoindentation with varying contact sizes might
277 provide the tool to understand the dual-porosity nature of bone. Recent poroelastic finite-
278 elements models of mouse cortical bone mechanotransduction have shown that the load-
279 repetition response is highly influenced by the assumed value for lacunar-canalicular
280 permeability (Pereira and Shefelbine 2013). The frequency of the load-repetition influences
281 the adaptation of the bone (Kumar et al. 2012, Robling et al. 2002, Warden and Turner 2004).
282 Therefore, it is essential to include accurate experimental lacunar-canalicular permeability
283 values into computational models to explore the influence of fluid flow in bone remodeling
284 and adaptation. Because fluid flow is likely involved in mechanotransduction of the bone's
285 mechanics environment into a cellular mechano-adaptive response, characterizing the
286 permeability of bone may help indicate alterations in mechanoadaptation.

287 **CONFLICT OF INTEREST**

288 None.

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CAPTIONS

Figure 1: Multi-scale porosity of cortical bone of a murine tibia from vascular (red big channels) to lacunar-canalicular (yellow dots and small channels) porosity.

Figure 2: Outline of the experimental setup for nanoindentation. The distal halves of the tibiae of three B6 mice of 2, 7 and 12 months were embedded in epoxy resin and tested submerged in distilled water. A minimum of ten indents were made on each sample.

Figure 3: Average and standard deviations of shear modulus (left) and Poisson's ratio (right) of B6 tibiae of 2, 7 and 12 months ($p < 0.05$).

Figure 4: Intrinsic permeability as a function of age when indenting bone with a 238 μm radius tip ($p < 0.05$).

Figure 5: Intrinsic permeability distribution as a function of age (2, 7 and 12 months) when indenting bone with a 238 μm (left) and 500 μm (right) radius tip ($p < 0.05$).

Figure 6: Displacement-time (h-t) curves corresponding to two indentations on the same 12 month-old bone using the 500 μm sphere tip. Fitting the high-displacement curves result in permeability values in the order of 10^{-21} m^2 , while low-displacement curves give values in the order of 10^{-24} m^2 .

Figure 7: Nano-CT image of a 12 month-old tibia at a resolution of 0.6 $\mu\text{m}/\text{pixel}$. Pores of varying sizes relative to the indenter size are shown. The shaded areas correspond to the contact areas imposed by the indenter. The 238 μm tip imposed contact radii a $\sim 7 \mu\text{m}$, whereas the 500 μm tip imposed contact radii a $\sim 11 \mu\text{m}$.

