

1     **Recent Progress for Hydrogen Production from Ammonia and Hydrous Hydrazine**  
2                     **Decomposition: A Review on Heterogeneous Catalysts**

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16  
17     **Abstract**

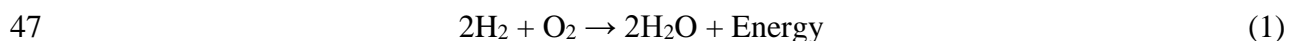
18     In response to the growing trend of greenhouse gas emissions from the production and use of  
19     conventional fuels, CO<sub>x</sub> free hydrogen generation is introduced as an alternative and efficient  
20     energy carrier. Due to hydrogen’s storage challenges, is more efficient to be produced *on-site*  
21     by other chemical compounds for fuel cell applications. This work outlines the production of  
22     hydrogen (H<sub>2</sub>) from ammonia (NH<sub>3</sub>) and hydrous hydrazine (N<sub>2</sub>H<sub>4</sub>.H<sub>2</sub>O) catalytic  
23     decomposition. Both substances are giving nitrogen (N<sub>2</sub>) as a by-product, which is not toxic.  
24     Moreover, heterogeneous catalysts that were studied through the years are presented. Lastly, a  
25     reactoristic view of the ammonia decomposition is provided with different reactors such as  
26     catalytic membrane reactors (CMRs), fixed-bed reactors (FBRs) and micro-reactors (MRs) for  
27     the evaluation of their performance.

28     Keywords: Ammonia, Hydrous Hydrazine, Hydrogen, Catalysts, Reactors

## 32 1 Introduction

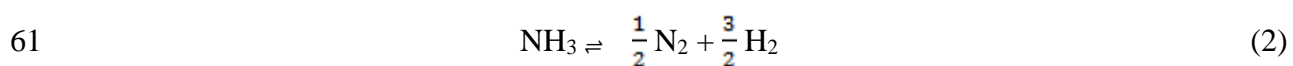
33 Environmental concerns are increasing as the extensive use of fossil fuels in the energy sector  
34 is the biggest contributor to climate change. Fossil fuels undergo the process of combustion to  
35 release their energy content, polluting the atmosphere with emissions of greenhouse gases  
36 (GHGs) and harmful substances. These resources are non-renewable and are not evenly  
37 distributed around the world [1]. There is an increasing urge in recent years to find and adopt  
38 alternative emission-free energy sources in hope to stabilise the negative impacts conventional  
39 fuels have created in the environment. Hydrogen (H<sub>2</sub>) is preferred as an energy carrier due to  
40 its zero emissions during combustion and its generation from various paths such as non-  
41 renewable sources, biomass and water electrolysis [2].

42 Hydrogen can be produced by either from fossil fuels, capturing carbon emissions or renewable  
43 resources. Depending on the material, H<sub>2</sub> can be classified as grey, blue, and green respectively.  
44 Two of the common methods to produce H<sub>2</sub> is steam methane reforming and water splitting  
45 reactions such as water electrolysis [3–6]. Fuel cells then can be used to convert H<sub>2</sub> into power  
46 through the electrochemical reaction that follows (Eq. 1):



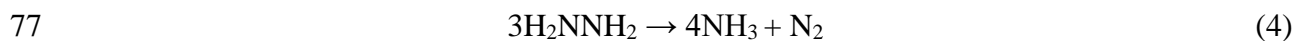
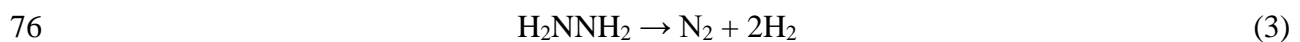
48 Eq. 1 shows H<sub>2</sub> reaction with oxygen to produce water and energy in the form of electricity or  
49 heat as the inverse reaction of electrolysis. Fuel cells are very promising and are already used  
50 in various stationary and mobile applications such as back-up power supplies, road vehicles,  
51 as well as rockets and space shuttles. The main concept revolves around generating green  
52 energy which is considered revolutionary [7]. However, its storage and transportation problems  
53 have not yet reached an applicable level for further industrial use.

