

Full-Duplex FAS-assisted Base Station for ISAC

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Abstract—This paper studies the use of multiple planar fluid antennas at a full-duplex base station (BS) for integrated sensing and communication (ISAC). In this model, the BS communicates with a downlink user, an uplink user, and performs target sensing simultaneously. Our objective is to maximize the communication sum-rate of the up and downlink users while meeting the sensing and power constraints. Given the problem is non-convex, we first reformulate the problem using the fractional programming (FP) framework. After that, we iteratively optimize the beamforming vectors of the BS, the uplink transmit power from the user, and the antenna positions of both transmit and receive fluid antenna systems (FASs) at the BS. In particular, the transmit and receive beamforming vectors are optimized by utilizing the majorization-minimization (MM) framework, and a closed-form solution for the uplink transmit power is derived. To optimize the BS antenna positions, we transform the problems into convex quadratically constrained quadratic programs (QCQP) by using Taylor series expansion. The subproblems can then be solved based on the successive convex approximation (SCA). Simulation results show that FAS can greatly improve the communication rate compared to the traditional fixed-position antenna (FPA) system.

Index Terms—Fractional programming, fluid antenna system, full-duplex system, integrated sensing and communication.

I. INTRODUCTION

THE SIXTH generation (6G) wireless network is hopeful to revolutionize communications to yet again an unprecedented level far beyond the current systems. This time there is huge excitement around artificial intelligence (AI) and sensing capabilities to innovate a plethora of applications [1], [2], [3]. The primary objectives in 6G can boil down to hitting data rates of 1 terabit per second (Tbps), achieving an extraordinary spectral efficiency of 1000 bps/Hz, and keeping latency as low as 1 microsecond (μ s), according to [4].

To support massive connectivity, conventional schemes rely on multiuser multiple-input multiple-output (MIMO) antenna technologies [5]. Multiuser MIMO emerged as early as 2000

[6], [7] and classical results were reported in [8], [9]. Since the fourth generation (4G), multiuser MIMO has been the root of the physical layer in wireless communications. In recent years, multiuser MIMO has also evolved into massive MIMO, as a key attempt to simplify the precoding design [10], [11]. Extra-large MIMO (XL-MIMO) is also being regarded as one key direction to pursue in the 6G development [12].

While the push to include more antennas at the base station (BS) will continue, this is met with concern for the low power efficiency and the hefty cost of the increasing number of radio-frequency (RF) chains. This has motivated researchers to seek alternatives to enhance MIMO without necessarily increasing the number of antennas. One direction is to leverage the new generation of reconfigurable antennas that offers new degrees-of-freedom (DoFs) within the antenna itself to strengthen the physical layer. In 2020, Wong *et al.* presented a broad concept, referred to as fluid antenna system (FAS), for embracing all forms of shape and position reconfigurability in antennas for improving wireless communications [13], [14], [15]. A recent article in [16] provides a comprehensive tutorial on the topic whereas [17] gives theoretical foundation and interpretation to FAS from the electromagnetic perspective.

The concept of FAS is motivated by the advances in highly reconfigurable antenna structures such as liquid antennas [18], [19], movable arrays [20], [21], metamaterial based antennas [22], [23], [24] and reconfigurable pixels [25], [26], etc. The latter two technologies are particularly suitable since they have practically zero response time and the reconfigurability does not impose high power consumption like the first two.

Following the early results in [13], [14], [15], great efforts have been made to advance the research field. For example, [27] examined the use of FAS to enhance the performance in the millimeter-wave band while [28], [29], [30], [31] studied the performance of FAS under different channel models. FAS with continuous antenna positioning was investigated in [32]. More recently, FAS has also been employed at both ends of a communication channel, with its diversity and multiplexing tradeoff characterized in [33]. FAS has also been shown to be effective in raising the DoF for MIMO in multiuser channels [34] while [35] adopted FAS at the BSs in a cell-free setup.

A branch of research efforts also sees FAS applied to tackle a niche multiple access problem, the one that is able to serve many users on the same physical channel without the channel state information (CSI) at the transmitter side. This has led to the fluid antenna multiple access (FAMA) technique in [36]. Since then, a practical scheme, called slow FAMA [37], [38], was proposed to allow several users to share the same channel without precoding or interference cancellation. More research on FAMA can be found in [39], [40], [41], [42].

Additionally, the application of FAS has also extended to wireless powered communication systems [43], [44], physical-

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layer security [45], [46] and near-field communications [47]. Needless to say, CSI is essential for a FAS-equipped terminal to optimize its antenna positioning. Several methods have been developed to tackle the channel estimation problems in FAS, including the successive Bayesian reconstructor [48], the low-sample-size sparse channel reconstruction (L3SCR) [49], and the linear minimum mean-squared error (LMMSE) technique [50]. In [51], the role of oversampling in the spatial domain in channel estimation for FAS channels was analyzed.

On the other hand, integrated sensing and communication (ISAC) in recent years has been a key driver for 6G [52]. The enormous interest in ISAC stems from the idea of combining sensing and communications into a unified system with shared resources [53], [54]. Despite its brilliance, ISAC puts pressure on the resources that are already very limited. Recent efforts therefore have explored the use of FAS to make ISAC viable. For example, [55] adopted a deep reinforcement learning based approach to maximize the sum rate in the downlink under a sensing constraint for a FAS-aided multiuser MIMO system. In [56] and [57], the results showed a considerable expansion of the ISAC tradeoff region when utilizing FAS compared to the fixed-position antenna (FPA) counterpart. The authors of [58], [59] further applied position-flexible antennas at both the transmitter and receiver sides to perform ISAC tasks in a bistatic radar system, where the transmitter and receiver are separated without self-interference (SI). Most recently, ISAC was also combined with backscatter communications in a FAS-aided system in [60], where the outage probability and ergodic sensing rate were derived. Recognizing the potential of smart environment technologies including FAS, [61] discusses the vision of future ISAC and its many opportunities.

On the other hand, there has been great interest to use full-duplex communication. Compared to traditional half-duplex systems that switch between transmission and reception, full-duplex communication significantly improves spectrum efficiency and reduces latency by enabling simultaneous transmission and reception over the same frequency band [62]. A stochastic-geometry-based analytical framework for the FAS-aided full-duplex communication was proposed in [63], while [64] presented a self-interference cancellation (SIC) framework for the FAS-aided full-duplex system. In [65], the authors investigated the outage probability of a multi-user full-duplex NOMA network, where the users were equipped with FAS. It is anticipated that in ISAC systems, full-duplex technology can further enhance sensing accuracy and real-time performance if the SI can be handled satisfactorily while reducing hardware overhead through the integrated architecture [66].

In this paper, we aim to further the efforts of using FAS for ISAC but different from previous studies, a full-duplex FAS-equipped BS is considered, meaning that the BS is required to transmit to a downlink user and also receive from an uplink user on the same physical data channel for higher spectral efficiency. Note that we consider the use of a mono-static radar and the SI in this paper to see if FAS has sufficient capability for the BS to mitigate the SI for full-duplex communication while performing the ISAC task. In particular, the BS has two separate, planar fluid antenna arrays, one for transmission and another for reception. Our objective is to jointly optimize

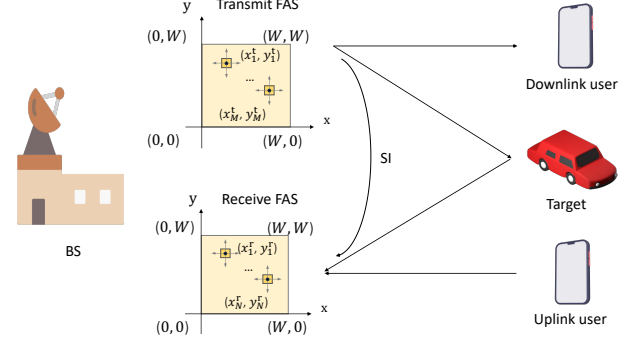


Fig. 1. An ISAC system with a full-duplex FAS-assisted BS, a downlink user, an uplink user, and a sensing target.

the beamforming vectors, the uplink transmit power, and the transmit and receive antenna positions of FAS at the BS to maximize the sum of the communication rates of the uplink and downlink users while satisfying the constraint of sensing signal-to-interference plus noise ratio (SINR).

Our main contributions are summarized as follows:

- First, we formulate the communication rate maximization problem for the full-duplex ISAC system, which is non-convex and intractable due to the coupled variables. To tackle this, we transform the problem using the fractional programming (FP) framework, and propose an alternative optimization algorithm to iteratively optimize the transmit and receive beamforming vectors, the transmit power of the uplink user, and both the transmit and receive antenna positions of the FAS at the BS. We obtain the transmit and receive beamforming vectors using majorization minimization (MM) and provide a closed-form solution for the uplink transmit power optimization.
- When the other variables are fixed, the subproblems of optimizing the transmit and receive antenna positions of the BS remain non-convex and hard to solve. To tackle this, we adopt Taylor series expansion to transform the problems into convex quadratically constrained quadratic program (QCQP) forms that can be solved efficiently. The antenna positions can then be optimized by the successive convex approximation (SCA) technique. Specifically, the proposed theorems and lemmas can reformulate the antenna position optimization problems that share the same structures in Table I into convex forms.
- Simulation results illustrate that using the proposed algorithm, the communication rate obtained by using FAS is much higher than that of the traditional FPA system. While the joint optimization of both transmit and receive antenna positions achieves a higher communication rate, updating only the transmit or receive FAS also greatly improves the system performance.

II. SYSTEM MODEL

A. Signal Model

As shown in Fig. 1, we consider a FAS-assisted full-duplex ISAC system where the BS serves a downlink user, an uplink user, and attempts to sense a target simultaneously. Both users are equipped with a FPA. The BS has an M -antenna planar

TABLE I
SUMMARY OF THE PROPOSED THEOREMS AND LEMMAS

Theorem	Original Function Form	Surrogate Type	Surrogate Function Form	Parameters	Reference Equations
Theorem 1	$ \mathbf{a}^T \mathbf{T}_{\chi 1}^H(\mathbf{V}) \mathbf{b} ^2$	Concave	$\mathbf{v}^T \hat{\mathbf{A}} \mathbf{v} + \hat{c} \mathbf{v} + \hat{d}$	$\hat{\mathbf{A}}$ (NSD), \hat{c} , \hat{d}	(53)
Theorem 1	$ \mathbf{a}^T \mathbf{T}_{\chi 1}^H(\mathbf{V}) \mathbf{b} ^2$	Convex	$-\mathbf{v}^T \hat{\mathbf{A}} \mathbf{v} + \hat{c} \mathbf{v} + \hat{d}$	$\hat{\mathbf{A}}$ (NSD), \hat{c} , \hat{d}	(53), (56)
Theorem 2	$\text{Re}\{\mathbf{a}^T \mathbf{T}_{\chi 1}^H(\mathbf{V}) \mathbf{b}\}$	Concave	$\mathbf{v}^T \tilde{\mathbf{A}} \mathbf{v} + \tilde{c} \mathbf{v} + \tilde{d}$	$\tilde{\mathbf{A}}$ (NSD), \tilde{c} , \tilde{d}	(59)
Theorem 3	$\text{Re}\{\mathbf{a}^T \mathbf{T}_{\chi}^H(\mathbf{V}) \mathbf{b} (\hat{\mathbf{a}}^T \mathbf{T}_{\chi}^H(\mathbf{V}) \mathbf{b})^H\}$	Convex	$\mathbf{v}^T \tilde{\mathbf{A}} \mathbf{v} + \tilde{c} \mathbf{v} + \tilde{d}$	$\tilde{\mathbf{A}}$ (PSD), \tilde{c} , \tilde{d}	(63)
Lemma 1	$ \mathbf{b}^T \mathbf{R}_{\chi 2}(\mathbf{U}) \mathbf{a} ^2$	Concave	$\mathbf{u}^T \hat{\Omega} \mathbf{u} + \hat{p} \mathbf{u} + \hat{q}$	$\hat{\Omega}$ (NSD), \hat{p} , \hat{q}	(40) (53)
Lemma 1	$ \mathbf{b}^T \mathbf{R}_{\chi 2}(\mathbf{U}) \mathbf{a} ^2$	Convex	$-\mathbf{u}^T \hat{\Omega} \mathbf{u} + \hat{p} \mathbf{u} + \hat{q}$	$\hat{\Omega}$ (NSD), \hat{p} , \hat{q}	(40) (53), (56)
Lemma 2	$\text{Re}\{\mathbf{b}^T \mathbf{R}_{\chi 2}(\mathbf{U}) \mathbf{a}\}$	Concave	$\mathbf{u}^T \tilde{\Omega} \mathbf{u} + \tilde{p} \mathbf{u} + \tilde{q}$	$\tilde{\Omega}$ (NSD), \tilde{p} , \tilde{q}	(66)
Lemma 3	$\text{Re}\{(\mathbf{b}^T \mathbf{R}_{\chi}(\mathbf{U}) \hat{\mathbf{a}})(\mathbf{b}^T \mathbf{R}_{\chi}(\mathbf{U}) \mathbf{a})^H\}$	Convex	$\mathbf{u}^T \tilde{\Omega} \mathbf{u} + \tilde{p} \mathbf{u} + \tilde{q}$	$\tilde{\Omega}$ (PSD), \tilde{p} , \tilde{q}	(46) (63)

FAS for transmitting signal and an N -antenna planar FAS for receiving signal. The size of each FAS is $\mathcal{S} = [0, W] \times [0, W]$. Each antenna at the FAS can be freely switched to any position within the given region instantly. The positions of the m -th transmit antenna and the n -th receive antenna are denoted by $\mathbf{v}_m = [x_m^t, y_m^t]^T$ and $\mathbf{u}_n = [x_n^r, y_n^r]^T$, respectively.

Let $\mathbf{w}_t \in \mathbb{C}^{M \times 1}$ and $s_d \sim \mathcal{CN}(0, 1)$ be the precoding vector and information symbol for the downlink user, respectively. Then the signal received by the downlink user is given by

$$y_d = \mathbf{h}_d(\mathbf{V}) \mathbf{w}_t s_d + n_d, \quad (1)$$

where $\mathbf{h}_d(\mathbf{V}) \in \mathbb{C}^{1 \times M}$ is the channel vector from the BS to the downlink user, $\mathbf{V} = [\mathbf{v}_1, \dots, \mathbf{v}_M] \in \mathbb{R}^{2 \times M}$, and $n_d \sim \mathcal{CN}(0, \sigma_d^2)$ is the additive complex white Gaussian noise.

Similarly, denote the uplink symbol and channel by $s_u \sim \mathcal{CN}(0, 1)$ and $\mathbf{h}_u(\mathbf{U}) \in \mathbb{C}^{N \times 1}$, and $\mathbf{U} = [\mathbf{u}_1, \dots, \mathbf{u}_N] \in \mathbb{R}^{2 \times N}$. The received signal at the BS is written as

$$\mathbf{y}_r = \mathbf{h}_u(\mathbf{U}) \sqrt{p_u} s_u + (\mathbf{H}_s(\mathbf{V}, \mathbf{U}) + \mathbf{H}_{\text{SI}}(\mathbf{V}, \mathbf{U})) \mathbf{w}_t s_d + \mathbf{n}_r, \quad (2)$$

where p_u is the transmit power of the uplink user, $\mathbf{H}_s \in \mathbb{C}^{N \times M}$ and $\mathbf{H}_{\text{SI}} \in \mathbb{C}^{N \times M}$ are the sensing and SI channels, respectively, and $\mathbf{n}_r \sim \mathcal{CN}(\mathbf{0}, \sigma_r^2 \mathbf{I})$ is the additive noise.

B. Channel Model

Here, we provide the expressions for the channel vectors \mathbf{h}_d and \mathbf{h}_u , and the channel matrices \mathbf{H}_s and \mathbf{H}_{SI} . Denote the azimuth and elevation angles of departure (AoDs) of the l -th downlink path by ϕ_l^d and θ_l^d , respectively. The propagation distance difference in the l -th path of the downlink channel between the position of the m -th transmit antenna $\mathbf{v}_m = [x_m^t, y_m^t]^T$ and its origin $[0, 0]^T$ is

$$\rho_l^d(\mathbf{v}_m) = x_m^t \delta_l^d + y_m^t \xi_l^d, \quad (3)$$

where $\delta_l^d = \sin \theta_l^d \cos \phi_l^d$ and $\xi_l^d = \cos \theta_l^d$. The steering vector of the l -th path of the downlink channel is thus given by

$$\mathbf{t}_l^d(\mathbf{V}) = \left[e^{-j \frac{2\pi}{\lambda} \rho_l^d(\mathbf{v}_1)}, \dots, e^{-j \frac{2\pi}{\lambda} \rho_l^d(\mathbf{v}_M)} \right]^T \in \mathbb{C}^{M \times 1}, \quad (4)$$

where λ is the wavelength. Let L_d be the number of downlink propagation paths. Then we have

$$\mathbf{h}_d(\mathbf{V}) = \mathbf{1}^H \mathbf{\Gamma}_d \mathbf{T}_d^H(\mathbf{V}) \in \mathbb{C}^{1 \times M}, \quad (5)$$

in which $\mathbf{1}$ represents an all-ones column vector, $\mathbf{\Gamma}_d = \text{diag}\{\gamma_d^1, \dots, \gamma_d^{L_d}\} \in \mathbb{C}^{L_d \times L_d}$ is the channel coefficient matrix, and $\mathbf{T}_d(\mathbf{V}) = [\mathbf{t}_1^d(\mathbf{V}), \dots, \mathbf{t}_{L_d}^d(\mathbf{V})] \in \mathbb{C}^{M \times L_d}$.