Figure1
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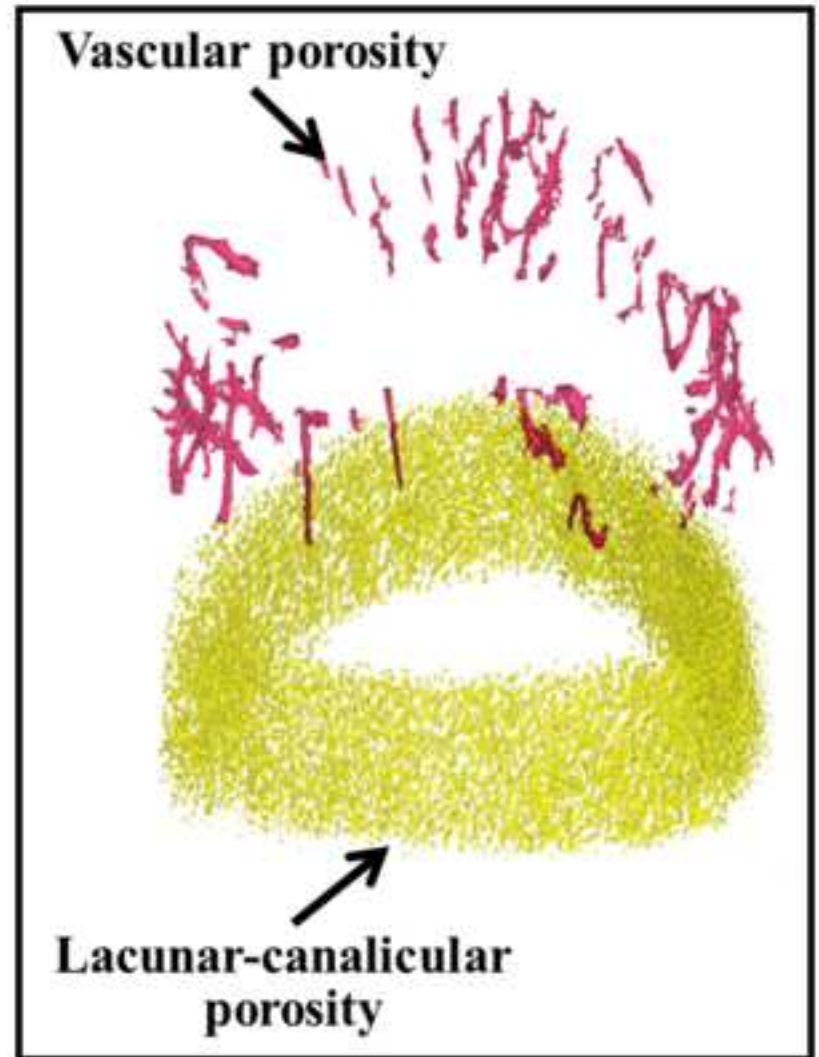
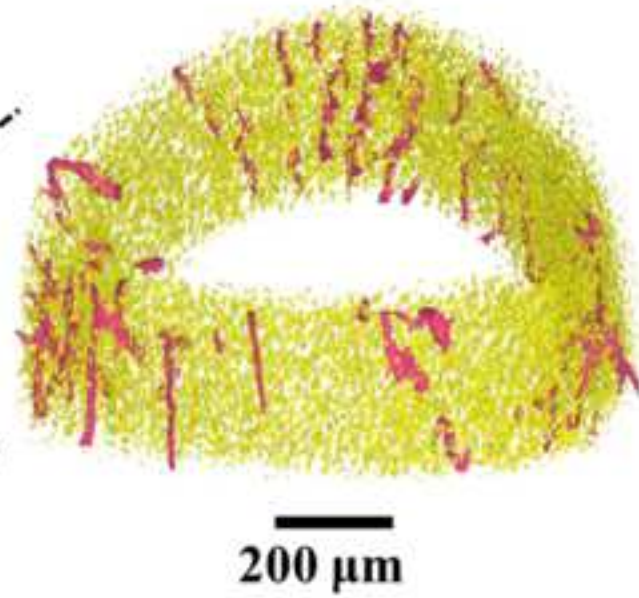
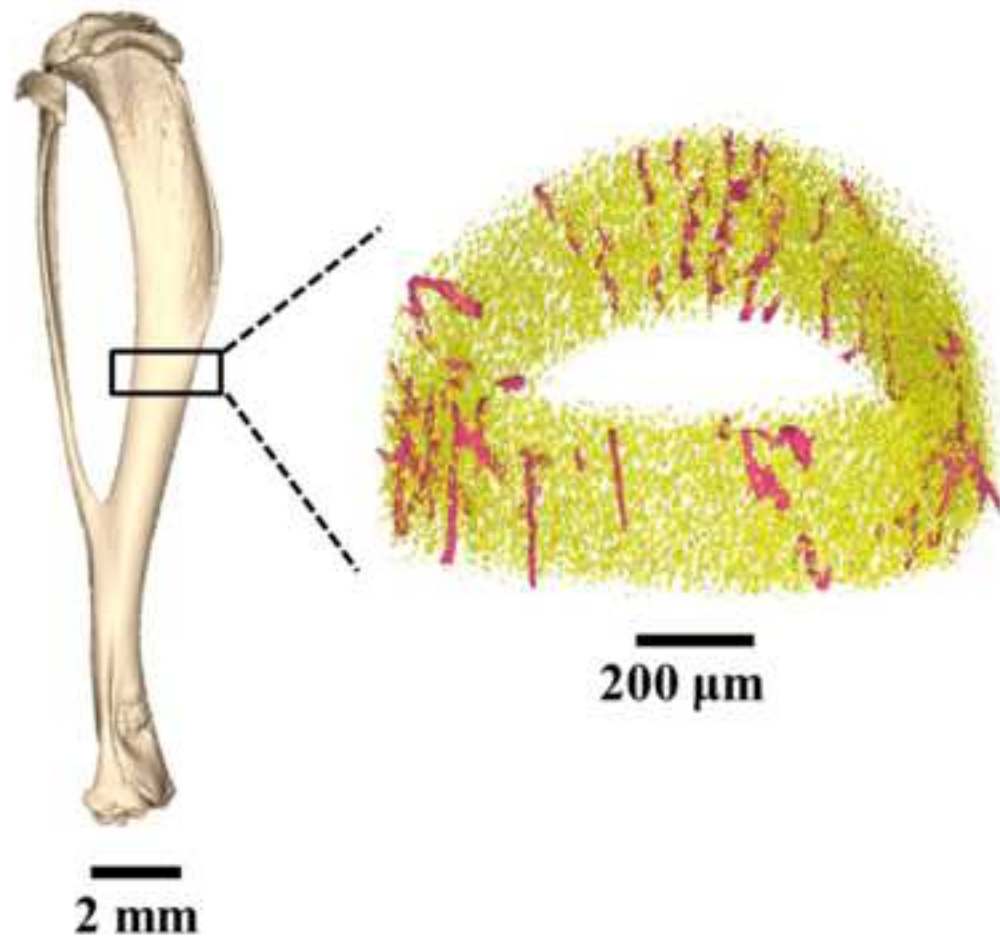