54 Ammonia (NH<sub>3</sub>), among other H<sub>2</sub> energy sources, is a promising alternative. It is mainly  
55 produced from the decomposition of urea and other nitrogen compounds during wastewater  
56 treatment processes or from the microbial decomposition of organic substances containing  
57 nitrogen [8]. It possesses high H<sub>2</sub> content (17.8 wt %) and a large energy density (3000 Wh/kg).  
58 It has greater volumetric hydrogen density than liquid H<sub>2</sub> (121 kg H<sub>2</sub>/m<sup>3</sup>) and can be liquefied  
59 and stored at room temperature facilitating transportation and storage [9–12]. Furthermore, the  
60 decomposition of ammonia is CO<sub>x</sub>-free producing only H<sub>2</sub> and nitrogen (N<sub>2</sub>) (Eq. 2) [13].



62 Ramsay and Young [14] were the first to study the temperature at which ammonia  
63 decomposition takes place and the influence of the vessel or tube material that contains the gas  
64 in the early 1880s. Then at the beginning of the 20<sup>th</sup> century Perman and Atkinson [15] studied  
65 both the effect of temperature and pressure on the rate of decomposition as well as the catalytic  
66 activity of Hg, Fe, and Pt.

67 Hydrous hydrazine (N<sub>2</sub>H<sub>4</sub>·H<sub>2</sub>O) has also been proposed as a promising candidate for H<sub>2</sub>  
68 generation. It can be produced by the Raschig process that involves the ammonolysis of  
69 hypochlorite to hydrazine and ammonia or the oxidation of anhydrous ammonia by chlorine  
70 [16]. Hydrous hydrazine has a high hydrogen content (8.0 wt %) and due to its carbon-free  
71 content, the generation of H<sub>2</sub> has zero emissions [17–20]. The products from hydrazine  
72 decomposition are H<sub>2</sub> and N<sub>2</sub>; however, an undesirable side reaction of incomplete  
73 decomposition may occur producing ammonia, which must be avoided because it reduces the  
74 efficiency of the H<sub>2</sub> generation process. The two reaction pathways for hydrazine  
75 decomposition are depicted in Eqs. (3-4) [21].



78 This review will highlight H<sub>2</sub> storage challenges and the generation of H<sub>2</sub> from ammonia and  
79 hydrous hydrazine. Moreover, the heterogeneous catalysts for the decomposition of the  
80 substances mentioned above and the structural properties of the catalysts, will be addressed.  
81 Furthermore, different types of reactors that have been applied for the ammonia decomposition,  
82 will be covered to provide an overview of the most innovative and efficient future systems.  
83 Regarding hydrous hydrazine, there are not many studies in the development and design of  
84 reactors and therefore, reactor set-ups will be not discussed.

85

## 86 **2 Hydrogen Storage Challenges**

87 Although H<sub>2</sub> offers an attractive and promising solution as an alternative energy carrier, its  
88 storage and transportation are one of the main technical barriers preventing H<sub>2</sub> for wider  
89 applications. This is due to hydrogen's very low density of 0.089 kg/m<sup>3</sup> at 0 °C and 1 bar. At  
90 ambient temperatures and 1 atm pressure, 1 kg of H<sub>2</sub> occupies 11 m<sup>3</sup>, which results in a large  
91 volume required for storage. Nonetheless, H<sub>2</sub> is extremely flammable with a flame speed nearly

92 an order of magnitude higher than gasoline when mixed with air, therefore, its safety issues  
93 must be resolved [22].

94 Due to the lack of appropriate infrastructure for storage, transportation and distribution of H<sub>2</sub>,  
95 new methods must be found to store it safely. For large scale and long-term storage, different  
96 underground storage sites were proposed such as salt caverns, aquifer formations or depleted  
97 oil and gas fields. Salt caverns are currently the most favorable method. No in-situ reactions  
98 either with microorganisms or any chemical elements occurred so far and the leakage rates are  
99 very low because salt caverns exhibit the required tightness. In contrast with aquifer formations  
100 or depleted oil and gas fields that occur naturally, salt caverns need to be developed in an  
101 already existing underground salt formations, so not all regions have the necessary geological  
102 characteristics [23].