Next, we denote the azimuth and elevation angles of arrival (AoAs) of the l -th uplink path by ϕ_l^u and θ_l^u , respectively. The propagation distance difference in the l -th path of the uplink channel between the n -th receive antenna position $\mathbf{u}_n = [x_n^r, y_n^r]^T$ and the origin is given by

$$\rho_l^u(\mathbf{u}_n) = x_n^r \delta_l^u + y_n^r \xi_l^u, \quad (6)$$

where $\delta_l^u = \sin \theta_l^u \cos \phi_l^u$ and $\xi_l^u = \cos \theta_l^u$. Then the steering vector of the uplink channel can be expressed as

$$\mathbf{r}_l^u(\mathbf{U}) = \left[e^{-j \frac{2\pi}{\lambda} \rho_l^u(\mathbf{u}_1)}, \dots, e^{-j \frac{2\pi}{\lambda} \rho_l^u(\mathbf{u}_N)} \right]^T \in \mathbb{C}^{N \times 1}. \quad (7)$$

Let L_u represent the number of uplink propagation paths. The uplink channel can then be written as

$$\mathbf{h}_u(\mathbf{U}) = \mathbf{R}_u(\mathbf{U}) \mathbf{\Gamma}_u \mathbf{1} \in \mathbb{C}^{N \times 1}, \quad (8)$$

where $\mathbf{\Gamma}_u = \text{diag}\{\gamma_u^1, \dots, \gamma_u^{L_u}\} \in \mathbb{C}^{L_u \times L_u}$ is the channel coefficient matrix and $\mathbf{R}_u(\mathbf{U}) = [\mathbf{r}_1^u(\mathbf{U}), \dots, \mathbf{r}_{L_u}^u(\mathbf{U})] \in \mathbb{C}^{N \times L_u}$.

Consider a mono-static radar, and that the AoA and AoD of the sensing channel are the same. Denote the azimuth and elevation angles of the sensing path with respect to the BS by ϕ^s and θ^s , respectively. The receiving and transmitting steering vectors of the sensing channel are written as

$$\begin{cases} \mathbf{a}_r(\mathbf{U}) = \left[e^{-j \frac{2\pi}{\lambda} \rho_r(\mathbf{u}_1)}, \dots, e^{-j \frac{2\pi}{\lambda} \rho_r(\mathbf{u}_N)} \right]^T \in \mathbb{C}^{N \times 1}, \\ \mathbf{a}_t(\mathbf{V}) = \left[e^{-j \frac{2\pi}{\lambda} \rho_t(\mathbf{v}_1)}, \dots, e^{-j \frac{2\pi}{\lambda} \rho_t(\mathbf{v}_M)} \right]^T \in \mathbb{C}^{M \times 1}, \end{cases} \quad (9)$$

where $\rho_r(\mathbf{u}_n) \triangleq x_n^r \delta^s + y_n^r \xi^s$ and $\rho_t(\mathbf{v}_m) = x_m^t \delta^s + y_m^t \xi^s$ with $\delta^s = \sin \theta^s \cos \phi^s$ and $\xi^s = \cos \theta^s$. The sensing channel can therefore be expressed as

$$\mathbf{H}_s(\mathbf{V}, \mathbf{U}) = \alpha_s \mathbf{a}_r(\mathbf{U}) \mathbf{a}_t^H(\mathbf{V}) \in \mathbb{C}^{N \times M}, \quad (10)$$

where α_s is the reflection coefficient including the path loss and the radar cross section (RCS).

Denote the AoDs and AoAs of the SI channel by $(\phi_{r,l}^{\text{SI}}, \theta_{r,l}^{\text{SI}})$ and $(\phi_{t,l}^{\text{SI}}, \theta_{t,l}^{\text{SI}})$, respectively. The receiving and transmitting steering vectors of the SI channel are found as

$$\begin{cases} \mathbf{r}_l^{\text{SI}}(\mathbf{U}) = \left[e^{-j \frac{2\pi}{\lambda} \rho_{r,l}^{\text{SI}}(\mathbf{u}_1)}, \dots, e^{-j \frac{2\pi}{\lambda} \rho_{r,l}^{\text{SI}}(\mathbf{u}_N)} \right]^T \in \mathbb{C}^{N \times 1}, \\ \mathbf{t}_l^{\text{SI}}(\mathbf{V}) = \left[e^{-j \frac{2\pi}{\lambda} \rho_{t,l}^{\text{SI}}(\mathbf{v}_1)}, \dots, e^{-j \frac{2\pi}{\lambda} \rho_{t,l}^{\text{SI}}(\mathbf{v}_M)} \right]^T \in \mathbb{C}^{M \times 1}, \end{cases} \quad (11)$$

where $\rho_{r,l}^{\text{SI}}(\mathbf{u}_n) \triangleq x_n^r \delta_{r,l}^{\text{SI}} + y_n^r \xi_{r,l}^{\text{SI}}$ with $\delta_{r,l}^{\text{SI}} = \sin \theta_{r,l}^{\text{SI}} \cos \phi_{r,l}^{\text{SI}}$ and $\xi_{r,l}^{\text{SI}} = \cos \theta_{r,l}^{\text{SI}}$, and $\rho_{t,l}^{\text{SI}}(\mathbf{v}_m) \triangleq x_m^t \delta_{t,l}^{\text{SI}} + y_m^t \xi_{t,l}^{\text{SI}}$ with $\delta_{t,l}^{\text{SI}} =$

$\sin \theta_{t,l}^{\text{SI}} \cos \phi_{t,l}^{\text{SI}}$ and $\xi_{t,l}^{\text{SI}} = \cos \theta_{t,l}^{\text{SI}}$. Let L_{SI} be the number of paths of the SI channel. Then, the SI channel is written as

$$\mathbf{H}_{\text{SI}}(\mathbf{V}, \mathbf{U}) = \mathbf{R}_{\text{SI}}(\mathbf{U}) \mathbf{I}_{L_{\text{SI}}} \mathbf{T}_{\text{SI}}^H(\mathbf{V}) \in \mathbb{C}^{N \times M}, \quad (12)$$

where $\mathbf{I}_{L_{\text{SI}}} = \text{diag}\{\gamma_{\text{SI}}^1, \dots, \gamma_{\text{SI}}^{L_{\text{SI}}}\} \in \mathbb{C}^{L_{\text{SI}} \times L_{\text{SI}}}$ is the channel coefficient matrix, $\mathbf{R}_{\text{SI}}(\mathbf{U}) = [\mathbf{r}_{\text{SI}}^1(\mathbf{U}), \dots, \mathbf{r}_{\text{SI}}^{L_{\text{SI}}}(\mathbf{U})] \in \mathbb{C}^{N \times L_{\text{SI}}}$, and $\mathbf{T}_{\text{SI}}(\mathbf{V}) = [\mathbf{t}_{\text{SI}}^1(\mathbf{V}), \dots, \mathbf{t}_{\text{SI}}^{L_{\text{SI}}}(\mathbf{V})] \in \mathbb{C}^{M \times L_{\text{SI}}}$.

III. PROBLEM FORMULATION

A. Communication Metric

According to (1), the SINR of the downlink user is

$$\eta_d(\mathbf{V}, \mathbf{w}_t) = \frac{|\mathbf{h}_d(\mathbf{V}) \mathbf{w}_t|^2}{\sigma_d^2}. \quad (13)$$

Similarly, the uplink communication SINR at the BS is

$$\eta_u(\Phi) = \frac{p_u |\mathbf{w}_r^H \mathbf{h}_u(\mathbf{U})|^2}{|\mathbf{w}_r^H \mathbf{H}(\mathbf{V}, \mathbf{U}) \mathbf{w}_t|^2 + \sigma_r^2 \|\mathbf{w}_r^H\|^2}, \quad (14)$$

where $\mathbf{w}_r \in \mathbb{C}^{N \times 1}$ is the linear beamformer adopted by the BS for detecting s_u , $\mathbf{H}(\mathbf{V}, \mathbf{U}) = \mathbf{H}_s(\mathbf{V}, \mathbf{U}) + \mathbf{H}_{\text{SI}}(\mathbf{V}, \mathbf{U})$, and $\Phi = \{\mathbf{V}, \mathbf{U}, \mathbf{w}_t, \mathbf{w}_r, p_u\}$ contains all the optimizing variables.

B. Sensing Metric

Since the detection probability is directly proportional to the sensing SINR [67], maximizing the sensing SINR has a direct effect of maximizing the detection probability. Therefore, we adopt the sensing SINR, given by

$$\eta_s(\Phi) = \frac{|\mathbf{w}_r^H \mathbf{H}_s(\mathbf{V}, \mathbf{U}) \mathbf{w}_t|^2}{p_u |\mathbf{w}_r^H \mathbf{h}_u(\mathbf{U})|^2 + |\mathbf{w}_r^H \mathbf{H}_{\text{SI}}(\mathbf{V}, \mathbf{U}) \mathbf{w}_t|^2 + \sigma_r^2 \|\mathbf{w}_r^H\|^2}, \quad (15)$$

as the main sensing performance metric.

C. Optimization Problem

We aim to maximize the communication sum rate subject to a sensing SINR constraint by optimizing the transmit and receive antenna positions \mathbf{V} and \mathbf{U} , the precoding and receive beamforming vectors \mathbf{w}_t and \mathbf{w}_r , and the uplink transmit power p_u . Mathematically, this is formulated as

$$\begin{aligned} \max_{\Phi} \quad & f_0(\Phi) = \log(1 + \eta_d(\mathbf{V}, \mathbf{w}_t)) + \log(1 + \eta_u(\Phi)) \\ \text{s.t.} \quad & \eta_s(\Phi) \geq \eta, \\ & \|\mathbf{w}_t\|^2 \leq P_t, \\ & 0 \leq p_u \leq P_u, \\ & \mathbf{v}_m, \mathbf{v}_{m'} \in \mathcal{S}, \mathbf{v}_m \neq \mathbf{v}_{m'}, \forall m, m' \in \mathcal{M}, m \neq m', \\ & \mathbf{u}_n, \mathbf{u}_{n'} \in \mathcal{S}, \mathbf{u}_n \neq \mathbf{u}_{n'}, \forall n, n' \in \mathcal{N}, n \neq n', \end{aligned} \quad (16)$$

where η is the sensing performance threshold, P_t and P_u are the power budgets of the BS and the uplink user, and $\mathcal{M} = \{1, \dots, M\}$ and $\mathcal{N} = \{1, \dots, N\}$ denote the index sets of the transmit and receive antennas, respectively.

IV. PROPOSED SOLUTION

Problem (16) is non-convex and hence intractable. To proceed, we first remove Φ from the log operation in the objective function $f_0(\Phi)$. Specifically, we introduce auxiliary variables $\Delta = \{\Delta_d, \Delta_u\}$ and transform $f_0(\Phi)$ to

$$\begin{aligned} f_1(\Phi, \Delta) = & \log(1 + \Delta_d) - \Delta_d + \frac{(1 + \Delta_d) |\mathbf{h}_d(\mathbf{V}) \mathbf{w}_t|^2}{|\mathbf{h}_d(\mathbf{V}) \mathbf{w}_t|^2 + \sigma_d^2} + \log(1 + \Delta_u) \\ & - \Delta_u + \frac{(1 + \Delta_u) p_u |\mathbf{w}_r^H \mathbf{h}_u(\mathbf{U})|^2}{p_u |\mathbf{w}_r^H \mathbf{h}_u(\mathbf{U})|^2 + |\mathbf{w}_r^H \mathbf{H}(\mathbf{V}, \mathbf{U}) \mathbf{w}_t|^2 + \sigma_r^2 \|\mathbf{w}_r^H\|^2}. \end{aligned} \quad (17)$$

For fixed Φ , by setting $\frac{\partial f_1}{\partial \Delta_d}$ and $\frac{\partial f_1}{\partial \Delta_u}$ to zero, we have

$$\begin{cases} \Delta_d^* = \frac{|\mathbf{h}_d(\mathbf{V}) \mathbf{w}_t|^2}{\sigma_d^2}, \\ \Delta_u^* = \frac{p_u |\mathbf{w}_r^H \mathbf{h}_u(\mathbf{U})|^2}{|\mathbf{w}_r^H \mathbf{H}(\mathbf{V}, \mathbf{U}) \mathbf{w}_t|^2 + \sigma_r^2 \|\mathbf{w}_r^H\|^2}. \end{cases} \quad (18)$$

It is easy to prove that $f_1(\Phi, \Delta^*) = f_0(\Phi)$. Therefore, (16) can be equivalently transformed to

$$\begin{aligned} \max_{\Phi, \Delta} \quad & f_1(\Phi, \Delta) \\ \text{s.t.} \quad & f_s(\Phi) \geq 0, \\ & \|\mathbf{w}_t\|^2 \leq P_t, \\ & 0 \leq p_u \leq P_u, \\ & \mathbf{v}_m, \mathbf{v}_{m'} \in \mathcal{S}, \mathbf{v}_m \neq \mathbf{v}_{m'}, \forall m, m' \in \mathcal{M}, m \neq m', \\ & \mathbf{u}_n, \mathbf{u}_{n'} \in \mathcal{S}, \mathbf{u}_n \neq \mathbf{u}_{n'}, \forall n, n' \in \mathcal{N}, n \neq n', \end{aligned} \quad (19)$$

where $f_s(\Phi) = |\mathbf{w}_r^H \mathbf{H}_s(\mathbf{V}, \mathbf{U}) \mathbf{w}_t|^2 - \eta(p_u |\mathbf{w}_r^H \mathbf{h}_u(\mathbf{U})|^2 + |\mathbf{w}_r^H \mathbf{H}_{\text{SI}}(\mathbf{V}, \mathbf{U}) \mathbf{w}_t|^2 + \sigma_r^2 \|\mathbf{w}_r^H\|^2)$. To deal with the fractional terms in $f_1(\Phi, \Delta)$, we further introduce auxiliary variables $\omega = \{\omega_d, \omega_u\}$ as in [68], [69] to reformulate $f_1(\Phi, \Delta)$ as

$$\begin{aligned} f_2(\Phi, \Delta, \omega) = & \log(1 + \Delta_d) - \Delta_d \\ & + (1 + \Delta_d) \left[2\text{Re}\{\omega_d^H \mathbf{h}_d(\mathbf{V}) \mathbf{w}_t\} - |\omega_d|^2 (|\mathbf{h}_d(\mathbf{V}) \mathbf{w}_t|^2 + \sigma_d^2) \right] \\ & + \log(1 + \Delta_u) - \Delta_u + p_u (1 + \Delta_u) \left[2\text{Re}\{\omega_u^H \mathbf{w}_r^H \mathbf{h}_u(\mathbf{U})\} \right. \\ & \left. - |\omega_u|^2 (p_u |\mathbf{w}_r^H \mathbf{h}_u(\mathbf{U})|^2 + |\mathbf{w}_r^H \mathbf{H}(\mathbf{V}, \mathbf{U}) \mathbf{w}_t|^2 + \sigma_r^2 \|\mathbf{w}_r^H\|^2) \right]. \end{aligned} \quad (20)$$

By setting $\frac{\partial f_2}{\partial \omega_d}$ and $\frac{\partial f_2}{\partial \omega_u}$ to zero, we can obtain the optimal value of $f_2(\Phi, \Delta, \omega)$ at

$$\begin{cases} \omega_d^* = \frac{\mathbf{h}_d(\mathbf{V}) \mathbf{w}_t}{|\mathbf{h}_d(\mathbf{V}) \mathbf{w}_t|^2 + \sigma_d^2}, \\ \omega_u^* = \frac{\mathbf{w}_r^H \mathbf{h}_u(\mathbf{U})}{p_u |\mathbf{w}_r^H \mathbf{h}_u(\mathbf{U})|^2 + |\mathbf{w}_r^H \mathbf{H}(\mathbf{V}, \mathbf{U}) \mathbf{w}_t|^2 + \sigma_r^2 \|\mathbf{w}_r^H\|^2}. \end{cases} \quad (21)$$

Since $f_2(\Phi, \Delta, \omega^*) = f_1(\Phi, \Delta)$, (19) can be recast as

$$\begin{aligned} \max_{\Phi, \Delta, \omega} \quad & f_2(\Phi, \Delta, \omega) \\ \text{s.t.} \quad & f_s(\Phi) \geq 0, \\ & \|\mathbf{w}_t\|^2 \leq P_t, \\ & 0 \leq p_u \leq P_u, \\ & \mathbf{v}_m, \mathbf{v}_{m'} \in \mathcal{S}, \mathbf{v}_m \neq \mathbf{v}_{m'}, \forall m, m' \in \mathcal{M}, m \neq m', \\ & \mathbf{u}_n, \mathbf{u}_{n'} \in \mathcal{S}, \mathbf{u}_n \neq \mathbf{u}_{n'}, \forall n, n' \in \mathcal{N}, n \neq n'. \end{aligned} \quad (22)$$

Though (22) is much simpler than (16), it is still hard. In the sequel, we iteratively update each variable while considering others fixed. For notation convenience, when \mathbf{V} and \mathbf{U} are fixed, we omit them from the channel variables, e.g., we denote $\mathbf{h}_d(\mathbf{V})$ and $\mathbf{h}_u(\mathbf{U})$ as \mathbf{h}_d and \mathbf{h}_u , respectively.