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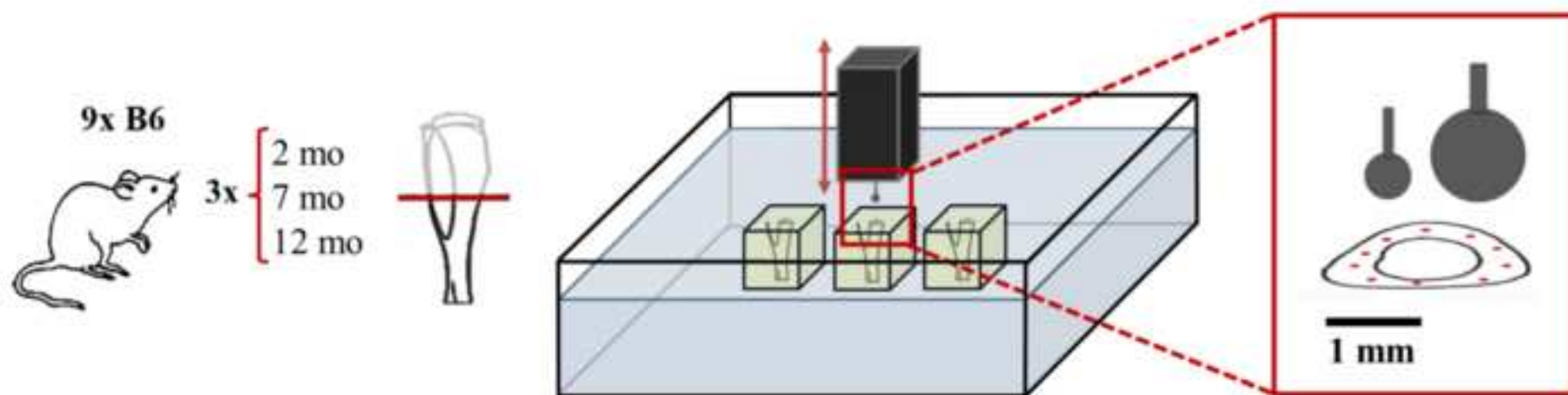