103 Moreover, it is necessary to increase the volumetric energy (density) of H<sub>2</sub> which can happen  
104 either by liquefying it or by compressing it. Pressurised tanks can take the form of cylindrical  
105 or spherical vessels or bottles, and while raising the pressure, gaseous H<sub>2</sub> density increases  
106 achieving higher storage density. These are currently used in stationary applications mainly to  
107 store hydrogen in hydrogen refuelling stations [24]. Their cost may differ from the material  
108 used and the pressure applied in the tank. On the other hand, cryogenic tanks store liquefied  
109 hydrogen at -253 °C (atmospheric pressure) because the liquefaction process increases H<sub>2</sub>  
110 volumetric density drastically. These are not designed to withstand high pressures inside, hence  
111 they must be isolated to reduce as much as possible heat transfer. However, compressing  
112 requires high pressures and liquefying needs extremely low temperatures such as -253 °C that  
113 can only be achieved with multiple heat exchangers and a combination of multiple cooling  
114 cycles [25].

115 New technologies such as metal hydrides and carbon nanotubes are gaining attention for their  
116 H<sub>2</sub> storage properties. Metal hydrides can store H<sub>2</sub> due to their large storage capacity at ambient  
117 pressure and temperature. Hydrogen reacts with metals which have the ability to absorb and  
118 desorb it by breaking or bonding the chemical bonds making them an efficient form of  
119 hydrogen storage [26]. Adsorption of H<sub>2</sub> in carbon nanostructures is an attractive solution for  
120 hydrogen storage due to the high surface area of carbon. There are a variety of carbon materials,  
121 such as single walled carbon nanotubes (SWCNTs), multiwalled carbon nanotubes (MWCNTs)  
122 and carbon nanofibers (CNFs). However due to some controversial results that were obtained  
123 from some studies regarding the H<sub>2</sub> adsorption measurements, much research is still needed for

124 their efficient usage [27]. For example, in the late 1990s, Dillon et al. [28] suggested that  
125 SWCNTs have a very high H<sub>2</sub> uptake up to 5-10 %. Moreover, Chambers et al. [29] published  
126 an even more extraordinary result. It was claimed that the hydrogen storage capacity of graphite  
127 nanofibers (GNFs) materials was up to 67.6 %. Both of these results were questionable thus  
128 research groups [30–32] tried to reproduce and validate the results without success since the  
129 capacity of the materials was very much lower.

130

### 131 **3 Hydrogen Production Routes**

132 Various raw materials can be utilised to produce H<sub>2</sub> following different production routes.  
133 Given the raw material, H<sub>2</sub> can be colour coded as black, grey, blue or green.

134 In spite of the growing number of studies focusing on renewable hydrogen production, fossil  
135 fuel-based hydrogen generation is still being examined. Black or brown H<sub>2</sub> is produced from  
136 coal through the process of gasification. It is considered a very environmentally damaging  
137 method as carbon dioxide and carbon monoxide are also generated and emitted in the  
138 atmosphere. Liu et al. [33] investigated the gasification mechanism and developed a coal  
139 supercritical water gasification reaction kinetic model taking into consideration the migration  
140 mechanism of nitrogen and sulfur. The model could not only predict the generation of  
141 hydrogen, carbon monoxide and carbon dioxide but ammonia and hydrogen sulfide as well,  
142 proving the interaction between hydrocarbon gas and the gasification products of nitrogen and  
143 sulfur.

144 H<sub>2</sub> is labelled grey when extracted from natural gas via steam-methane reforming. It is the most  
145 common form nowadays with over 95 % of the global hydrogen production coming from  
146 reforming of conventional fuels and around 50 % of that is generated from steam reforming of  
147 natural gas [4]. Steam methane reforming (SMR) is an endothermic reaction (600-700 °C) and  
148 the catalysts mostly used for this reaction are nickel-based. Ngo et al. [34] utilised a SMR unit  
149 with a furnace and a reactor, where the furnace produces heat via the natural gas reaction with  
150 oxygen and the reactor consumes heat and generates H<sub>2</sub>. Another study conducted by Cho et  
151 al. [35] used facility-level data to examine the pollutant emissions which may differ from the  
152 theoretical estimates due to various process conditions and types of pollution controlled  
153 equipment. Direct emissions from 33 facilities used were 9.35 kg CO<sub>2</sub>/kg H<sub>2</sub> and increased up

154 to 11.2 kg CO<sub>2</sub>/kg H<sub>2</sub> when the full cycle of H<sub>2</sub> production was included. Increasing 10 % in  
155 hydrogen production efficiency the global warming impact can be reduced up to 11.1 %.