A. Updating Auxiliary Variables

According to the FP framework, we find the optimal values of Δ and ω based on (18) and (21), respectively.

B. Updating Transmit Beamforming Vector

Here, we aim to solve the sub-problem of optimizing \mathbf{w}_t . With fixed $\{\mathbf{V}, \mathbf{U}, \mathbf{w}_r, p_u, \Delta, \omega\}$, (22) reduces to

$$\max_{\mathbf{w}_t} \quad -\mathbf{w}_t^H \phi_1 \mathbf{w}_t + \mu_1 \text{Re}\{\omega_d^H \mathbf{h}_d \mathbf{w}_t\} \quad (23a)$$

$$\text{s.t.} \quad \mathbf{w}_t^H \phi_2 \mathbf{w}_t - \mathbf{w}_t^H \phi_3 \mathbf{w}_t + \mu_2 \leq 0, \quad (23b)$$

$$\|\mathbf{w}_t\|^2 \leq P_t, \quad (23c)$$

where $\mu_1 = 2(1 + \Delta_d)$, $\phi_1 = (1 + \Delta_d)|\omega_d|^2 \mathbf{h}_d^H \mathbf{h}_d + p_u(1 + \Delta_u)|\omega_u|^2 \mathbf{H}^H \mathbf{w}_r \mathbf{w}_r^H \mathbf{H}$, $\phi_2 = \eta \mathbf{H}_{\text{SI}}^H \mathbf{w}_r \mathbf{w}_r^H \mathbf{H}_{\text{SI}}$, $\phi_3 = \mathbf{H}_s^H \mathbf{w}_r \mathbf{w}_r^H \mathbf{H}_s$, and $\mu_2 = \eta(p_u \|\mathbf{w}_r^H \mathbf{h}_u\|^2 + \sigma_r^2 \|\mathbf{w}_r^H\|^2)$. Since (23b) is in the difference of convex (DC) form, we apply the MM framework to iteratively optimize \mathbf{w}_t . In particular, a lower-bound of $\mathbf{w}_t^H \phi_3 \mathbf{w}_t$ can be constructed through the Taylor series expansion, given by

$$\mathbf{w}_t^H \phi_3 \mathbf{w}_t \geq 2\text{Re}\{\mathbf{w}_{t,0}^H \phi_3 (\mathbf{w}_t - \mathbf{w}_{t,0})\} + \mathbf{w}_{t,0}^H \phi_3 \mathbf{w}_{t,0}, \quad (24)$$

where $\mathbf{w}_{t,0}$ is the value of \mathbf{w}_t in the previous iteration. Then (23) can be rewritten as

$$\begin{aligned} \max_{\mathbf{w}_t} \quad & -\mathbf{w}_t^H \phi_1 \mathbf{w}_t + \mu_1 \text{Re}\{\omega_d^H \mathbf{h}_d \mathbf{w}_t\} \\ \text{s.t.} \quad & \mathbf{w}_t^H \phi_2 \mathbf{w}_t - 2\text{Re}\{\mathbf{w}_{t,0}^H \phi_3 \mathbf{w}_t\} + \mu_3 \leq 0, \\ & \|\mathbf{w}_t\|^2 \leq P_t, \end{aligned} \quad (25)$$

where $\mu_3 = \mu_2 + \mathbf{w}_{t,0}^H \phi_3 \mathbf{w}_{t,0}$. Obviously, problem (25) is a QCQP and thus can be solved by CVX.

C. Updating Receive Beamforming Vector

Now, we deal with the sub-problem of optimizing \mathbf{w}_r . With fixed $\{\mathbf{V}, \mathbf{U}, \mathbf{w}_t, p_u, \Delta, \omega\}$, problem (22) becomes

$$\begin{aligned} \max_{\mathbf{w}_r} \quad & -\mathbf{w}_r^H \psi_1 \mathbf{w}_r + 2\text{Re}\{\omega_u^H \mathbf{w}_r^H \mathbf{h}_u\} \\ \text{s.t.} \quad & \mathbf{w}_r^H \psi_2 \mathbf{w}_r - \mathbf{w}_r^H \psi_3 \mathbf{w}_r \leq 0, \end{aligned} \quad (26)$$

where $\psi_1 = |\omega_u|^2(p_u \mathbf{h}_u \mathbf{h}_u^H + \mathbf{H} \mathbf{w}_t \mathbf{w}_t^H \mathbf{H}^H + \sigma_r^2 \mathbf{I})$, $\psi_2 = \eta(p_u \mathbf{h}_u \mathbf{h}_u^H + \mathbf{H}_{\text{SI}} \mathbf{w}_t \mathbf{w}_t^H \mathbf{H}_{\text{SI}}^H + \sigma_r^2 \mathbf{I})$, and $\psi_3 = \mathbf{H}_s \mathbf{w}_t \mathbf{w}_t^H \mathbf{H}_s^H$. Note that (26) has the same form as (23). Therefore, it can also be transformed into a QCQP and solved by CVX.

D. Updating Uplink Transmit Power

Next, we address the sub-problem related to p_u . With fixed $\{\mathbf{V}, \mathbf{U}, \mathbf{w}_t, \mathbf{w}_r, \Delta, \omega\}$, (22) becomes

$$\begin{aligned} \max_{p_u} \quad & -\alpha_1 p_u^2 + \alpha_2 p_u \\ \text{s.t.} \quad & p_u \leq \alpha_3, \\ & 0 \leq p_u \leq P_u, \end{aligned} \quad (27)$$

where $\alpha_1 = |\omega_u|^2 |\mathbf{w}_r^H \mathbf{h}_u|^2$, $\alpha_2 = 2\text{Re}\{\omega_u^H \mathbf{w}_r^H \mathbf{h}_u\} - |\omega_u|^2 (|\mathbf{w}_r^H \mathbf{H} \mathbf{w}_t|^2 + \sigma_r^2 \|\mathbf{w}_r^H\|^2)$, and $\alpha_3 = \left[|\mathbf{w}_r^H \mathbf{H}_s \mathbf{w}_t|^2 - \eta (|\mathbf{w}_r^H \mathbf{H}_{\text{SI}} \mathbf{w}_t|^2 + \sigma_r^2 \|\mathbf{w}_r^H\|^2) \right] / \left(\eta |\mathbf{w}_r^H \mathbf{h}_u|^2 \right)$. Obviously, problem (27) is feasible only when $\alpha_3 \geq 0$. If $\alpha_3 \geq 0$ and $\alpha_1 = 0$, the optimal solution of the problem can be reached at $p_u = 0$ if $\alpha_2 \leq 0$, or at $p_u = \min\{\alpha_3, P_u\}$ if $\alpha_2 > 0$. If $\alpha_3 \geq 0$ and $\alpha_1 > 0$, the objective function of (27) is a parabola with a downward opening. Then, it is easy to verify that for $\alpha_3 \geq 0$ and $\alpha_1 > 0$, the optimal value of p_u is given by

$$p_u^* = \min \left\{ \max \left\{ \frac{\alpha_2}{2\alpha_1}, 0 \right\}, \min\{\alpha_3, P_u\} \right\}. \quad (28)$$

E. Updating Transmit Antenna Positions

In this subsection, we solve the sub-problem of optimizing \mathbf{V} using the proposed theorems and the SCA algorithm. With fixed $\{\mathbf{U}, \mathbf{w}_t, \mathbf{w}_r, p_u, \Delta, \omega\}$, problem (22) becomes

$$\begin{aligned} \max_{\mathbf{V}} \quad & \alpha_d \left(2\text{Re}\{\omega_d^H \mathbf{h}_d(\mathbf{V}) \mathbf{w}_t\} - |\omega_d|^2 |\mathbf{h}_d(\mathbf{V}) \mathbf{w}_t|^2 \right) \\ & - \alpha_u |\mathbf{w}_r^H \mathbf{H}(\mathbf{V}) \mathbf{w}_t|^2 \\ \text{s.t.} \quad & |\mathbf{w}_r^H \mathbf{H}_s(\mathbf{V}) \mathbf{w}_t|^2 - \eta |\mathbf{w}_r^H \mathbf{H}_{\text{SI}}(\mathbf{V}) \mathbf{w}_t|^2 \geq \beta_1, \\ & \mathbf{v}_m, \mathbf{v}_{m'} \in \mathcal{S}, \mathbf{v}_m \neq \mathbf{v}_{m'}, \forall m, m \in \mathcal{M}, m \neq m', \end{aligned} \quad (29)$$

where $\alpha_d = 1 + \Delta_d$, $\alpha_u = p_u(1 + \Delta_u)|\omega_u|^2$, and $\beta_1 = \eta(p_u \|\mathbf{w}_r^H \mathbf{h}_u\|^2 + \sigma_r^2 \|\mathbf{w}_r^H\|^2)$. Denoting $\mathbf{T}_s(\mathbf{V}) = \mathbf{a}_t(\mathbf{V})$ and considering the model in Section II-B, (29) is rewritten as

$$\begin{aligned} \max_{\mathbf{V}} \quad & \alpha_d \left(2\text{Re}\{\omega_d^H \mathbf{1}^H \Gamma_d \mathbf{T}_d^H(\mathbf{V}) \mathbf{w}_t\} - |\omega_d|^2 |\mathbf{1}^H \Gamma_d \mathbf{T}_d^H(\mathbf{V}) \mathbf{w}_t|^2 \right) \\ & - \alpha_u \left(|\alpha_s \mathbf{w}_r^H \mathbf{a}_r \mathbf{T}_s^H(\mathbf{V}) \mathbf{w}_t|^2 + |\mathbf{w}_r^H \mathbf{R}_{\text{SI}} \Gamma_{\text{SI}} \mathbf{T}_{\text{SI}}^H(\mathbf{V}) \mathbf{w}_t|^2 \right. \\ & \left. + 2\text{Re}\{(\alpha_s \mathbf{w}_r^H \mathbf{a}_r \mathbf{T}_s^H(\mathbf{V}) \mathbf{w}_t)(\mathbf{w}_r^H \mathbf{R}_{\text{SI}} \Gamma_{\text{SI}} \mathbf{T}_{\text{SI}}^H(\mathbf{V}) \mathbf{w}_t)^H\} \right) \\ \text{s.t.} \quad & \eta |\mathbf{w}_r^H \mathbf{R}_{\text{SI}} \Gamma_{\text{SI}} \mathbf{T}_{\text{SI}}^H(\mathbf{V}) \mathbf{w}_t|^2 - |\alpha_s \mathbf{w}_r^H \mathbf{a}_r \mathbf{T}_s^H(\mathbf{V}) \mathbf{w}_t|^2 \leq -\beta_1, \\ & \mathbf{v}_m, \mathbf{v}_{m'} \in \mathcal{S}, \mathbf{v}_m \neq \mathbf{v}_{m'}, \forall m, m \in \mathcal{M}, m \neq m'. \end{aligned} \quad (30)$$

Since the problem is still non-convex and difficult to solve, we resort to SCA. For convenience, denote $\mathbf{v} = \text{vector}\{\mathbf{V}\} = [x_1^t, \dots, x_M^t, y_1^t, \dots, y_M^t]^T = [v_1, \dots, v_{2M}]^T$.

Theorem 1. For arbitrary vectors $\mathbf{a} = [a_1, \dots, a_L]^T$ and $\mathbf{b} = [b_1, \dots, b_M]^T$, $\mathbf{v}^T \hat{\mathbf{A}} \mathbf{v} + \hat{\mathbf{c}} \mathbf{v} + \hat{\mathbf{d}}$ and $-\mathbf{v}^T \hat{\mathbf{A}} \mathbf{v} + \hat{\mathbf{c}} \mathbf{v} + \hat{\mathbf{d}}$ are concave and convex quadratic surrogate functions for $|\mathbf{a}^T \mathbf{T}_{\chi_1}^H(\mathbf{V}) \mathbf{b}|^2$ respectively, where $\chi_1 \in \{d, \text{SI}, s\}$, $\hat{\mathbf{A}}$, $\hat{\mathbf{c}}$, and $\hat{\mathbf{d}}$ are given in (53), while $\bar{\mathbf{c}}$ and $\bar{\mathbf{d}}$ are given in (56), and $\hat{\mathbf{A}}$ is a negative semi-definite (NSD) matrix.

Proof: See Appendix A. ■

Based on Theorem 1, a concave quadratic surrogate function of $|\alpha_s \mathbf{w}_r^H \mathbf{a}_r \mathbf{T}_s^H(\mathbf{V}) \mathbf{w}_t|^2$ can be obtained as

$$\mathbf{v}^T \hat{\mathbf{A}}_s \mathbf{v} + \hat{\mathbf{c}}_s \mathbf{v} + \hat{d}_s. \quad (31)$$

Moreover, we can obtain the convex quadratic surrogate functions of $|\mathbf{1}^H \mathbf{T}_d \mathbf{T}_d^H(\mathbf{V}) \mathbf{w}_t|^2$, $|\alpha_s \mathbf{w}_r^H \mathbf{a}_r \mathbf{T}_s^H(\mathbf{V}) \mathbf{w}_t|^2$, and $|\mathbf{w}_r^H \mathbf{R}_{\text{SI}} \mathbf{T}_{\text{SI}}^H(\mathbf{V}) \mathbf{w}_t|^2$ as

$$-\mathbf{v}^T \hat{\mathbf{A}}_d \mathbf{v} + \bar{\mathbf{c}}_d \mathbf{v} + \bar{d}_d, \quad (32)$$

$$-\mathbf{v}^T \hat{\mathbf{A}}_s \mathbf{v} + \bar{\mathbf{c}}_s \mathbf{v} + \bar{d}_s, \quad (33)$$

$$-\mathbf{v}^T \hat{\mathbf{A}}_{\text{SI}} \mathbf{v} + \bar{\mathbf{c}}_{\text{SI}} \mathbf{v} + \bar{d}_{\text{SI}}. \quad (34)$$

Theorem 2. For any $\mathbf{a} \in \mathbb{C}^{L \times 1}$ and $\mathbf{b} \in \mathbb{C}^{M \times 1}$, a concave quadratic surrogate function for $\text{Re}\{\mathbf{a}^T \mathbf{T}_{\chi_1}^H(\mathbf{V}) \mathbf{b}\}$ is given by $\mathbf{v}^T \tilde{\mathbf{A}} \mathbf{v} + \tilde{\mathbf{c}} \mathbf{v} + \tilde{d}$, where $\chi_1 \in \{\text{d}, \text{SI}, \text{s}\}$, and $\tilde{\mathbf{A}}$ is an NSD matrix defined in (59) along with $\tilde{\mathbf{c}}$ and \tilde{d} .