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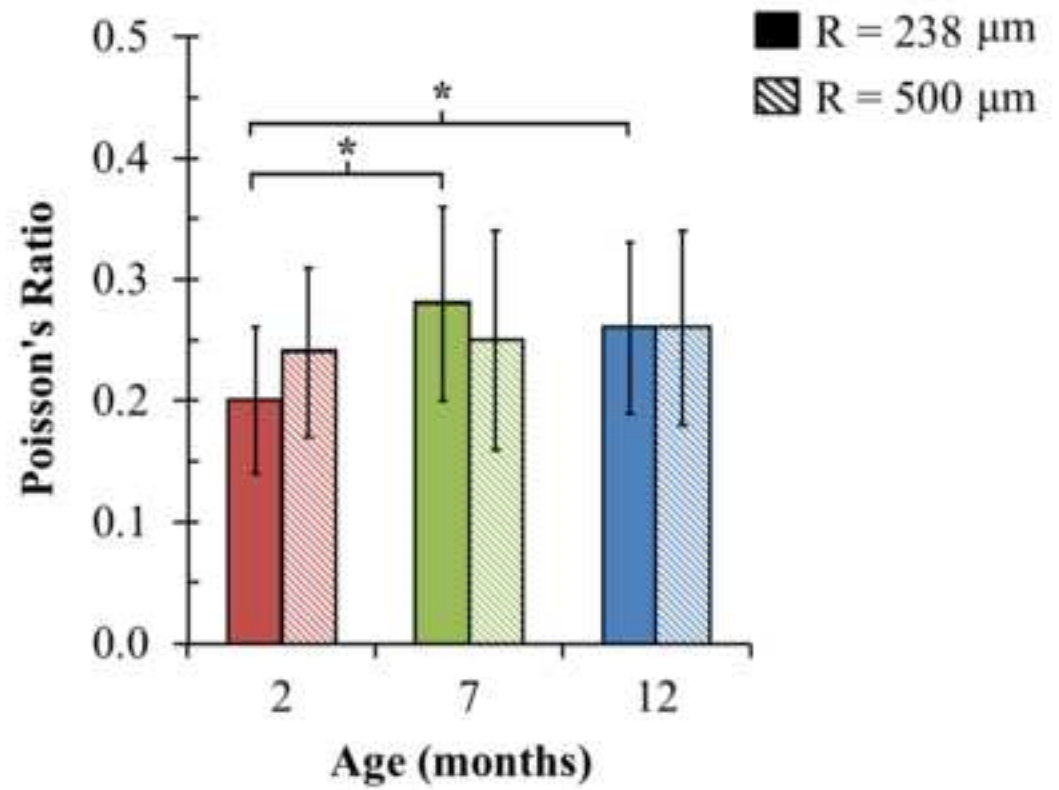