156 Blue H<sub>2</sub> is produced from fossil fuels like black and grey H<sub>2</sub> but the carbon generated from the  
157 process is captured. It can be described with the term carbon neutral but low-carbon H<sub>2</sub> would  
158 be a more appropriate term since not all carbon emissions are captured. Even though CO<sub>2</sub> can  
159 be captured by absorbents or amine solvents, it must be stored after, which is costly. Therefore  
160 Khan et al. [36] explored the possibility to use the carbon captured by converting into formic  
161 acid by the electrode-reduction. An amine-based CO<sub>2</sub> capture unit was utilised with 90 %  
162 capture efficiency. The carbon could either be stored or utilised. It was concluded that by  
163 utilising it instead of storing it, is more cost-effective and is a promising approach for further  
164 future work.

165 Lastly, green H<sub>2</sub> uses renewable sources such as biomass, geothermal, wind and solar energy  
166 [37]. Biomass feedstock such as agricultural crop residues, food and municipal waste can  
167 produce hydrogen carrier compounds through the process of fermentation, hydrolysis, or  
168 oxidation. Formic acid, an organic hydrogen carrier, is considered as one of the main products  
169 derived from biomass. The catalytic decomposition of formic acid is well investigated because  
170 of its properties as an excellent hydrogen source. Hafeez and Sanchez et al. [38] utilised a Pd/C  
171 catalyst for the decomposition of formic acid in a packed bed microreactor. The validation of  
172 experimental data was confirmed by the development of a CFD model. Moreover, the  
173 deactivation of the catalyst was accurately depicted by the model promoting the use of the  
174 model to predict the formic acid decomposition. Another study by Hafeez et al. [39]  
175 investigated the use of a 2%Pd<sub>6</sub>Zn<sub>4</sub> catalyst in a batch reactor for the decomposition of formic  
176 acid and a process-simulation model gave a good validation of the experimental data. The  
177 catalyst was studied in a temperature range of 30-60 °C and with different concentrations (0.1-  
178 0.5 M), where in both cases no loss of activity was observed. The dehydrogenation of hydrogen  
179 carrier compounds with zero CO<sub>2</sub> emissions is an alternative solution to formic acid and will  
180 be discussed later. Another common method used to obtain green H<sub>2</sub> is water splitting reactions  
181 such as electrolysis of water. Water reacts at the cell's anode and under the influence of current  
182 it decomposes and produces O<sub>2</sub> at the anode of the cell and finally H<sub>2</sub> at the cathode [40].

183

184 Apart from these, H<sub>2</sub> can be classified to turquoise, pink, yellow and white which are not  
185 commonly used. Turquoise refers to H<sub>2</sub> produced from methane pyrolysis with solid carbon as  
186 a by-product. Even though methane pyrolysis is not a sustainable process since natural gas  
187 reserves are depleting, it can provide a temporary solution until renewable technologies are  
188 fully developed. The process begins with the cracking of methane to H<sub>2</sub> and solid carbon, then  
189 the removal of the carbon from the stream and lastly, the purification of the gas stream. High  
190 temperatures are needed for methane pyrolysis, up to 1000 °C for non-catalytic systems.  
191 Suitable catalysts such as nickel, iron, and carbon have been extensively studied and the  
192 decomposition of methane can be triggered at lower temperatures (500-800 °C) [41].

193 Pink (or purple) and yellow H<sub>2</sub> are both produced through electrolysis using nuclear power and  
194 solar power respectively [42]. The difference from conventional electrolysis to nuclear high  
195 temperature electrolysis (HTE), is that the later uses heat from nuclear power plants to  
196 moderate electricity consumed for electrolysis. In general, nuclear HTE occurs at 800-1000 °C  
197 and an yttria-stabilised zirconia is used as an electrolyte [43]. A solar-based electrolysis  
198 consists of a concentrating collector, a heat engine, an electrical generator, and electrolyser. A  
199 part of the absorbed solar radiation is converted to mechanical work and then the electrical  
200 generator transforms it to electrical power. Then, the generated electricity is used to electrolyse  
201 water and produce H<sub>2</sub> and O<sub>2</sub> [44].