Proof: See Appendix B. ■

According to Theorem 2, a concave quadratic surrogate function of $\text{Re}\{\omega_d^H \mathbf{1}^H \mathbf{T}_d \mathbf{T}_d^H(\mathbf{V}) \mathbf{w}_t\}$ can be written as

$$\mathbf{v}^T \tilde{\mathbf{A}}_d \mathbf{v} + \tilde{\mathbf{c}}_d \mathbf{v} + \tilde{d}_d. \quad (35)$$

Theorem 3. For any vectors $\mathbf{a} = [a_1, \dots, a_L]^T$, $\mathbf{b} = [b_1, \dots, b_M]^T$, and $\tilde{\mathbf{a}} = [\tilde{a}_1, \dots, \tilde{a}_L]^T$, a convex quadratic surrogate function for $\text{Re}\{(\mathbf{a}^T \mathbf{T}_{\chi}^H(\mathbf{V}) \mathbf{b})(\tilde{\mathbf{a}}^T \mathbf{T}_{\tilde{\chi}}^H(\mathbf{V}) \mathbf{b})^H\}$ can be expressed as $\mathbf{v}^T \tilde{\mathbf{A}} \mathbf{v} + \tilde{\mathbf{c}} \mathbf{v} + \tilde{d}$, where $\chi, \tilde{\chi} \in \{\text{d}, \text{SI}, \text{s}\}$, $\chi \neq \tilde{\chi}$, $\tilde{\mathbf{A}}$ is a positive semi-definite (PSD) matrix, and $\tilde{\mathbf{A}}$, $\tilde{\mathbf{c}}$, \tilde{d} are given in (63).

Proof: See Appendix C. ■

Then we denote the convex quadratic surrogate function for $\text{Re}\{(\alpha_s \mathbf{w}_r^H \mathbf{a}_r \mathbf{T}_s^H(\mathbf{V}) \mathbf{w}_t)(\mathbf{w}_r^H \mathbf{R}_{\text{SI}} \mathbf{T}_{\text{SI}}^H(\mathbf{V}) \mathbf{w}_t)^H\}$ using Theorem 3 as

$$\mathbf{v}^T \tilde{\mathbf{A}}_{\text{SI}} \mathbf{v} + \tilde{\mathbf{c}}_{\text{SI}} \mathbf{v} + \tilde{d}_{\text{SI}}. \quad (36)$$

Denoting $\mathbf{A}_1 = \alpha_d(2\tilde{\mathbf{A}}_d + |\omega_d|^2 \hat{\mathbf{A}}_d) + \alpha_u(\hat{\mathbf{A}}_s + \hat{\mathbf{A}}_{\text{SI}} - 2\tilde{\mathbf{A}}_{\text{SI}})$, $\mathbf{c}_1 = \alpha_d(2\tilde{\mathbf{c}}_d + |\omega_d|^2 \bar{\mathbf{c}}_d) - \alpha_u(\bar{\mathbf{c}}_s + \bar{\mathbf{c}}_{\text{SI}} + 2\tilde{\mathbf{c}}_{\text{SI}})$, $d_1 = \alpha_d(2\tilde{d}_d - |\omega_d|^2 \bar{d}_d) - \alpha_u(\bar{d}_s + \bar{d}_{\text{SI}} + 2\tilde{d}_{\text{SI}})$, $\mathbf{A}_2 = -\eta \hat{\mathbf{A}}_{\text{SI}} - \hat{\mathbf{A}}_s$, $\mathbf{c}_2 = \eta \bar{\mathbf{c}}_{\text{SI}} - \bar{\mathbf{c}}_s$, and $d_2 = \eta \bar{d}_{\text{SI}} - \bar{d}_s$, (30) can be transformed to

$$\max_{\mathbf{v}} \quad \mathbf{v}^T \mathbf{A}_1 \mathbf{v} + \mathbf{c}_1 \mathbf{v} + d_1, \quad (37a)$$

$$\text{s.t.} \quad \mathbf{v}^T \mathbf{A}_2 \mathbf{v} + \mathbf{c}_2 \mathbf{v} + d_2 \leq -\beta_1, \quad (37b)$$

$$0 \leq v_m \leq W, m = 1, \dots, 2M, \quad (37c)$$

$$[v_m, v_{m+M}] \neq [v_{m'}, v_{m'+M}], \forall m, m' \in \mathcal{M}, m \neq m'. \quad (37d)$$

Without (37d), (37) is convex and can be solved by CVX. Noting that in Theorems 1, 2, and 3, the quadratic surrogate functions are based on the Taylor series expansion in the given antenna positions \mathbf{V}_0 , we apply the SCA method to solve (29). Specifically, we start SCA from valid \mathbf{v} that satisfies (37d), and then update \mathbf{v} only if it satisfies (37d) in each iteration. The main steps of solving (29) are summarized in Algorithm 1.

Algorithm 1 SCA-based algorithm for solving (29)

Initialize \mathbf{V}_0 by randomly generating antenna positions that satisfy (37d). Let $i = 0$.

repeat

 Calculate \mathbf{A}_1 , \mathbf{c}_1 , d_1 , \mathbf{A}_2 , \mathbf{c}_2 , and d_2 .

 Solve (37a), (37b) and (37c) by CVX and obtain \mathbf{v} .

if \mathbf{v} satisfies (37d) **then**

 Let $i = i+1$ and $\mathbf{V}^{(i)} = [v_1, \dots, v_M; v_{M+1}, \dots, v_{2M}]$.

end if

until convergence

Let $\mathbf{V}^{(i)}$ be the solution of problem (29).

F. Updating Receive Antenna Positions

In the following, we address the sub-problem of optimizing \mathbf{U} using the proposed lemmas and the SCA algorithm. With fixed $\{\mathbf{V}, \mathbf{w}_t, \mathbf{w}_r, p_u, \mathbf{A}, \omega\}$, (22) can be recast as

$$\begin{aligned} \max_{\mathbf{U}} \quad & 2\text{Re}\{\omega_u^H \mathbf{w}_r^H \mathbf{h}_u(\mathbf{U})\} - |\omega_u|^2 (p_u |\mathbf{w}_r^H \mathbf{h}_u(\mathbf{U})|^2 + |\mathbf{w}_r^H \mathbf{H}(\mathbf{U}) \mathbf{w}_t|^2) \\ \text{s.t.} \quad & |\mathbf{w}_r^H \mathbf{H}_s(\mathbf{U}) \mathbf{w}_t|^2 - \eta p_u |\mathbf{w}_r^H \mathbf{h}_u(\mathbf{U})|^2 - \eta |\mathbf{w}_r^H \mathbf{H}_{\text{SI}}(\mathbf{U}) \mathbf{w}_t|^2 \geq \beta_2, \\ & \mathbf{u}_n, \mathbf{u}_{n'} \in \mathcal{S}, \mathbf{u}_n \neq \mathbf{u}_{n'}, \forall n, n' \in \mathcal{N}, n \neq n', \end{aligned} \quad (38)$$

where $\beta_2 = \eta \sigma_r^2 \|\mathbf{w}_r^H\|^2$. For convenience, denote $\mathbf{R}_s(\mathbf{U}) = \mathbf{a}_r(\mathbf{U})$. Based on the model in Section II-B, (38) is

$$\begin{aligned} \max_{\mathbf{U}} \quad & 2\text{Re}\{\omega_u^H \mathbf{w}_r^H \mathbf{R}_u(\mathbf{U}) \mathbf{T}_u \mathbf{1}\} - |\omega_u|^2 (p_u |\mathbf{w}_r^H \mathbf{R}_u(\mathbf{U}) \mathbf{T}_u \mathbf{1}|^2 \\ & + |\alpha_s \mathbf{w}_r^H \mathbf{R}_s(\mathbf{U}) \mathbf{a}_t^H \mathbf{w}_t|^2 + |\mathbf{w}_r^H \mathbf{R}_{\text{SI}}(\mathbf{U}) \mathbf{T}_{\text{SI}} \mathbf{T}_{\text{SI}}^H \mathbf{w}_t|^2 \\ & + 2\text{Re}\{(\alpha_s \mathbf{w}_r^H \mathbf{R}_s(\mathbf{U}) \mathbf{a}_t^H \mathbf{w}_t)(\mathbf{w}_r^H \mathbf{R}_{\text{SI}}(\mathbf{U}) \mathbf{T}_{\text{SI}} \mathbf{T}_{\text{SI}}^H \mathbf{w}_t)^H\}) \\ \text{s.t.} \quad & (\eta p_u |\mathbf{w}_r^H \mathbf{R}_u(\mathbf{U}) \mathbf{T}_u \mathbf{1}|^2 + \eta |\mathbf{w}_r^H \mathbf{R}_{\text{SI}}(\mathbf{U}) \mathbf{T}_{\text{SI}} \mathbf{T}_{\text{SI}}^H \mathbf{w}_t|^2 \\ & - |\alpha_s \mathbf{w}_r^H \mathbf{R}_s(\mathbf{U}) \mathbf{a}_t^H \mathbf{w}_t|^2 + \beta_2) \leq 0, \\ & \mathbf{u}_n, \mathbf{u}_{n'} \in \mathcal{S}, \mathbf{u}_n \neq \mathbf{u}_{n'}, \forall n, n' \in \mathcal{N}, n \neq n'. \end{aligned} \quad (39)$$

Although (39) cannot be transformed directly into a convex problem, we can obtain the concave and convex quadratic surrogate functions for the terms in (39) based on Theorems 1–3. For convenience, we denote $\mathbf{u} = \text{vector}\{\mathbf{U}\} = [x_1^r, \dots, x_N^r, y_1^i, \dots, y_N^i]^T = [u_1, \dots, u_{2N}]^T$.

Lemma 1. For $\chi_2 \in \{\text{u}, \text{SI}, \text{s}\}$, $\forall \mathbf{a} = [a_1, \dots, a_L]^T$ and $\forall \mathbf{b} = [b_1, \dots, b_N]^T$, we can construct concave and convex quadratic surrogate functions for $|\mathbf{b}^T \mathbf{R}_{\chi_2}(\mathbf{U}) \mathbf{a}|^2$ as $\mathbf{u}^T \hat{\mathbf{\Omega}} \mathbf{u} + \hat{\mathbf{p}} \mathbf{u} + \hat{\mathbf{q}}$ and $-\mathbf{u}^T \hat{\mathbf{\Omega}} \mathbf{u} + \hat{\mathbf{p}} \mathbf{v} + \hat{\mathbf{q}}$, respectively, according to the transformation in (40) and Theorem 1.

Proof: Now we omit the subscript χ_2 for brevity. For vectors $\mathbf{a} = [a_1, \dots, a_L]^T$ and $\mathbf{b} = [b_1, \dots, b_N]^T$, we know that $\mathbf{b}^T \mathbf{R}(\mathbf{U}) \mathbf{a} = \sum_{l=1}^L \sum_{n=1}^N a_l r_l(\mathbf{u}_n) b_n$, where $r_l(\mathbf{u}_n) =$

$e^{-j\frac{2\pi}{\lambda}\rho_l(\mathbf{u}_n)}$. Then, similar to (49), $|\mathbf{b}^T \mathbf{R}(\mathbf{U}) \mathbf{a}|^2$ becomes

$$\begin{aligned} & |\mathbf{b}^T \mathbf{R}(\mathbf{U}) \mathbf{a}|^2 \\ &= \sum_{i=1}^L \sum_{m=1}^N \sum_{l=1}^L \sum_{n=1}^N a_l r_l(\mathbf{u}_n) b_n b_m^H r_i^H(\mathbf{u}_m) a_i^H \\ &= \sum_{i=1}^L \sum_{l=1}^L |a_i| |a_l| \left[\sum_{m=1}^N \sum_{n=1}^N |b_m| |b_n| \cos(\hat{f}_{i,l}(\mathbf{u}_m, \mathbf{u}_n)) \right], \end{aligned} \quad (40)$$

where $\hat{f}_{i,l}(\mathbf{u}_m, \mathbf{u}_n) = \frac{2\pi}{\lambda} [\rho_i(\mathbf{u}_m) - \rho_l(\mathbf{u}_n)] + \angle(a_l b_n b_m^H a_i^H)$. Since (40) has a similar form to that of (49), the concave and convex quadratic surrogate functions of $|\mathbf{b}^T \mathbf{R}(\mathbf{U}) \mathbf{a}|^2$ can be obtained using Theorem 1 by taking $\hat{f}_{i,l} \rightarrow f_{i,l}$, $\mathbf{u} \rightarrow \mathbf{v}$, and $N \rightarrow M$. As a consequence, Lemma 1 is now proven. ■

Using Lemma 1, we can derive a concave quadratic surrogate functions of $|\alpha_s \mathbf{w}_r^H \mathbf{R}_s(\mathbf{U}) \mathbf{a}_t^H \mathbf{w}_t|^2$ as

$$\mathbf{u}^T \hat{\Omega}_s \mathbf{u} + \hat{\mathbf{p}}_s \mathbf{u} + \hat{q}_s, \quad (41)$$

and furthermore, the convex quadratic surrogate functions of $|\mathbf{w}_r^H \mathbf{R}_u(\mathbf{U}) \mathbf{I}_u \mathbf{1}|^2$, $|\alpha_s \mathbf{w}_r^H \mathbf{R}_s(\mathbf{U}) \mathbf{a}_t^H \mathbf{w}_t|^2$, and $|\mathbf{w}_r^H \mathbf{R}_{SI}(\mathbf{U}) \mathbf{I}_{SI} \mathbf{T}_{SI}^H \mathbf{w}_t|^2$ are obtained as

$$-\mathbf{u}^T \hat{\Omega}_u \mathbf{u} + \bar{\mathbf{p}}_u \mathbf{v} + \bar{q}_u, \quad (42)$$

$$-\mathbf{u}^T \hat{\Omega}_s \mathbf{u} + \bar{\mathbf{p}}_s \mathbf{v} + \bar{q}_s, \quad (43)$$

$$-\mathbf{u}^T \hat{\Omega}_{SI} \mathbf{u} + \bar{\mathbf{p}}_{SI} \mathbf{v} + \bar{q}_{SI}. \quad (44)$$

Lemma 2. For any vectors $\mathbf{a} = [a_1, \dots, a_L]^T$ and $\mathbf{b} = [b_1, \dots, b_N]^T$, $\mathbf{u}^T \tilde{\Omega} \mathbf{u} + \tilde{\mathbf{p}} \mathbf{u} + \tilde{q}$ is a concave quadratic surrogate function for $\text{Re}\{\mathbf{b}^T \mathbf{R}_{\chi_2}(\mathbf{U}) \mathbf{a}\} \forall \chi_2 \in \{\text{u, SI, s}\}$, where $\tilde{\Omega}$ is NSD, and $\tilde{\Omega}$, $\tilde{\mathbf{p}}$ and \tilde{q} are given in (66).

Proof: See Appendix D. ■

Based on Lemma 2, a concave quadratic surrogate function of $\text{Re}\{\omega_u^H \mathbf{w}_r^H \mathbf{R}_u(\mathbf{U}) \mathbf{I}_u \mathbf{1}\}$ can be obtained as

$$\mathbf{u}^T \tilde{\Omega}_u \mathbf{u} + \tilde{\mathbf{p}}_u \mathbf{u} + \tilde{q}_u. \quad (45)$$

Lemma 3. By letting $\tilde{f}_{i,l} \rightarrow \check{f}_{i,l}$, $\mathbf{u} \rightarrow \mathbf{v}$, and $N \rightarrow M$, a convex quadratic surrogate function of $\text{Re}\{(\mathbf{b}^T \mathbf{R}_{\check{\chi}}(\mathbf{U}) \check{\mathbf{a}})(\mathbf{b}^T \mathbf{R}_{\chi}(\mathbf{U}) \mathbf{a})^H\}$ can be written as $\mathbf{u}^T \tilde{\Omega} \mathbf{u} + \tilde{\mathbf{p}} \mathbf{u} + \tilde{q}$ using Theorem 3, where $\chi, \check{\chi} \in \{\text{u, SI, s}\}$, $\chi \neq \check{\chi}$, $\mathbf{a} \in \mathbb{C}^{L \times 1}$, $\check{\mathbf{a}} \in \mathbb{C}^{\tilde{L} \times 1}$ and $\mathbf{b} \in \mathbb{C}^{N \times 1}$.