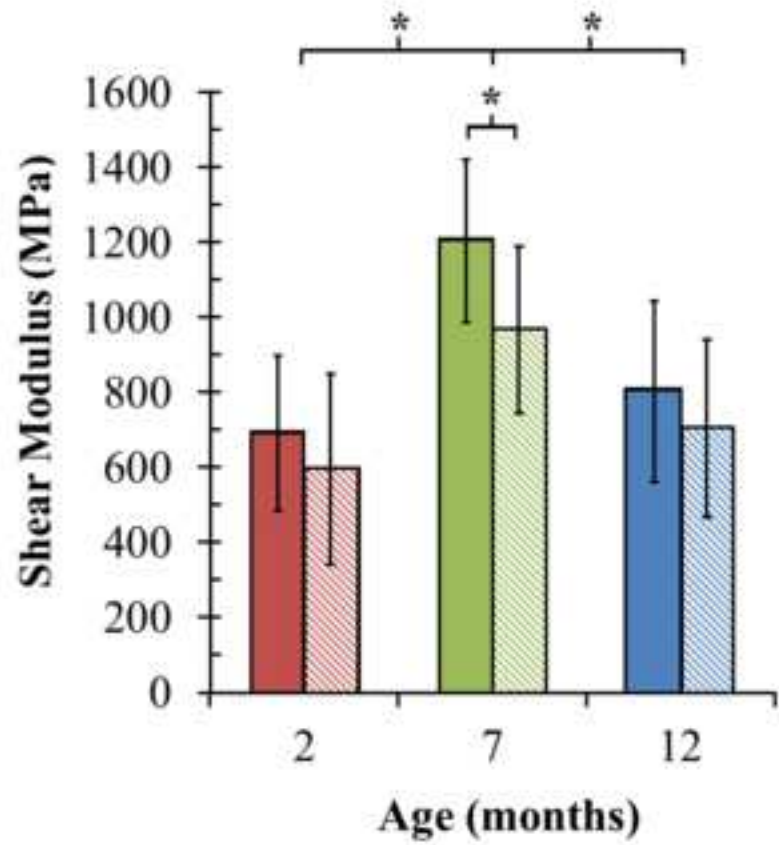
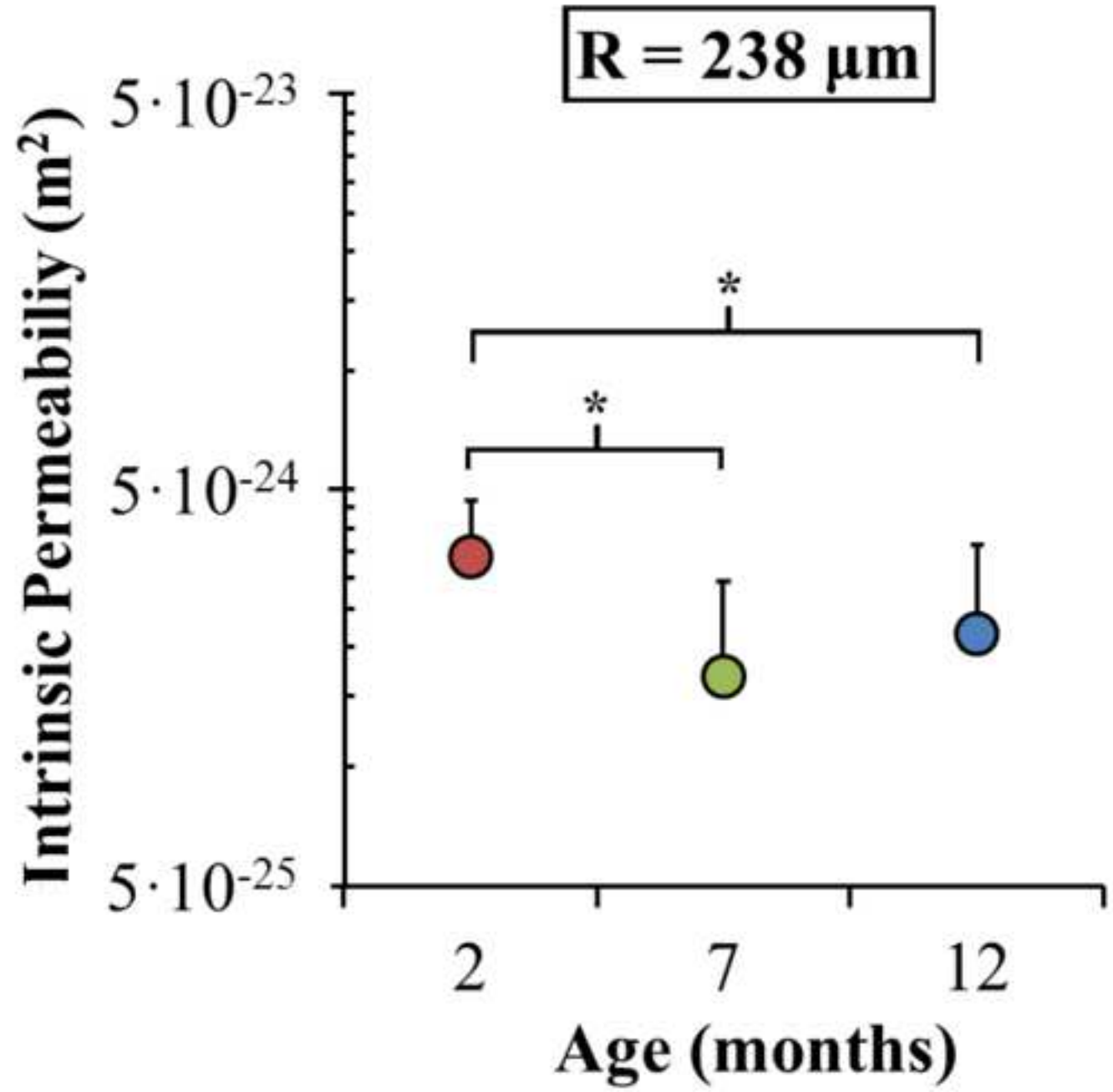