202 White H<sub>2</sub> refers to the by-product obtained from industrial processes such as catalytic  
203 thermochemical splitting of water, or it may be referred as its natural occurring form. The  
204 thermochemical splitting occurs without intermediate step and is based on the use of  
205 concentrated solar energy. This pathway may further reduce economic and environmental costs  
206 [45].

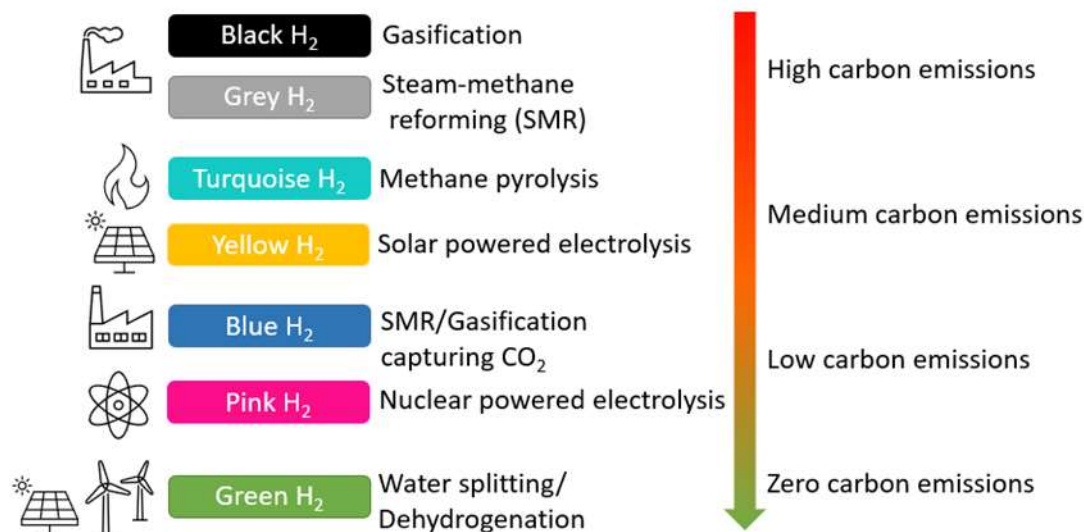
207 Potential applications of H<sub>2</sub> after its production are its use as an industrial feedstock, power  
208 generation, stationary and transportation [46]. Fig. 1 summarises the H<sub>2</sub> colour spectrum  
209 according to the feedstock and production used.

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211

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214 Fig. 1. Hydrogen colour spectrum.

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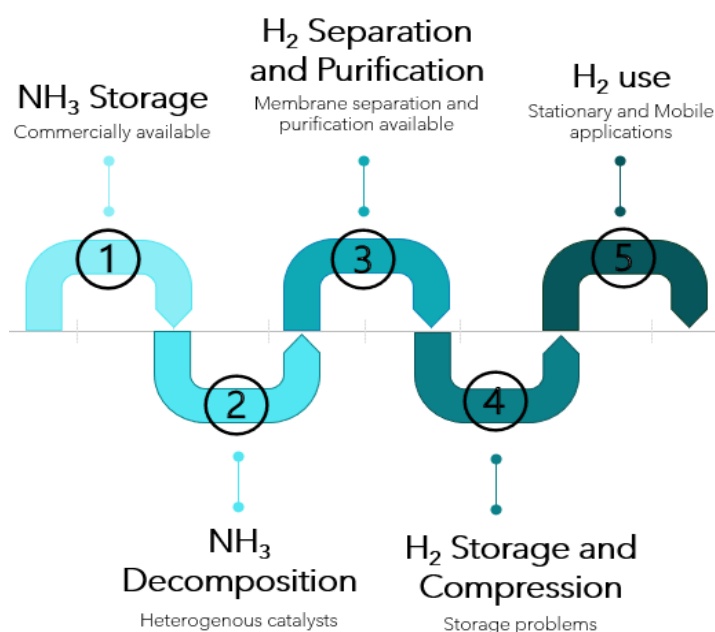
## 216 **4 Ammonia Decomposition as a sustainable hydrogen production method**