Proof: With $\mathbf{a} = [a_1, \dots, a_L]^T$, $\mathbf{b} = [b_1, \dots, b_N]^T$, and $\check{\mathbf{a}} = [\check{a}_1, \dots, \check{a}_{\tilde{L}}]^T$, we get $\mathbf{b}^T \mathbf{R}_{\chi}(\mathbf{U}) \mathbf{a} = \sum_{i=1}^L \sum_{m=1}^N a_i r_i^{\chi}(\mathbf{u}_m) b_m$ and $\mathbf{b}^T \mathbf{R}_{\check{\chi}}(\mathbf{U}) \check{\mathbf{a}} = \sum_{l=1}^{\tilde{L}} \sum_{n=1}^N \check{a}_l r_l^{\check{\chi}}(\mathbf{u}_n) b_n$, where $r_i^{\chi}(\mathbf{u}_m) = e^{-j\frac{2\pi}{\lambda}\rho_i^{\chi}(\mathbf{u}_m)}$. Then, similar to (60), we obtain

$$\begin{aligned} & \text{Re}\{(\mathbf{b}^T \mathbf{R}_{\check{\chi}}(\mathbf{U}) \check{\mathbf{a}})(\mathbf{b}^T \mathbf{R}_{\chi}(\mathbf{U}) \mathbf{a})^H\} \\ &= \text{Re}\left\{ \sum_{i=1}^L \sum_{m=1}^N \sum_{l=1}^{\tilde{L}} \sum_{n=1}^N \check{a}_l r_l^{\check{\chi}}(\mathbf{u}_n) b_n b_m^H (r_i^{\chi}(\mathbf{u}_m))^H a_i^H \right\} \\ &= \sum_{i=1}^L \sum_{l=1}^{\tilde{L}} |a_i| |\check{a}_l| \left[\sum_{m=1}^N \sum_{n=1}^N |b_m| |b_n| \cos(\check{f}_{i,l}(\mathbf{u}_m, \mathbf{u}_n)) \right], \end{aligned} \quad (46)$$

where $\check{f}_{i,l}(\mathbf{u}_m, \mathbf{u}_n) = \frac{2\pi}{\lambda} [\rho_i^{\chi}(\mathbf{u}_m) - \rho_l^{\check{\chi}}(\mathbf{u}_n)] + \angle(\check{a}_l b_n b_m^H a_i^H)$. Considering $\check{f}_{i,l} \rightarrow \check{f}_{i,l}$, $\mathbf{u} \rightarrow \mathbf{v}$, and $N \rightarrow M$, (46) is the same

as (60). The convex surrogate function $\mathbf{u}^T \tilde{\Omega} \mathbf{u} + \tilde{\mathbf{p}} \mathbf{u} + \tilde{q}$ can thus be obtained by Theorem 3, which proves Lemma 3. ■

Based on Lemma 3, we can now express the convex quadratic surrogate function for $\text{Re}\{(\alpha_s \mathbf{w}_r^H \mathbf{R}_s(\mathbf{U}) \mathbf{a}_t^H \mathbf{w}_t)(\mathbf{w}_r^H \mathbf{R}_{SI}(\mathbf{U}) \mathbf{I}_{SI} \mathbf{T}_{SI}^H \mathbf{w}_t)^H\}$ as

$$\mathbf{v}^T \tilde{\Omega}_{sSI} \mathbf{v} + \tilde{\mathbf{p}}_{sSI} \mathbf{v} + \tilde{q}_{sSI}. \quad (47)$$

Denoting $\Omega_1 = 2\tilde{\Omega}_u + |\omega_u|^2(p_u \hat{\Omega}_u + \hat{\Omega}_s + \hat{\Omega}_{SI} - 2\tilde{\Omega}_{sSI})$, $\mathbf{p}_1 = 2\tilde{\mathbf{p}}_u - |\omega_u|^2(p_u \bar{\mathbf{p}}_u + \bar{\mathbf{p}}_s + \bar{\mathbf{p}}_{SI} + 2\tilde{\mathbf{p}}_{sSI})$, $q_1 = 2\tilde{q}_u - |\omega_u|^2(p_u \bar{q}_u + \bar{q}_s + \bar{q}_{SI} + 2\tilde{q}_{sSI})$, $\Omega_2 = -\eta p_u \hat{\Omega}_u - \eta \hat{\Omega}_{SI} - \hat{\Omega}_s$, $\mathbf{p}_2 = \eta p_u \bar{\mathbf{p}}_u + \eta \bar{\mathbf{p}}_{SI} - \hat{\mathbf{p}}_s$, and $q_2 = \eta p_u \bar{q}_u + \eta \bar{q}_{SI} - \hat{q}_s$, (39) is transformed to

$$\max_{\mathbf{u}} \quad \mathbf{u}^T \Omega_1 \mathbf{u} + \mathbf{p}_1 \mathbf{u} + q_1, \quad (48a)$$

$$\text{s.t.} \quad \mathbf{u}^T \Omega_2 \mathbf{u} + \mathbf{p}_2 \mathbf{u} + q_2 \leq -\beta_2, \quad (48b)$$

$$0 \leq u_n \leq W, n = 1, \dots, 2N, \quad (48c)$$

$$[u_n, u_{n+N}] \neq [u_{n'}, u_{n'+N}], \forall n, n' \in \mathcal{N}, n \neq n'. \quad (48d)$$

Note that (48) has the same form as (37). Therefore, we can solve the original problem (38) using Algorithm 1.

G. Alternative Optimization

So far, we have provided different schemes for optimizing each variable. Overall, the main steps of solving problem (16) can be summarized in Algorithm 2. The summary of the proposed theorems and lemmas is given in Table I.

Algorithm 2 Alternative optimization for solving (16)

Initialize: $\mathbf{w}_t, \mathbf{w}_r, p_u, \mathbf{V}, \mathbf{U}$.

Using the FP framework to reformulate the original problem (16) as (22) by introducing variables Δ and ω .

repeat

1. *Update* Δ and ω using (18) and (21), respectively.

2. *Optimize* \mathbf{w}_t : obtain the sub-problem (23) of optimizing the transmit beamforming vector and update \mathbf{w}_t via (25).

3. *Optimize* \mathbf{w}_r : solve the sub-problem (26) using CVX to optimize the receive beamforming vector \mathbf{w}_t .

4. *Optimize* p_u : obtain the sub-problem (27) of optimizing the uplink transmit power p_u and optimize it through the closed-form solution in (28), respectively.

5. *Optimize* \mathbf{V} : transform the sub-problem (29) into (37) based on Theorems 1, 2, 3 and update the transmit FAS positions \mathbf{V} by using Algorithm 1.

6. *Optimize* \mathbf{U} : transform the sub-problem (38) into (48) based on Lemmas 1, 2, 3 and update the receive FAS positions \mathbf{U} by using Algorithm 1.

until convergence

H. Convergence and Complexity Analysis

1) *Convergence Analysis:* To begin, we denote the objective function of (29) by $f(\mathbf{v})$ and (37a) by $g(\mathbf{v})$. According to (53), (56), (59), and (63), we know that $f(\mathbf{v}^{(i+1)}) \geq g(\mathbf{v}^{(i+1)}|\mathbf{v}^{(i)})$ and $f(\mathbf{v}^{(i)}) = g(\mathbf{v}^{(i)}|\mathbf{v}^{(i)})$. In each iteration, we can always find $\mathbf{v}^{(i+1)}$ satisfying $g(\mathbf{v}^{(i+1)}|\mathbf{v}^{(i)}) \geq g(\mathbf{v}^{(i)}|\mathbf{v}^{(i)})$.

The convergence of Algorithm 1 is thus guaranteed since $f(\mathbf{v}^{(i+1)}) \geq g(\mathbf{v}^{(i+1)}|\mathbf{v}^{(i)}) \geq g(\mathbf{v}^{(i)}|\mathbf{v}^{(i)}) = f(\mathbf{v}^{(i)})$.

For Algorithm 2, the communication rate increases in each iteration by optimizing $\Delta, \omega, \mathbf{w}_t, \mathbf{w}_r, p_u, \mathbf{V}, \mathbf{U}$ iteratively. The convergence of Algorithm 2 is guaranteed since the communication rate is upper-bounded.

2) *Complexity Analysis*: We assume that the number of propagation paths for each channel is the same, i.e., $L_d = L_u = L_{SI} = L$. Algorithm 1 involves solving a QCQP problem using CVX for a vector variable with $2M$ elements, which has a complexity of $\mathcal{O}((2M)^3)$. Denoting the maximum number of iterations in Algorithm 1 by N_{SCA} , the complexity of updating \mathbf{V} and \mathbf{U} using Algorithm 1 are $\mathcal{O}_V = \mathcal{O}(N_{SCA}[(2M)^3 + M^2L^2])$ and $\mathcal{O}_U = \mathcal{O}(N_{SCA}[(2N)^3 + N^2L^2])$, respectively. Calculating p_u based on (28) has a complexity of $\mathcal{O}_p = \mathcal{O}(NM)$. Denote the maximum number of iterations in optimizing \mathbf{w}_t and \mathbf{w}_r by N_t and N_r , respectively. The complexity of updating the beamforming vectors \mathbf{w}_t and \mathbf{w}_r are $\mathcal{O}_t = \mathcal{O}(N_t(M)^3 + M(N+M))$ and $\mathcal{O}_r = \mathcal{O}(N_r(N)^3 + N(N+M))$, respectively. Denote the maximum number of iterations of Algorithm 2 by N_{AO} , solving (16) requires a complexity of $\mathcal{O}(N_{AO}(\mathcal{O}_t + \mathcal{O}_r + \mathcal{O}_p + \mathcal{O}_V + \mathcal{O}_U))$.

V. SIMULATION RESULTS

Here, we evaluate the performance of the proposed algorithms using Monte Carlo simulation. The carrier frequency is 30 GHz. The azimuth and elevation AoAs and AoDs follow uniform distribution over $[0, \pi]$, and all the channel coefficients $\gamma \sim \mathcal{CN}(0, 1)$. We assume that the number of paths is equal, i.e., $L_d = L_u = L_{SI} = L$. Considering unit noise power, the maximum transmit signal-to-noise ratios (SNRs) of the BS and the uplink user are $\text{SNR}_t = 10 \log P_t$ dB and $\text{SNR}_u = 10 \log P_u$ dB. Unless otherwise specified, we set $W = 5\lambda$, $M = N = L = 2$, $\alpha_s = 10$, $\eta = 1$, $\text{SNR}_t = 20$ dB, and $\text{SNR}_u = 17$ dB in the simulations. We compare the proposed algorithm with the following benchmarks:

- **FPA-nonAO**: BS adopts FPAs with antenna spacing of $\lambda/2$, and the beamforming vectors and the transmit power are optimized once without iteration.
- **FPA-AO**: BS uses FPAs with antenna spacing of $\lambda/2$, and the beamforming vectors and the transmit power are alternatively optimized until convergence.
- **Transmit FAS (FAS-Tx)**: The BS transmits signals using FAS while receiving signals using FPA. The positions of the transmit FAS \mathbf{V} are optimized while the positions of FPA are fixed and spaced by $\lambda/2$.
- **Receive FAS (FAS-Rx)**: The BS transmits signals using FPA while receiving signals using FAS. The positions of the receive FAS \mathbf{U} are optimized while the positions of FPA are fixed and spaced by $\lambda/2$.
- **FAS-Tx+Rx**: The BS uses FAS for both transmitting and receiving signals.

In Fig. 2, we show the communication rate with different numbers of transmit BS antennas. As expected, the communication rate increases with M for all schemes. In particular, when M increases from 2 to 50, the communication rate obtained by using FAS increases by 3 bps/Hz. Note that FAS

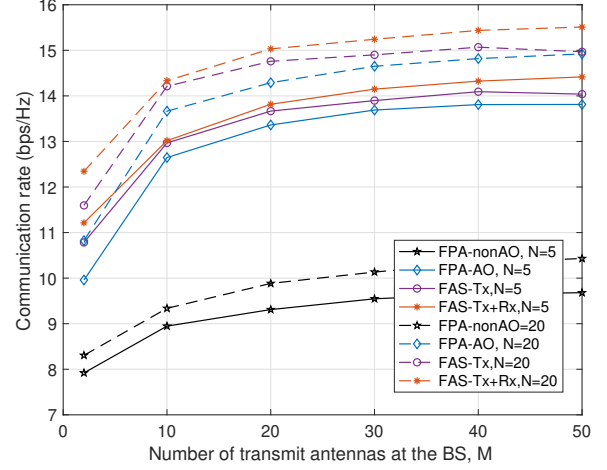


Fig. 2. Communication rate versus the number of transmit BS antennas, M .

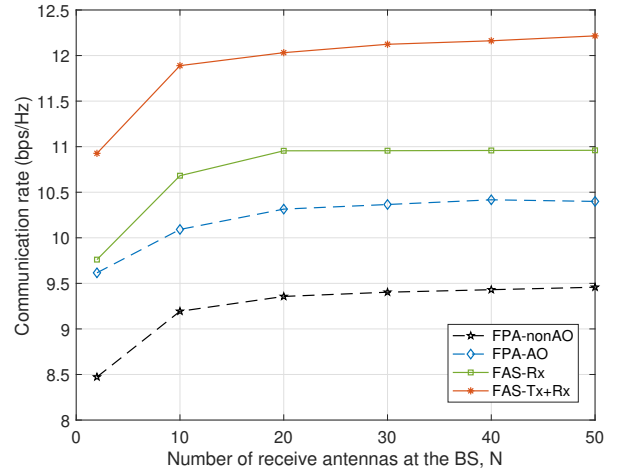


Fig. 3. Communication rate versus the number of receive BS antennas N .

with 20 transmit antennas can outperform the FPA system with 50 transmit antennas when $N = 5$ and $N = 20$. While optimizing only the transmit FAS can significantly enhance the communication rate, updating both the transmit and receive FAS can further improve the communication performance.

Fig. 3 considers how the number of receive BS antennas affects the communication rate. By updating the positions of the receive antennas, the communication rate is increased by 1.5 bps/Hz compared to the FPA when $L = 2$. Optimizing both transmit and receive FAS also further increases the communication rate by 1.25 bps/Hz compared to optimizing only the receive FAS.

In Fig. 4, we verify the relationship between the communication rate and the number of paths. In comparison, updating the transmit FAS has better performance than updating the receive FAS. This is because both the uplink and downlink rates are related to the BS transmitter, but only the BS receiver is independent of the downlink rate. In addition, optimizing

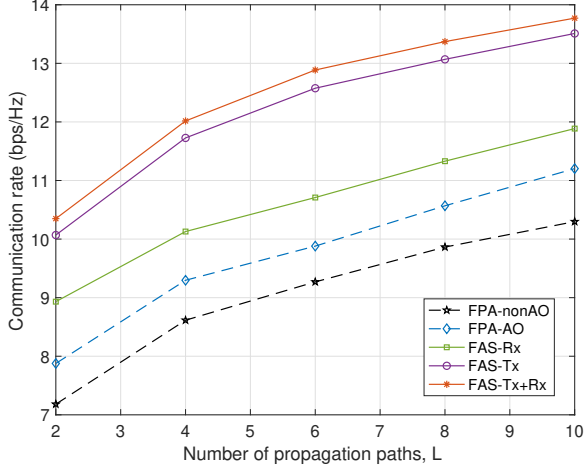


Fig. 4. Communication rate versus the number of propagation paths, L .

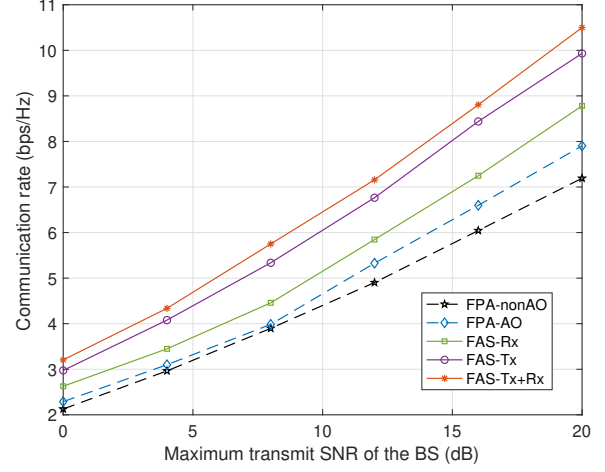


Fig. 6. Communication rate versus the maximum transmit SNR of the BS, $\text{SNR}_t = 10 \log P_t$ dB.

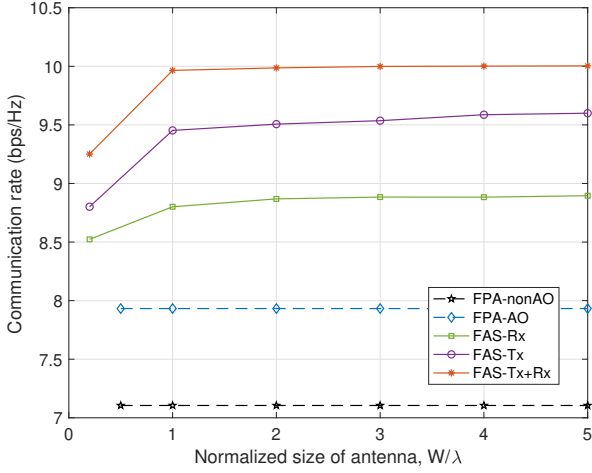


Fig. 5. Communication rate versus the normalized antenna size, W/λ .