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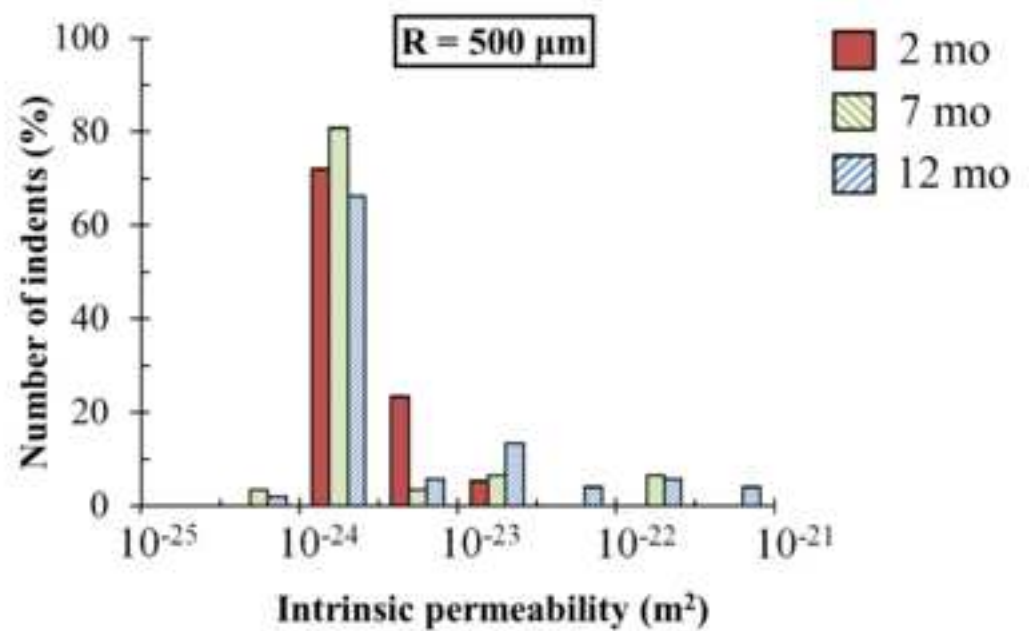
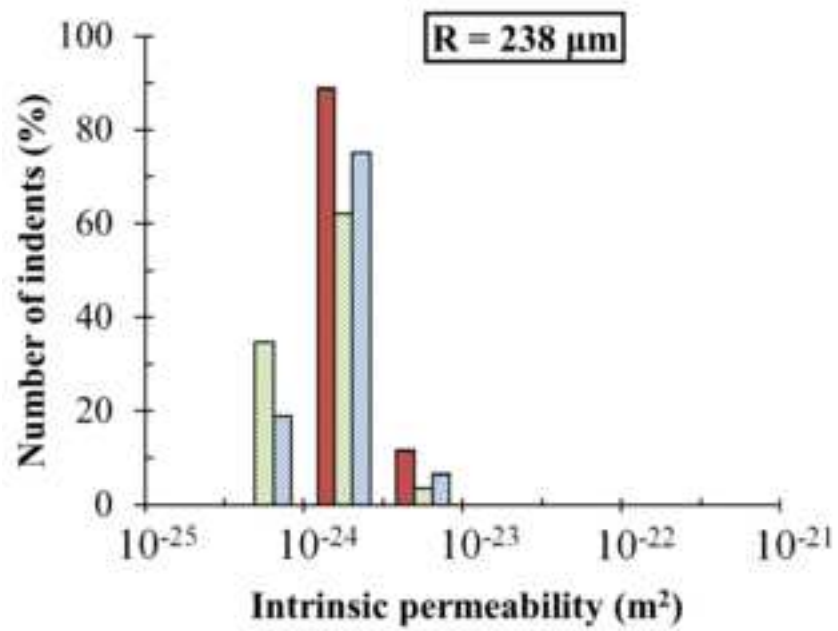