### 217 **4.1 Heterogeneous Catalysis of Ammonia Decomposition**

218 Heterogeneous catalysis can be described as the catalysis whereas the phase of the catalyst is  
 219 different from the phase of the reactants/products. Thus, heterogeneous catalysts are, mostly,  
 220 in the solid state while the reactant mixture is either liquid or gas, in contrast with homogeneous  
 221 catalysts that exist in the same phase with the mixture. Heterogeneous catalysts have the ability  
 222 to regenerate, separate easily from the products, shaped into different geometries and give high  
 223 rates [47]. Table 1 summarises the most effective heterogeneous catalysts utilized for the  
 224 decomposition of ammonia.



225 Since the 19<sup>th</sup> century, ammonia decomposition has been investigated mostly to understand the  
 226 ammonia synthesis with the presence or absence of catalysts. Over the last decade, the catalytic  
 227 decomposition of ammonia has gained a lot of attention and catalysts such as platinum (Pt)  
 228 [48], palladium (Pd) [49], ruthenium (Ru) [50] and, rhodium (Rh) [51] that were known to  
 229 catalyse ammonia synthesis have been used in different experiments [52]. Ru was found to be  
 230 the most active and studied catalyst as there is a plethora of studies according to Ru-based  
 231 catalysts [53–57]. Unfortunately, the large scale of application of Ru catalysts is not cost  
 232 effective and their limited availability leads to the necessary development of cheaper catalytic  
 233 systems with the same efficacy. The production steps of H<sub>2</sub> by ammonia are depicted in Fig. 2.



234 Fig. 2. Production steps of hydrogen by ammonia [12].

235 Ni metal particles were used as catalysts with MgAl<sub>2</sub>O<sub>4</sub> as supports by Qiu et al. [58] for  
 236 investigation of the support effect on the catalytic decomposition of ammonia. From the  
 237 catalysts tested Ni/MgAl<sub>2</sub>O<sub>4</sub> – LDH, developed by hydrothermal synthesis, had the best  
 238 catalytic activity with 88.7 % NH<sub>3</sub> conversion and a H<sub>2</sub> production rate of 1782.6 mmol g<sub>cat</sub><sup>-1</sup>  
 239 h<sup>-1</sup> at 600 °C with a stable performance for a period of 30 h. Ni/MgAl<sub>2</sub>O<sub>4</sub> – LDH catalyst had  
 240 the highest surface area (148.3 m<sup>2</sup>/g) and therefore it resulted in high Ni dispersion (29.6 %)   
 241 enhancing the NH<sub>3</sub> conversion and weakening the H<sub>2</sub> poisoning. Ni/MgAl<sub>2</sub>O<sub>4</sub> – LDH catalyst  
 242 was further examined for its stability at a temperature range of 550-650 °C for 24 h and the  
 243 results showed that the catalyst was highly stable due to the strong metal-support interactions.

244 It was concluded that this catalyst with high stability, activity, and low cost it is essential to be  
245 developed more and used in upscale application for H<sub>2</sub> generation.

246 Cobalt particles supported on carbon doped with nitrogen were prepared via pyrolysis of ZIF-  
247 67 at a range of temperatures (Co/NC-X, X = 500, 600, 700 and 800 °C) by Li et al. [59]. The  
248 synthesis process of the catalysts resulted in an evenly dispersion of the Co particles hindering  
249 their aggregation. At temperatures below 300 °C the catalysts were inactive. While increasing  
250 the temperature the conversion of ammonia increased and the best catalytic activity was  
251 obtained by Co/NC-600 with an NH<sub>3</sub> conversion of 80 % and H<sub>2</sub> production rate of 26.8 mmol  
252 H<sub>2</sub> g<sub>cat</sub><sup>-1</sup> min<sup>-1</sup> at 500 °C and hardly decreased even after 72 h. The bond strength between the  
253 metal and nitrogen, according to previous studies, plays a key role in the decomposition of  
254 ammonia. If the bond is either too weak or too strong it affects the adsorption of NH<sub>3</sub> and the  
255 desorption of the intermediate products resulting in a low catalytic activity. Thus, medium  
256 metal-nitrogen bond strength is required for this reaction and from further investigation it was  
257 found that the Co-N bond energy of Co/NC-600 catalyst is in the middle range and thus acting  
258 beneficial for the reaction.