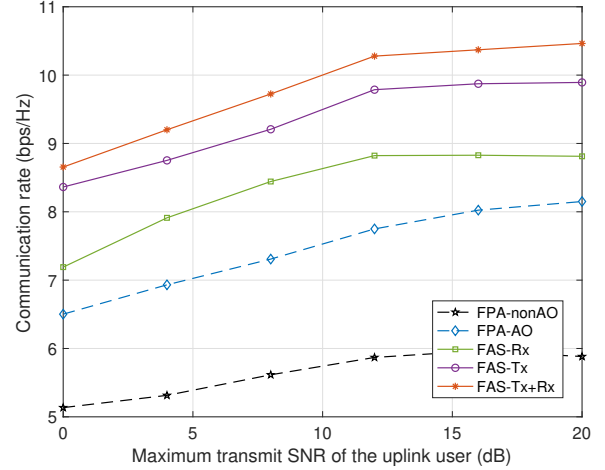


Fig. 7. Communication rate versus the maximum transmit SNR of the uplink user, $\text{SNR}_u = 10 \log P_u$ dB.

both the transmit and receive FAS achieves the highest rate, showing an improvement of 2 bps/Hz over FPA.

In Fig. 5, we analyze how the communication rate changes with the size of FAS. We can see that the communication rate initially increases with the antenna size and then saturates. When the antenna size is small, the spatial DoF obtained by changing the antenna positions is limited, so is the performance. Once the antenna size is large enough, further increases in size no longer increase the communication performance.

Figs. 6 and 7 illustrate the communication rate obtained with different values of the power budgets of the BS and the uplink user, respectively. As expected, the communication rate increases with the power budgets. Compared to increasing the power budget of the uplink user, increasing the power budget of the BS contributes more to the communication rate since the downlink rate is independent of the uplink transmit power. As SNR_t increases from 0 dB to 20 dB, the communication rate obtained by using FAS and FPA increases by 7.5 bps/Hz

and 5.8 bps/Hz, respectively. FAS always provides a 2 bps/Hz improvement compared to FPA as SNR_u increases.

Finally, in Fig. 8, we study the communication rate under different sensing thresholds. As we can see, the communication rate decreases for all schemes when the sensing threshold increases. As η increases, the communication rate obtained by FAS shows more decrease compared to FPA. However, when $\eta = 5$, FAS still outperforms FPA by more than 1 bps/Hz.

VI. CONCLUSION

This paper addressed the problem of maximizing the communication rate under sensing performance and power budget constraints. We first introduced the FP framework to transform the problem into subproblems, each of which could be solved in an iterative manner. In particular, the beamforming vectors were optimized using the MM algorithm, while a closed-form solution of the uplink transmit power was given. In addition,

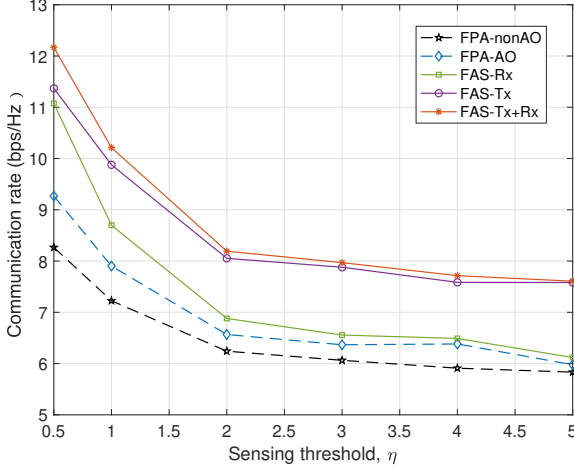


Fig. 8. Communication rate versus the sensing threshold, η .

we provided an SCA-based algorithm to optimize the antenna positions by transforming the corresponding subproblems into convex forms. Simulation results demonstrated that using the proposed algorithm, FAS greatly outperforms FPA in terms of communication rate for ISAC tasks. It is noted that in real-time systems, hardware constraints such as processing latency, response times, and energy consumption should be carefully taken into account. As such, future research should consider these practical limitations and explore the development of low-complexity, real-time-compatible algorithms to enable efficient deployment of FAS in real-world scenarios.

APPENDIX A PROOF OF THEOREM 1

Subscript χ_1 is omitted in this proof for notational brevity. For vectors $\mathbf{a} = [a_1, \dots, a_L]^T$ and $\mathbf{b} = [b_1, \dots, b_M]^T$, we have $\mathbf{a}^T \mathbf{T}^H(\mathbf{V}) \mathbf{b} = \sum_{i=1}^L \sum_{m=1}^M a_i t_i^H(\mathbf{v}_m) b_m$, where $t_i(\mathbf{v}_m) = e^{-j \frac{2\pi}{\lambda} \rho_i(\mathbf{v}_m)}$. Then we have

$$\begin{aligned}
 |\mathbf{a}^T \mathbf{T}(\mathbf{V})^H \mathbf{b}|^2 &= \sum_{i=1}^L \sum_{m=1}^M \sum_{l=1}^L \sum_{n=1}^M a_i t_i^H(\mathbf{v}_m) b_m b_n^H t_l(\mathbf{v}_n) a_l^H \\
 &= \sum_{i=1}^L \sum_{m=1}^M \sum_{l=1}^L \sum_{n=1}^M a_i b_m b_n^H a_l^H e^{j \frac{2\pi}{\lambda} [\rho_i(\mathbf{v}_m) - \rho_l(\mathbf{v}_n)]} \\
 &\stackrel{(a)}{=} \sum_{i=1}^L \sum_{m=1}^M \sum_{l=1}^L \sum_{n=1}^M \text{Re} \left\{ a_i b_m b_n^H a_l^H e^{j \frac{2\pi}{\lambda} [\rho_i(\mathbf{v}_m) - \rho_l(\mathbf{v}_n)]} \right\} \\
 &= \sum_{i=1}^L \sum_{m=1}^M \sum_{l=1}^L \sum_{n=1}^M |a_i b_m b_n^H a_l^H| \cos(f_{i,l}(\mathbf{v}_m, \mathbf{v}_n)) \\
 &\stackrel{(b)}{=} \sum_{i=1}^L \sum_{m=1}^M \sum_{l=1}^L \sum_{n=1}^M |a_i| |b_m| |b_n| |a_l| \cos(f_{i,l}(\mathbf{v}_m, \mathbf{v}_n)) \\
 &= \sum_{i=1}^L \sum_{l=1}^L |a_i| |a_l| \left[\sum_{m=1}^M \sum_{n=1}^M |b_m| |b_n| \cos(f_{i,l}(\mathbf{v}_m, \mathbf{v}_n)) \right], \tag{49}
 \end{aligned}$$

where $f_{i,l}(\mathbf{v}_m, \mathbf{v}_n) = \frac{2\pi}{\lambda} [\rho_i(\mathbf{v}_m) - \rho_l(\mathbf{v}_n)] + \angle(a_i b_m b_n^H a_l^H)$, equation (a) holds since $|\mathbf{a}^T \mathbf{T}(\mathbf{V})^H \mathbf{b}|^2$ is real, and equation (b) holds due to the fact that $|pq| = |p||q| \forall p, q \in \mathbb{C}$. Based on Taylor series expansion, we can construct a concave quadratic surrogate function g for any cosine function as

$$\begin{aligned}
 \cos(\psi) &\stackrel{(c)}{\approx} \cos(\psi_0) - \sin(\psi_0)(\psi - \psi_0) - \frac{1}{2} \cos(\psi_0)(\psi - \psi_0)^2 \\
 &\stackrel{(d)}{\geq} g(\psi|\psi_0) \triangleq \cos(\psi_0) - \sin(\psi_0)(\psi - \psi_0) - \frac{1}{2}(\psi - \psi_0)^2, \tag{50}
 \end{aligned}$$

where (c) is the second order Taylor series expansion of the cosine function, and (d) holds since $\cos(\psi_0) \leq 1$. Denoting $\mathbf{v}_{m,0}$ and $\mathbf{v}_{n,0}$ as the position vectors obtained in the previous iteration and using (50), we know that

$$\begin{aligned}
 \cos(f_{i,l}(\mathbf{v}_m, \mathbf{v}_n)) &\geq g(f_{i,l}(\mathbf{v}_m, \mathbf{v}_n) | f_{i,l}(\mathbf{v}_{m,0}, \mathbf{v}_{n,0})) \\
 &= \cos(f_{i,l,m,n}^0) - \sin(f_{i,l,m,n}^0)(f_{i,l}(\mathbf{v}_m, \mathbf{v}_n) - f_{i,l,m,n}^0) \\
 &\quad - \frac{1}{2}(f_{i,l}(\mathbf{v}_m, \mathbf{v}_n) - f_{i,l,m,n}^0)^2 \\
 &= \cos(f_{i,l,m,n}^0) - \sin(f_{i,l,m,n}^0) \left(\frac{2\pi}{\lambda} [\rho_i(\mathbf{v}_m) - \rho_l(\mathbf{v}_n)] - \tau_{i,l,m,n} \right) \\
 &\quad - \frac{1}{2} \left(\frac{2\pi}{\lambda} [\rho_i(\mathbf{v}_m) - \rho_l(\mathbf{v}_n)] - \tau_{i,l,m,n} \right)^2 \\
 &= \cos(f_{i,l,m,n}^0) - \sin(f_{i,l,m,n}^0) \left(\frac{2\pi}{\lambda} z_{i,l}(\mathbf{v}_m, \mathbf{v}_n) - \tau_{i,l,m,n} \right) \\
 &\quad - \frac{1}{2} \left(\frac{2\pi}{\lambda} z_{i,l}(\mathbf{v}_m, \mathbf{v}_n) - \tau_{i,l,m,n} \right)^2 \\
 &= \frac{-2\pi^2}{\lambda^2} (z_{i,l}(\mathbf{v}_m, \mathbf{v}_n))^2 + \frac{2\pi}{\lambda} (\tau_{i,l,m,n} - \sin(f_{i,l,m,n}^0)) z_{i,l}(\mathbf{v}_m, \mathbf{v}_n) \\
 &\quad + \cos(f_{i,l,m,n}^0) + \sin(f_{i,l,m,n}^0) \tau_{i,l,m,n} - \frac{1}{2} \tau_{i,l,m,n}^2, \tag{51}
 \end{aligned}$$

where $f_{i,l,m,n}^0 = f_{i,l}(\mathbf{v}_{m,0}, \mathbf{v}_{n,0})$, $\tau_{i,l,m,n} = \frac{2\pi}{\lambda} [\rho_i(\mathbf{v}_{m,0}) - \rho_l(\mathbf{v}_{n,0})]$, and $z_{i,l}(\mathbf{v}_m, \mathbf{v}_n) = \rho_i(\mathbf{v}_m) - \rho_l(\mathbf{v}_n) = x_m^t \delta_i + y_m^t \xi_i - x_n^t \delta_l - y_n^t \xi_l$. Then we obtain a lower-bound of (49) as

$$\begin{aligned}
 |\mathbf{a}^T \mathbf{T}(\mathbf{V})^H \mathbf{b}|^2 &\geq \sum_{i=1}^L \sum_{l=1}^L |a_i| |a_l| \left[\sum_{m=1}^M \sum_{n=1}^M |b_m| |b_n| g(f_{i,l}(\mathbf{v}_m, \mathbf{v}_n) | f_{i,l}(\mathbf{v}_{m,0}, \mathbf{v}_{n,0})) \right] \\
 &= \sum_{i=1}^L \sum_{l=1}^L |a_i| |a_l| \left[\mathbf{v}^T \hat{\mathbf{A}}_{i,l} \mathbf{v} + \hat{\mathbf{c}}_{i,l} \mathbf{v} + \hat{d}_{i,l} \right], \tag{52}
 \end{aligned}$$

where

$$\begin{aligned}
\hat{\mathbf{A}}_{i,l} &= \frac{-2\pi^2}{\lambda^2} \begin{bmatrix} \mathbf{A}_{i,l} & \mathbf{C}_{i,l} \\ \mathbf{C}_{i,l}^T & \mathbf{B}_{i,l} \end{bmatrix}, \\
\mathbf{A}_{i,l} &= (\delta_i^2 + \delta_l^2) \text{diag}(\kappa \bar{\mathbf{b}}) - 2\delta_i \delta_l \bar{\mathbf{b}} \bar{\mathbf{b}}^T, \\
\mathbf{B}_{i,l} &= (\xi_i^2 + \xi_l^2) \text{diag}(\kappa \bar{\mathbf{b}}) - 2\xi_i \xi_l \bar{\mathbf{b}} \bar{\mathbf{b}}^T, \\
\mathbf{C}_{i,l} &= (\delta_i \xi_i + \delta_l \xi_l) \text{diag}(\kappa \bar{\mathbf{b}}) - (\delta_i \xi_l + \delta_l \xi_i) \bar{\mathbf{b}} \bar{\mathbf{b}}^T, \\
\bar{\mathbf{b}} &= [|b_1|, \dots, |b_M|]^T, \\
\kappa &= \sum_{m=1}^M |b_m|, \\
\hat{\mathbf{c}}_{i,l} &= \frac{2\pi}{\lambda} [\delta_i \mathbf{r}_{i,l} - \delta_l \mathbf{\Psi}_{i,l}, \xi_i \mathbf{r}_{i,l} - \xi_l \mathbf{\Psi}_{i,l}], \\
\mathbf{r}_{i,l} &= [|b_1| \mathbf{r}_1^{i,l}, \dots, |b_M| \mathbf{r}_M^{i,l}], \\
\mathbf{\Psi}_{i,l} &= [|b_1| \mathbf{\Psi}_1^{i,l}, \dots, |b_M| \mathbf{\Psi}_M^{i,l}], \\
\mathbf{r}_m^{i,l} &= \sum_{n=1}^M |b_n| (\tau_{i,l,m,n} - \sin(f_{i,l,m,n}^0)), \\
\mathbf{\Psi}_n^{i,l} &= \sum_{m=1}^M |b_m| (\tau_{i,l,m,n} - \sin(f_{i,l,m,n}^0)), \\
\hat{d}_{i,l} &= \sum_{m=1}^M \sum_{n=1}^M |b_m| |b_n| \hat{q}_{i,l,m,n}, \\
\hat{q}_{i,l,m,n} &\triangleq \cos(f_{i,l,m,n}^0) + \sin(f_{i,l,m,n}^0) \tau_{i,l,m,n} - \frac{1}{2} \tau_{i,l,m,n}^2.
\end{aligned}$$

Now, denoting $\hat{\mathbf{A}} = \sum_{i=1}^L \sum_{l=1}^L |a_i| |a_l| \hat{\mathbf{A}}_{i,l}$, $\hat{\mathbf{c}} = \sum_{i=1}^L \sum_{l=1}^L |a_i| |a_l| \hat{\mathbf{c}}_{i,l}$, and $\hat{\mathbf{d}} = \sum_{i=1}^L \sum_{l=1}^L |a_i| |a_l| \hat{d}_{i,l}$, (52) can be rewritten as

$$|\mathbf{a}^T \mathbf{T}(\mathbf{V})^H \mathbf{b}|^2 \geq \mathbf{v}^T \hat{\mathbf{A}} \mathbf{v} + \hat{\mathbf{c}} \mathbf{v} + \hat{\mathbf{d}}. \quad (53)$$

Since $\hat{\mathbf{A}}_{i,l}$ is symmetric and $\mathbf{v}^T \hat{\mathbf{A}}_{i,l} \mathbf{v} = \frac{-2\pi^2}{\lambda^2} \sum_{m=1}^M \sum_{n=1}^M |b_m| |b_n| (z_{i,l}(\mathbf{v}_m, \mathbf{v}_n))^2 \leq 0$, $\hat{\mathbf{A}}_{i,l}$ is an NSD matrix, and so is $\hat{\mathbf{A}}$.