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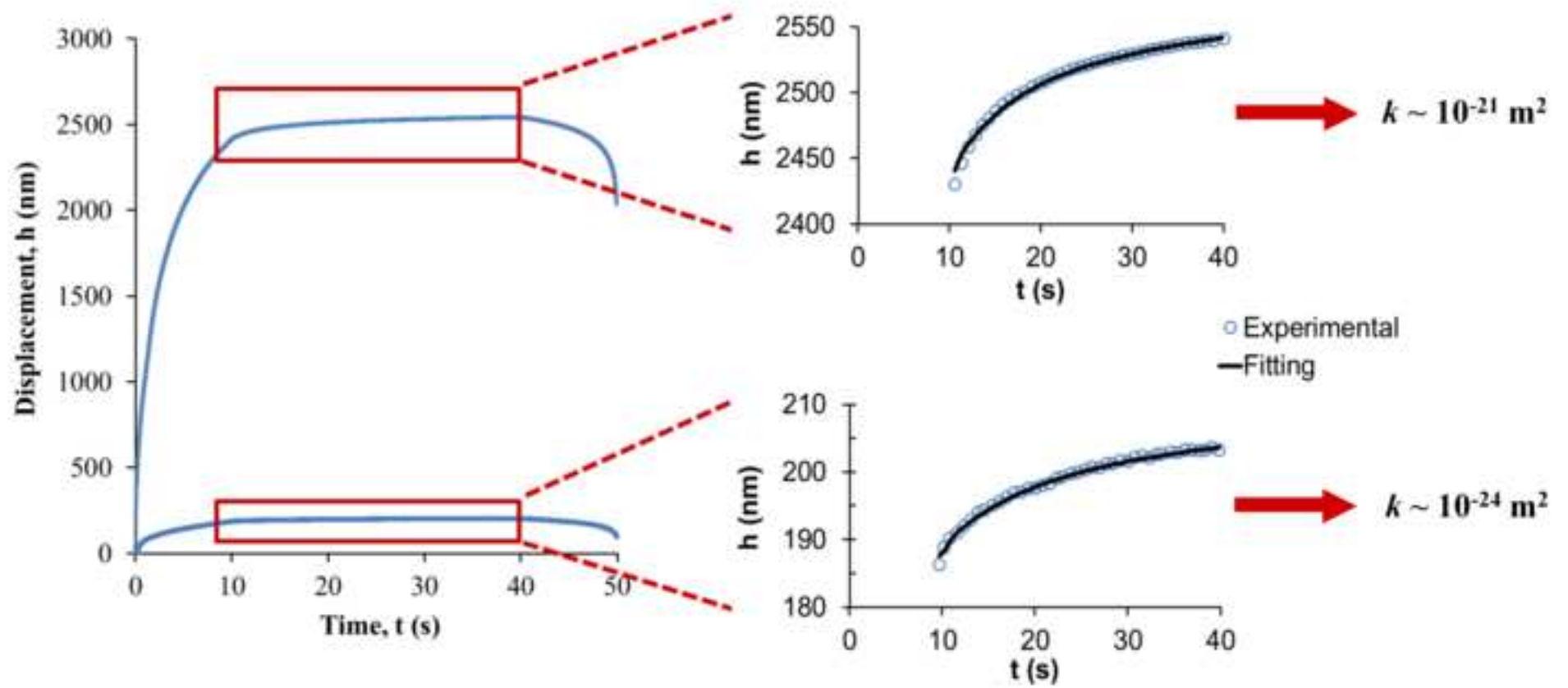


Figure7

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