259 Ru particles supported on SmCeO<sub>x</sub> were investigated by Tang et al. [60] for evaluation of the  
260 effect of the Sm doping to the catalysts. At 400 °C, the Ru/SmCeO<sub>x</sub> catalyst, with 1.4 nm  
261 average particle size, obtained a conversion rate of 74.9 % corresponding to a H<sub>2</sub> production  
262 rate of 161.1 mmol g<sub>Ru</sub><sup>-1</sup> min<sup>-1</sup>, much higher than other supports with Ru particles tested for  
263 this catalytic reaction. Characterisation techniques were used to study the properties and  
264 structure of the Ru/SmCeO<sub>x</sub> catalyst. The high activity was attributed to the doping of Sm that  
265 formed in plenty of oxygen vacancies which have strong interaction with Ru resulting in a high  
266 Ru dispersion.

267 A series of Co<sub>3</sub>O<sub>4</sub> catalysts supported on barium hexaaluminate (BHA) with various mass  
268 loadings of Co (XCo/BHA, X = 10 %, 20 %, 30 %, 35 % and 40 %) and 0.5 g BHA were  
269 prepared by Li et al. [61]. BHA alone was inactive and with an increase of Co loading the  
270 activity also increased. The 35Co/BHA catalyst demonstrated the highest catalytic activity  
271 among the others with a conversion rate of 87.2 % at 500 °C and a H<sub>2</sub> production rate of 29.2  
272 mmol H<sub>2</sub> g<sub>cat</sub><sup>-1</sup> min<sup>-1</sup>. After 200 h the conversion rate was at 85 % indicating the catalysts great  
273 stability.

274 Ru-based catalysts supported on reduced graphene oxide were developed by Pinzón et al. [62]  
275 for hydrogen generation by ammonia decomposition. The effect of the Ru loading as well as

276 the effect of the amount of the support material were examined. With a content of Ru up to 2.5  
277 wt %, an increase in the catalytic activity was noticed (92 %), while Ru loading higher than 2.5  
278 wt % resulted in agglomeration decreasing the number of active sites and therefore the  
279 ammonia conversion. With the addition of the pre-reducing agent the catalytic activity  
280 increased. The optimal catalytic activity was observed from 2.5Ru/10C-rGO catalyst with a  
281 conversion of 96 % and H<sub>2</sub> production rate of 349.7 mmol H<sub>2</sub> g<sub>Ru</sub><sup>-1</sup> min<sup>-1</sup>. After 60 h of reaction  
282 the catalyst did not show any significant change in its performance.

283 In an attempt to imitate the activity of the Ru catalysts, Kirste et al. [63] developed alloys of  
284 different unsupported bimetallic catalysts (CoRe<sub>1.6</sub>, Ni<sub>2</sub>Mo<sub>3</sub>N and Co<sub>3</sub>Mo<sub>3</sub>N) for the on-  
285 demand production of H<sub>2</sub> via ammonia decomposition. In parallel, 7 wt % Ru/CNTs catalytic  
286 particles were also synthesized to compare the catalytic activities. CoRe<sub>1.6</sub> obtained a similar  
287 activity with Ru/CNTs due to the alloy synergistic effect. The catalyst was pre-reduced at a  
288 temperature range of 400-600 °C, which had a major impact on the catalytic performance with  
289 an increase of the temperature. At 500 °C reaction temperature and 600 °C reduction  
290 temperature, NH<sub>3</sub> conversion was above 90 % and after 6 consecutive runs CoRe<sub>1.6</sub> presented  
291 excellent stability with no significant changes in the structure except the partial oxidation and  
292 re-reduction of the Co particles that acts in favour on the restart of the NH<sub>3</sub> decomposition.

293 Potassium promoted iron catalysts supported on carbon (K<sup>+</sup>-Fe/C) were studied by Jedynak et  
294 al. [64] to show the influence of the iron particle sizes on the rate of ammonia decomposition.  
295 Results showed that smaller particles gave higher TOFs in contrast with larger particles. K<sup>+</sup>-  
296 Fe<sub>5.7</sub>/C (12.5 nm) gave a TOF value of 0.5 s<sup>-1</sup> in contrast with the K<sup>+</sup>-Fe<sub>24</sub>/C (24 nm) that  
297 displayed a TOF value of 0.25 s<sup>-1</sup> concluding, that the smaller the surface of iron crystallites is,  
298 the more advantageous are the catalytic properties.