Similar to (50), a convex quadratic surrogate function \bar{g} for the cos function can also be derived as

$$\begin{aligned}
\cos(\psi) &\approx \cos(\psi_0) - \sin(\psi_0)(\psi - \psi_0) - \frac{1}{2} \cos(\psi_0)(\psi - \psi_0)^2 \\
&\stackrel{(e)}{\leq} \bar{g}(\psi|\psi_0) \triangleq \cos(\psi_0) - \sin(\psi_0)(\psi - \psi_0) + \frac{1}{2}(\psi - \psi_0)^2, \quad (54)
\end{aligned}$$

where (e) holds due to $\cos(\psi_0) \geq -1$. Therefore, based on

(54), we have

$$\begin{aligned}
\cos(f_{i,l}(\mathbf{v}_m, \mathbf{v}_n)) &\leq \bar{g}(f_{i,l}(\mathbf{v}_m, \mathbf{v}_n) | f_{i,l}(\mathbf{v}_{m,0}, \mathbf{v}_{n,0})) \\
&= \cos(f_{i,l,m,n}^0) - \sin(f_{i,l,m,n}^0)(f_{i,l}(\mathbf{v}_m, \mathbf{v}_n) - f_{i,l,m,n}^0) \\
&\quad + \frac{1}{2}(f_{i,l}(\mathbf{v}_m, \mathbf{v}_n) - f_{i,l,m,n}^0)^2 \\
&= \cos(f_{i,l,m,n}^0) - \sin(f_{i,l,m,n}^0) \left(\frac{2\pi}{\lambda} [\rho_i(\mathbf{v}_m) - \rho_l(\mathbf{v}_n)] - \tau_{i,l,m,n} \right) \\
&\quad + \frac{1}{2} \left(\frac{2\pi}{\lambda} [\rho_i(\mathbf{v}_m) - \rho_l(\mathbf{v}_n)] - \tau_{i,l,m,n} \right)^2 \\
&= \cos(f_{i,l,m,n}^0) - \sin(f_{i,l,m,n}^0) \left(\frac{2\pi}{\lambda} z_{i,l}(\mathbf{v}_m, \mathbf{v}_n) - \tau_{i,l,m,n} \right) \\
&\quad + \frac{1}{2} \left(\frac{2\pi}{\lambda} z_{i,l}(\mathbf{v}_m, \mathbf{v}_n) - \tau_{i,l,m,n} \right)^2 \\
&= \frac{2\pi^2}{\lambda^2} (z_{i,l}(\mathbf{v}_m, \mathbf{v}_n))^2 - \frac{2\pi}{\lambda} (\tau_{i,l,m,n} + \sin(f_{i,l,m,n}^0)) z_{i,l}(\mathbf{v}_m, \mathbf{v}_n) \\
&\quad + \cos(f_{i,l,m,n}^0) + \sin(f_{i,l,m,n}^0) \tau_{i,l,m,n} + \frac{1}{2} \tau_{i,l,m,n}^2, \quad (55)
\end{aligned}$$

where $f_{i,l,m,n}^0$, $\tau_{i,l,m,n}$ and $z_{i,l}(\mathbf{v}_m, \mathbf{v}_n)$ are defined in (51). An upper-bound of (49) can thus be written as

$$\begin{aligned}
&|\mathbf{a}^T \mathbf{T}(\mathbf{V})^H \mathbf{b}|^2 \\
&\leq \sum_{i=1}^L \sum_{l=1}^L |a_i| |a_l| \left[\sum_{m=1}^M \sum_{n=1}^M |b_m| |b_n| \bar{g}(f_{i,l}(\mathbf{v}_m, \mathbf{v}_n) | f_{i,l}(\mathbf{v}_{m,0}, \mathbf{v}_{n,0})) \right] \\
&= \sum_{i=1}^L \sum_{l=1}^L |a_i| |a_l| \left[-\mathbf{v}^T \hat{\mathbf{A}}_{i,l} \mathbf{v} + \bar{\mathbf{c}}_{i,l} \mathbf{v} + \bar{d}_{i,l} \right], \\
&= -\mathbf{v}^T \hat{\mathbf{A}} \mathbf{v} + \bar{\mathbf{c}} \mathbf{v} + \bar{\mathbf{d}}, \quad (56)
\end{aligned}$$

where $\hat{\mathbf{A}}_{i,l}$ is given in (52),

$$\begin{aligned}
\bar{\mathbf{c}} &= \sum_{i=1}^L \sum_{l=1}^L |a_i| |a_l| \bar{\mathbf{c}}_{i,l}, \\
\bar{\mathbf{d}} &= \sum_{i=1}^L \sum_{l=1}^L |a_i| |a_l| \bar{d}_{i,l}, \\
\bar{\mathbf{c}}_{i,l} &= \frac{-2\pi}{\lambda} [\delta_i \mathbf{r}_{i,l} - \delta_l \mathbf{\Psi}_{i,l}, \xi_i \mathbf{r}_{i,l} - \xi_l \mathbf{\Psi}_{i,l}], \\
\mathbf{r}_{i,l} &= [|b_1| \mathbf{r}_1^{i,l}, \dots, |b_M| \mathbf{r}_M^{i,l}], \\
\mathbf{\Psi}_{i,l} &= [|b_1| \mathbf{\Psi}_1^{i,l}, \dots, |b_M| \mathbf{\Psi}_M^{i,l}], \\
\mathbf{r}_m^{i,l} &= \sum_{n=1}^M |b_n| (\tau_{i,l,m,n} + \sin(f_{i,l,m,n}^0)), \\
\mathbf{\Psi}_n^{i,l} &= \sum_{m=1}^M |b_m| (\tau_{i,l,m,n} + \sin(f_{i,l,m,n}^0)), \\
\bar{d}_{i,l} &= \sum_{m=1}^M \sum_{n=1}^M |b_m| |b_n| \bar{q}_{i,l,m,n}, \\
\bar{q}_{i,l,m,n} &= \cos(f_{i,l,m,n}^0) + \sin(f_{i,l,m,n}^0) \tau_{i,l,m,n} + \frac{1}{2} \tau_{i,l,m,n}^2.
\end{aligned}$$

Since $\hat{\mathbf{A}}$ is a NSD matrix as given in (53), $-\mathbf{v}^T \hat{\mathbf{A}} \mathbf{v} + \bar{\mathbf{c}} \mathbf{v} + \bar{\mathbf{d}}$ is a convex quadratic function. This completes the proof.

APPENDIX B
PROOF OF THEOREM 2

In the following, we omit the subscript χ_1 for brevity. Denote $\mathbf{a} = [a_1, \dots, a_L]^T$ and $\mathbf{b} = [b_1, \dots, b_M]^T$. Based on the transmitting steering matrices in Section II-B, we have

$$\begin{aligned} \text{Re}\{\mathbf{a}^T \mathbf{T}(\mathbf{V})^H \mathbf{b}\} &= \text{Re}\left\{\sum_{i=1}^L \sum_{m=1}^M a_i t_i^H(\mathbf{v}_m) b_m\right\} \\ &= \text{Re}\left\{\sum_{i=1}^L \sum_{m=1}^M a_i b_m e^{j\frac{2\pi}{\lambda} \rho_i(\mathbf{v}_m)}\right\} \\ &= \sum_{i=1}^L \sum_{m=1}^M |a_i b_m| \cos\left(\frac{2\pi}{\lambda} \rho_i(\mathbf{v}_m) + \angle a_i b_m\right) \\ &\stackrel{(f)}{=} \sum_{i=1}^L \sum_{m=1}^M |a_i| |b_m| \cos\left(\frac{2\pi}{\lambda} \rho_i(\mathbf{v}_m) + \angle a_i b_m\right) \\ &= \sum_{i=1}^L |a_i| \sum_{m=1}^M |b_m| \cos(\bar{f}_i(\mathbf{v}_m)), \end{aligned} \quad (57)$$

where $\bar{f}_i(\mathbf{v}_m) = \frac{2\pi}{\lambda} \rho_i(\mathbf{v}_m) + \angle(a_i b_m)$ and equation (f) holds for the same reason as equation (b) in (49). Based on the Taylor series expansion in (50), we have

$$\begin{aligned} \cos(\bar{f}_i(\mathbf{v}_m)) &\geq g(\bar{f}_i(\mathbf{v}_m)) |\bar{f}_i(\mathbf{v}_m, 0)| \\ &= \cos(\bar{f}_i(\mathbf{v}_m, 0)) - \sin(\bar{f}_i(\mathbf{v}_m, 0)) (\bar{f}_i(\mathbf{v}_m) - \bar{f}_i(\mathbf{v}_m, 0)) \\ &\quad - \frac{1}{2} (\bar{f}_i(\mathbf{v}_m) - \bar{f}_i(\mathbf{v}_m, 0))^2 \\ &= \cos(\bar{f}_i(\mathbf{v}_m, 0)) - \sin(\bar{f}_i(\mathbf{v}_m, 0)) \left(\frac{2\pi}{\lambda} [\rho_i(\mathbf{v}_m) - \rho_i(\mathbf{v}_m, 0)]\right) \\ &\quad - \frac{1}{2} \left(\frac{2\pi}{\lambda} [\rho_i(\mathbf{v}_m) - \rho_i(\mathbf{v}_m, 0)]\right)^2 \\ &= \frac{-2\pi^2}{\lambda^2} (\rho_i(\mathbf{v}_m))^2 + \frac{2\pi}{\lambda} \left[\frac{2\pi}{\lambda} \rho_i(\mathbf{v}_m, 0) - \sin(\bar{f}_i(\mathbf{v}_m, 0))\right] \rho_i(\mathbf{v}_m) \\ &\quad + \cos(\bar{f}_i(\mathbf{v}_m, 0)) + \frac{2\pi}{\lambda} \sin(\bar{f}_i(\mathbf{v}_m, 0)) \rho_i(\mathbf{v}_m, 0) - \frac{2\pi^2}{\lambda^2} (\rho_i(\mathbf{v}_m, 0))^2, \end{aligned} \quad (58)$$

which gives a lower-bound of (57) as

$$\begin{aligned} \text{Re}\{\mathbf{a}^T \mathbf{T}(\mathbf{V})^H \mathbf{b}\} &\geq \sum_{i=1}^L |a_i| \sum_{m=1}^M |b_m| g(\bar{f}_i(\mathbf{v}_m)) |\bar{f}_i(\mathbf{v}_m, 0)| \\ &= \sum_{i=1}^L |a_i| (\mathbf{v}^T \tilde{\mathbf{A}}_i \mathbf{v} + \tilde{\mathbf{c}}_i \mathbf{v} + \tilde{d}_i) \\ &= \mathbf{v}^T \tilde{\mathbf{A}} \mathbf{v} + \tilde{\mathbf{c}} \mathbf{v} + \tilde{d}, \end{aligned} \quad (59)$$

where $\tilde{\mathbf{A}} = \sum_{i=1}^L |a_i| \tilde{\mathbf{A}}_i$, $\tilde{\mathbf{c}} = \sum_{i=1}^L |a_i| \tilde{\mathbf{c}}_i$, $\tilde{d} = \sum_{i=1}^L |a_i| \tilde{d}_i$,

$$\tilde{\mathbf{A}}_i = \frac{-2\pi^2}{\lambda^2} \begin{bmatrix} \tilde{\mathbf{A}}_i & \tilde{\mathbf{C}}_i \\ \tilde{\mathbf{C}}_i & \tilde{\mathbf{B}}_i \end{bmatrix},$$

$$\tilde{\mathbf{A}}_i = \delta_i^2 \text{diag}(\tilde{\mathbf{b}}), \tilde{\mathbf{B}}_i = \xi_i^2 \text{diag}(\tilde{\mathbf{b}}), \tilde{\mathbf{C}}_i = \delta_i \xi_i \text{diag}(\tilde{\mathbf{b}}),$$

$$\tilde{\mathbf{r}}_m^i = \frac{2\pi}{\lambda} \rho_i(\mathbf{v}_m, 0) - \sin(\bar{f}_i(\mathbf{v}_m, 0)), \tilde{\mathbf{r}}_i = [b_1 |\tilde{\mathbf{r}}_1^i|, \dots, b_M |\tilde{\mathbf{r}}_M^i|],$$

$$\tilde{\mathbf{c}}_i = \frac{2\pi}{\lambda} [\delta_i \tilde{\mathbf{r}}_i, \xi_i \tilde{\mathbf{r}}_i], \tilde{d}_i = \sum_{m=1}^M |b_m| \tilde{\varrho}_{i,m},$$

$$\tilde{\varrho}_{i,m} = \cos(\bar{f}_i(\mathbf{v}_m, 0)) + \frac{2\pi}{\lambda} \sin(\bar{f}_i(\mathbf{v}_m, 0)) \rho_i(\mathbf{v}_m, 0) - \frac{2\pi^2}{\lambda^2} (\rho_i(\mathbf{v}_m, 0))^2,$$

and the definition of $\tilde{\mathbf{b}}$ is given in (52). Since $\mathbf{v}^T \tilde{\mathbf{A}}_i \mathbf{v} = \frac{-2\pi^2}{\lambda^2} \sum_{m=1}^M |b_m| (\rho_i(\mathbf{v}_m))^2 \leq 0$, $\tilde{\mathbf{A}}_i$ is NSD. Therefore, $\tilde{\mathbf{A}} = \sum_{i=1}^L |a_i| \tilde{\mathbf{A}}_i$ is also NSD, which proves Theorem 2.

APPENDIX C
PROOF OF THEOREM 3

For any vectors $\mathbf{a} = [a_1, \dots, a_L]^T$, $\mathbf{b} = [b_1, \dots, b_M]^T$, and $\tilde{\mathbf{a}} = [\tilde{a}_1, \dots, \tilde{a}_{\tilde{L}}]^T$, we have $\mathbf{a}^T \mathbf{T}_\chi^H(\mathbf{V}) \mathbf{b} = \sum_{i=1}^L \sum_{m=1}^M a_i (t_i^\chi(\mathbf{v}_m))^H b_m$ and $\tilde{\mathbf{a}}^T \mathbf{T}_{\tilde{\chi}}^H(\mathbf{V}) \mathbf{b} = \sum_{\tilde{l}=1}^{\tilde{L}} \sum_{n=1}^M \tilde{a}_{\tilde{l}} (t_{\tilde{l}}^{\tilde{\chi}}(\mathbf{v}_n))^H b_n$, where $t_i^\chi(\mathbf{v}_m) = e^{-j\frac{2\pi}{\lambda} \rho_i^\chi(\mathbf{v}_m)}$ and $t_{\tilde{l}}^{\tilde{\chi}}(\mathbf{v}_m) = e^{-j\frac{2\pi}{\lambda} \rho_{\tilde{l}}^{\tilde{\chi}}(\mathbf{v}_m)}$. Then, it is known that

$$\begin{aligned} &\text{Re}\left\{(\mathbf{a}^T \mathbf{T}_\chi^H(\mathbf{V}) \mathbf{b})(\tilde{\mathbf{a}}^T \mathbf{T}_{\tilde{\chi}}^H(\mathbf{V}) \mathbf{b})^H\right\} \\ &= \text{Re}\left\{\sum_{i=1}^L \sum_{m=1}^M \sum_{\tilde{l}=1}^{\tilde{L}} \sum_{n=1}^M a_i (t_i^\chi(\mathbf{v}_m))^H b_m b_n^H t_{\tilde{l}}^{\tilde{\chi}}(\mathbf{v}_n) \tilde{a}_{\tilde{l}}^H\right\} \\ &= \text{Re}\left\{\sum_{i=1}^L \sum_{m=1}^M \sum_{\tilde{l}=1}^{\tilde{L}} \sum_{n=1}^M a_i b_m b_n^H \tilde{a}_{\tilde{l}}^H e^{j\frac{2\pi}{\lambda} [\rho_i^\chi(\mathbf{v}_m) - \rho_{\tilde{l}}^{\tilde{\chi}}(\mathbf{v}_n)]}\right\} \\ &= \sum_{i=1}^L \sum_{m=1}^M \sum_{\tilde{l}=1}^{\tilde{L}} \sum_{n=1}^M \text{Re}\left\{a_i b_m b_n^H \tilde{a}_{\tilde{l}}^H e^{j\frac{2\pi}{\lambda} [\rho_i^\chi(\mathbf{v}_m) - \rho_{\tilde{l}}^{\tilde{\chi}}(\mathbf{v}_n)]}\right\} \\ &= \sum_{i=1}^L \sum_{m=1}^M \sum_{\tilde{l}=1}^{\tilde{L}} \sum_{n=1}^M |a_i b_m b_n \tilde{a}_{\tilde{l}}| \cos(\check{f}_{i,\tilde{l}}(\mathbf{v}_m, \mathbf{v}_n)) \\ &\stackrel{(g)}{=} \sum_{i=1}^L \sum_{m=1}^M \sum_{\tilde{l}=1}^{\tilde{L}} \sum_{n=1}^M |a_i| |b_m| |b_n| |\tilde{a}_{\tilde{l}}| \cos(\check{f}_{i,\tilde{l}}(\mathbf{v}_m, \mathbf{v}_n)) \\ &= \sum_{i=1}^L \sum_{\tilde{l}=1}^{\tilde{L}} |a_i| |\tilde{a}_{\tilde{l}}| \left[\sum_{m=1}^M \sum_{n=1}^M |b_m| |b_n| \cos(\check{f}_{i,\tilde{l}}(\mathbf{v}_m, \mathbf{v}_n))\right], \end{aligned} \quad (60)$$

where $\check{f}_{i,\tilde{l}}(\mathbf{v}_m, \mathbf{v}_n) = \frac{2\pi}{\lambda} [\rho_i^\chi(\mathbf{v}_m) - \rho_{\tilde{l}}^{\tilde{\chi}}(\mathbf{v}_n)] + \angle(a_i b_m b_n^H \tilde{a}_{\tilde{l}}^H)$, and equation (g) holds due to the same reason as equation (b) in (49). According to (54), we have

$$\begin{aligned} \cos(\check{f}_{i,\tilde{l}}(\mathbf{v}_m, \mathbf{v}_n)) &\leq \bar{g}(\check{f}_{i,\tilde{l}}(\mathbf{v}_m, \mathbf{v}_n)) |\check{f}_{i,\tilde{l}}(\mathbf{v}_m, 0, \mathbf{v}_n, 0)| \\ &= \frac{2\pi^2}{\lambda^2} (\check{z}_{i,\tilde{l}}(\mathbf{v}_m, \mathbf{v}_n))^2 - \frac{2\pi}{\lambda} (\check{\tau}_{i,\tilde{l},m,n} + \sin(\check{f}_{i,\tilde{l},m,n}^0)) \check{z}_{i,\tilde{l}}(\mathbf{v}_m, \mathbf{v}_n) \\ &\quad + \cos(\check{f}_{i,\tilde{l},m,n}^0) + \sin(\check{f}_{i,\tilde{l},m,n}^0) \check{\tau}_{i,\tilde{l},m,n} + \frac{1}{2} \check{\tau}_{i,\tilde{l},m,n}^2, \end{aligned} \quad (61)$$

where $\check{f}_{i,\tilde{l},m,n}^0 = \check{f}_{i,\tilde{l}}(\mathbf{v}_m, 0, \mathbf{v}_n, 0)$, $\check{\tau}_{i,\tilde{l},m,n} = \frac{2\pi}{\lambda} [\rho_i^\chi(\mathbf{v}_m, 0) - \rho_{\tilde{l}}^{\tilde{\chi}}(\mathbf{v}_n, 0)]$, and $\check{z}_{i,\tilde{l}}(\mathbf{v}_m, \mathbf{v}_n) = \rho_i^\chi(\mathbf{v}_m) - \rho_{\tilde{l}}^{\tilde{\chi}}(\mathbf{v}_n) = x_m^t \delta_i^\chi + y_m^t \xi_i^\chi - x_n^t \delta_{\tilde{l}}^{\tilde{\chi}} - y_n^t \xi_{\tilde{l}}^{\tilde{\chi}}$.

Although the expressions of (55) and (61) look similar, the construction of the convex surrogate function of $\text{Re}\{(\mathbf{a}^T \mathbf{T}_\chi^H(\mathbf{V}) \mathbf{b})(\tilde{\mathbf{a}}^T \mathbf{T}_{\tilde{\chi}}^H(\mathbf{V}) \mathbf{b})^H\}$ is very different from that of $\text{Re}\{(\mathbf{a}^T \mathbf{T}_\chi^H(\mathbf{V}) \mathbf{b})\}$, since the corresponding angles in $\rho_i^\chi(\mathbf{v}_n)$ are different from those in $\rho_{\tilde{l}}^{\tilde{\chi}}(\mathbf{v}_n)$.

Using (61), an upper-bound of (60) can be found as

$$\begin{aligned} & \text{Re} \left\{ (\mathbf{a}^T \mathbf{T}_\chi^H(\mathbf{V}) \mathbf{b})(\check{\mathbf{a}}^T \mathbf{T}_\chi^H(\mathbf{V}) \check{\mathbf{b}})^H \right\} \\ & \leq \sum_{i=1}^L \sum_{l=1}^{\tilde{L}} |a_i| |\check{a}_l| \left[\sum_{m=1}^M \sum_{n=1}^M |b_m| |\check{b}_n| \bar{g}(\check{f}_{i,l}(\mathbf{v}_m, \mathbf{v}_n)) | \check{f}_{i,l}(\mathbf{v}_{m,0}, \mathbf{v}_{n,0}) \right] \\ & = \sum_{i=1}^L \sum_{l=1}^{\tilde{L}} |a_i| |\check{a}_l| [\mathbf{v}^T \check{\mathbf{A}}_{i,l} \mathbf{v} + \check{\mathbf{c}}_{i,l} \mathbf{v} + \check{d}_{i,l}], \end{aligned} \quad (62)$$

where

$$\begin{aligned} \check{\mathbf{A}}_{i,l} &= \frac{2\pi^2}{\lambda^2} \begin{bmatrix} \check{\mathbf{A}}_{i,l} & \check{\mathbf{C}}_{i,l} \\ \check{\mathbf{C}}_{i,l}^T & \check{\mathbf{B}}_{i,l} \end{bmatrix}, \\ \check{\mathbf{A}}_{i,l} &= ((\delta_i^x)^2 + (\delta_l^x)^2) \text{diag}(\kappa \bar{\mathbf{b}}) - 2\delta_i^x \delta_l^x \bar{\mathbf{b}} \bar{\mathbf{b}}^T, \\ \check{\mathbf{B}}_{i,l} &= ((\xi_i^x)^2 + (\xi_l^x)^2) \text{diag}(\kappa \bar{\mathbf{b}}) - 2\xi_i^x \xi_l^x \bar{\mathbf{b}} \bar{\mathbf{b}}^T, \\ \check{\mathbf{C}}_{i,l} &= (\delta_i^x \xi_l^x + \delta_l^x \xi_i^x) \text{diag}(\kappa \bar{\mathbf{b}}) - (\delta_i^x \xi_l^x + \delta_l^x \xi_i^x) \bar{\mathbf{b}} \bar{\mathbf{b}}^T, \\ \check{\mathbf{c}}_{i,l} &= \frac{-2\pi}{\lambda} [\delta_i^x \check{\mathbf{r}}_{i,l} - \delta_l^x \check{\mathbf{r}}_{i,l}, \xi_i^x \check{\mathbf{r}}_{i,l} - \xi_l^x \check{\mathbf{r}}_{i,l}]^T, \\ \check{\mathbf{r}}_{i,l} &= [b_1 |\check{\mathbf{r}}_1^{i,l}, \dots, |b_M |\check{\mathbf{r}}_M^{i,l}]^T, \\ \check{\mathbf{r}}_{i,l} &= [b_1 |\check{\mathbf{r}}_1^{i,l}, \dots, |b_M |\check{\mathbf{r}}_M^{i,l}]^T, \\ \check{\mathbf{r}}_m^{i,l} &= \sum_{n=1}^M |b_n| (\check{r}_{i,l,m,n} + \sin(\check{f}_{i,l,m,n}^0)), \\ \check{\mathbf{r}}_n^{i,l} &= \sum_{m=1}^M |b_m| (\check{r}_{i,l,m,n} + \sin(\check{f}_{i,l,m,n}^0)), \\ \check{d}_{i,l} &= \sum_{m=1}^M \sum_{n=1}^M |b_m| |\check{b}_n| \check{d}_{i,l,m,n}, \\ \check{d}_{i,l,m,n} &\triangleq \cos(\check{f}_{i,l,m,n}^0) + \sin(\check{f}_{i,l,m,n}^0) \check{r}_{i,l,m,n} + \frac{1}{2} \check{r}_{i,l,m,n}^2, \end{aligned}$$

with κ and $\bar{\mathbf{b}}$ are given in (52).

Defining $\check{\mathbf{A}} = \sum_{i=1}^L \sum_{l=1}^{\tilde{L}} |a_i| |\check{a}_l| \check{\mathbf{A}}_{i,l}$, $\check{\mathbf{c}} = \sum_{i=1}^L \sum_{l=1}^{\tilde{L}} |a_i| |\check{a}_l| \check{\mathbf{c}}_{i,l}$, and $\check{d} = \sum_{i=1}^L \sum_{l=1}^{\tilde{L}} |a_i| |\check{a}_l| \check{d}_{i,l}$, (62) can then be simplified as

$$\text{Re} \left\{ (\mathbf{a}^T \mathbf{T}_\chi^H(\mathbf{V}) \mathbf{b})(\check{\mathbf{a}}^T \mathbf{T}_\chi^H(\mathbf{V}) \check{\mathbf{b}})^H \right\} \leq \mathbf{v}^T \check{\mathbf{A}} \mathbf{v} + \check{\mathbf{c}} \mathbf{v} + \check{d}. \quad (63)$$

Since $\check{\mathbf{A}}_{i,l}$ is in a symmetric form and $\mathbf{v}^T \check{\mathbf{A}}_{i,l} \mathbf{v} = \frac{2\pi^2}{\lambda^2} \sum_{m=1}^M \sum_{n=1}^M |b_m| |\check{b}_n| (\check{z}_{i,l}(\mathbf{v}_m, \mathbf{v}_n))^2 \geq 0$, $\check{\mathbf{A}}_{i,l}$ is a PSD matrix, and so is $\check{\mathbf{A}} = \sum_{i=1}^L \sum_{l=1}^{\tilde{L}} |a_i| |\check{a}_l| \check{\mathbf{A}}_{i,l}$. As a consequence, Theorem 3 is now proven.

APPENDIX D PROOF OF LEMMA 2

Subscript χ_2 is omitted here for brevity. For vectors $\mathbf{a} = [a_1, \dots, a_L]^T$ and $\mathbf{b} = [b_1, \dots, b_N]^T$, we know that

$$\begin{aligned} \text{Re} \{ \mathbf{b}^T \mathbf{R}(\mathbf{U}) \mathbf{a} \} &= \text{Re} \left\{ \sum_{i=1}^L \sum_{m=1}^N a_i r_i(\mathbf{u}_m) b_m \right\} \\ &= \text{Re} \left\{ \sum_{i=1}^L \sum_{m=1}^N a_i b_m e^{-j \frac{2\pi}{\lambda} \rho_i(\mathbf{u}_m)} \right\} \\ &= \sum_{i=1}^L \sum_{m=1}^N |a_i b_m| \cos \left(-\frac{2\pi}{\lambda} \rho_i(\mathbf{u}_m) + \angle a_i b_m \right) \\ &\stackrel{(h)}{=} \sum_{i=1}^L \sum_{m=1}^N |a_i| |b_m| \cos \left(-\frac{2\pi}{\lambda} \rho_i(\mathbf{u}_m) + \angle a_i b_m \right) \\ &= \sum_{i=1}^L |a_i| \sum_{m=1}^N |b_m| \cos(\bar{f}'_i(\mathbf{u}_m)), \end{aligned} \quad (64)$$

where $\bar{f}'_i(\mathbf{u}_m) = \frac{-2\pi}{\lambda} \rho_i(\mathbf{u}_m) + \angle(a_i b_m)$ and equation (h) holds for the same reason as equation (b) in (49).

Based on the Taylor series expansion in (50), a lower bound of (64) is written as

$$\begin{aligned} \cos(\bar{f}'_i(\mathbf{u}_m)) &\geq g(\bar{f}'_i(\mathbf{u}_m)) | \bar{f}'_i(\mathbf{u}_{m,0}) \\ &= \cos(\bar{f}'_i(\mathbf{u}_{m,0})) - \sin(\bar{f}'_i(\mathbf{u}_{m,0})) (\bar{f}'_i(\mathbf{u}_m) - \bar{f}'_i(\mathbf{u}_{m,0})) \\ &\quad - \frac{1}{2} (\bar{f}'_i(\mathbf{u}_m) - \bar{f}'_i(\mathbf{u}_{m,0}))^2 \\ &= \cos(\bar{f}'_i(\mathbf{u}_{m,0})) + \sin(\bar{f}'_i(\mathbf{u}_{m,0})) \left(\frac{2\pi}{\lambda} [\rho_i(\mathbf{u}_m) - \rho_i(\mathbf{u}_{m,0})] \right) \\ &\quad - \frac{1}{2} \left(\frac{2\pi}{\lambda} [\rho_i(\mathbf{u}_m) - \rho_i(\mathbf{u}_{m,0})] \right)^2 \\ &= \frac{-2\pi^2}{\lambda^2} (\rho_i(\mathbf{u}_m))^2 + \frac{2\pi}{\lambda} \left[\frac{2\pi}{\lambda} \rho_i(\mathbf{u}_{m,0}) + \sin(\bar{f}'_i(\mathbf{u}_{m,0})) \right] \rho_i(\mathbf{u}_m) \\ &\quad + \cos(\bar{f}'_i(\mathbf{u}_{m,0})) - \frac{2\pi}{\lambda} \sin(\bar{f}'_i(\mathbf{u}_{m,0})) \rho_i(\mathbf{u}_{m,0}) - \frac{2\pi^2}{\lambda^2} (\rho_i(\mathbf{u}_{m,0}))^2. \end{aligned} \quad (65)$$

Note that the Taylor series expansion of (64) is different from that of (57) due to the negative term in $\bar{f}'_i(\mathbf{u}_m)$. Thus, the concave quadratic surrogate function cannot be constructed directly from Theorem 2. A concave quadratic surrogate function of $\text{Re}\{\mathbf{b}^T \mathbf{R}(\mathbf{U}) \mathbf{a}\}$ can be obtained using (65) as

$$\begin{aligned} \text{Re} \{ \mathbf{b}^T \mathbf{R}(\mathbf{U}) \mathbf{a} \} &\geq \sum_{i=1}^L |a_i| \sum_{m=1}^N |b_m| g(\bar{f}'_i(\mathbf{u}_m)) | \bar{f}'_i(\mathbf{u}_{m,0}) \\ &= \sum_{i=1}^L |a_i| (\mathbf{u}^T \tilde{\mathbf{\Omega}}_i \mathbf{u} + \tilde{\mathbf{p}}_i \mathbf{u} + \tilde{q}_i) \\ &= \mathbf{u}^T \tilde{\mathbf{\Omega}} \mathbf{u} + \tilde{\mathbf{p}} \mathbf{u} + \tilde{q}, \end{aligned} \quad (66)$$

where $\tilde{\Omega} = \sum_{i=1}^L |a_i| \tilde{\Omega}_i$, $\tilde{\mathbf{p}} = \sum_{i=1}^L |a_i| \tilde{\mathbf{p}}_i$, $\tilde{\mathbf{q}} = \sum_{i=1}^L |a_i| \tilde{\mathbf{q}}_i$,

$$\tilde{\Omega}_i = \frac{-2\pi^2}{\lambda^2} \begin{bmatrix} \tilde{\mathbf{A}}'_i & \tilde{\mathbf{C}}'_i \\ \tilde{\mathbf{C}}'_i & \tilde{\mathbf{B}}'_i \end{bmatrix},$$

$$\tilde{\mathbf{A}}'_i = \delta_i^2 \text{diag}(\hat{\mathbf{b}}), \tilde{\mathbf{B}}'_i = \xi_i^2 \text{diag}(\hat{\mathbf{b}}), \tilde{\mathbf{C}}'_i = \delta_i \xi_i \text{diag}(\hat{\mathbf{b}}),$$

$$\hat{\mathbf{b}} \triangleq [|b_1|, \dots, |b_N|]^T,$$

$$\tilde{\mathbf{p}}_i = \frac{2\pi}{\lambda} [\delta_i \tilde{\epsilon}_i, \xi_i \tilde{\epsilon}_i]^T, \tilde{\mathbf{q}}_i = \sum_{m=1}^M |b_m| \tilde{\mathbf{q}}'_{i,m},$$

$$\tilde{\epsilon}_i = [|b_1| \tilde{\epsilon}_1^i, \dots, |b_N| \tilde{\epsilon}_N^i]^T, \tilde{\epsilon}_m^i = \frac{2\pi}{\lambda} \rho_i(\mathbf{u}_{m,0}) + \sin(\tilde{f}'_i(\mathbf{u}_{m,0})),$$

$$\tilde{\mathbf{q}}'_{i,m} = \cos(\tilde{f}'_i(\mathbf{u}_{m,0})) - \frac{2\pi}{\lambda} \sin(\tilde{f}'_i(\mathbf{u}_{m,0})) \rho_i(\mathbf{u}_{m,0}) - \frac{2\pi^2}{\lambda^2} (\rho_i(\mathbf{u}_{m,0}))^2,$$

Since $\tilde{\Omega}_i$ is symmetric and $\mathbf{u}^T \tilde{\Omega}_i \mathbf{u} = \frac{-2\pi^2}{\lambda^2} \sum_{m=1}^N |b_m| (\rho_i(\mathbf{u}_m))^2 \leq 0$, $\tilde{\Omega}_i$ is an NSD matrix, and so is $\tilde{\Omega}$. Lemma 2 is thus proven.

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