299 Ganley et al. [65] examined 13 metallic catalysts (Ru, Ni, Rh, Co, Ir, Fe, Pt, Cr, Pd, Cu, Te,  
300 Se, Pb) supported on pellets of activated alumina in order to suggest potential alternatives of  
301 Ru catalysts due to their high cost. Ru was the most active catalyst and besides Ni that had 40%  
302 lower activity than Ru, all the others were not efficient for the ammonia decomposition  
303 reaction. Also, depending on the catalyst that is used, the rate limiting step differs regarding  
304 nitrogen desorption or N-H bond scission. This suggests that is unlikely to predict catalytic  
305 behaviour using only one parameter by assuming that a range of metallic catalysts have the  
306 same rate determining step for a given reaction.

307 Carbon nanotubes (CNTs) with residual Co or Fe nanoparticles were used as catalysts by Zhang  
308 et al. [66] for ammonia decomposition. With an increase in the temperature, ammonia  
309 conversion also increased and even at higher temperatures such as 700 °C the chemical  
310 composition and microstructure of CNTs remained the same as it was before the reaction took  
311 place. Fe containing CNTs had an activation period of 1200 min with a conversion up to 76 %  
312 but Co containing CNTs showed the highest activity overall with a conversion almost up to  
313 100 %. The higher activity of Co-containing CNTs might be due to their smaller particle size  
314 (4-20 nm) when compared with Fe-containing particles that were in the range of 10-50 nm, and  
315 the capacity of CNTs as electron reservoirs.

316 El-Shafie et al. [67] developed zeolite (SA-600A)-based catalysts with Ru and Li as supporting  
317 materials at different mixing ratios for H<sub>2</sub> generation from ammonia decomposition. For all the  
318 developed catalysts it was observed that increasing the temperature the conversion rate  
319 increased as well. It was observed that the catalyst was enhanced when the Li mixing ratio was  
320 increased, and the highest NH<sub>3</sub> conversion rate (99.9 %) was obtained from the catalyst with a  
321 Li mixing ratio of 4 %. The increase of Ru ratio enhanced the conversion rate even more at  
322 lower temperatures. The catalyst with mixing ratio of 40 g (SA-600A)/5 g RuCl<sub>3</sub>.nH<sub>2</sub>O/3 g  
323 LiOH·H<sub>2</sub>O obtained the highest catalytic activity and NH<sub>3</sub> conversion of 99.9 % at 490 °C.

324 Core-shell iron-based catalysts ( $\alpha$ -FeO<sub>2</sub>O<sub>3-x</sub>@pSiO<sub>2</sub>) were synthesized for ammonia  
325 decomposition by Feyen et al. [68]. The catalysts were found to be highly stable up to  
326 temperatures of 800 °C with higher reaction rates and full conversion for all the tested catalysts.  
327 Moreover, particle sizes between 35 and 75 nm showed a limited influence on the catalytic  
328 activity. Lastly, there were no diffusion limitations up to flow rates of 120000 cm<sup>3</sup> g<sub>cat</sub><sup>-1</sup> h<sup>-1</sup> that  
329 could have been observed from the porous silica shells.

330 Cobalt catalysts supported on different carbon materials were developed for H<sub>2</sub> production  
331 from ammonia decomposition by Zhang et al. [69]. The carbon materials that were utilised for  
332 the research were multi-walled carbon nanotubes (MWCNTs), single wall carbon nanotube  
333 (SWCNTs), three types of activated carbons (AC) and reduced graphene oxides (RGO). The  
334 highest NH<sub>3</sub> conversion was conducted by the Co/MWCNTs catalyst. The conversion of  
335 Co/RGO and Co/SWCNTs catalysts was very low and therefore they weren't used for further  
336 studies. Moreover, the influence of post-treatment temperature on the catalytic performance of  
337 10Co/MWCNTs (10% wt Co) was evaluated in this study at a temperature range of 230-700  
338 °C. Highest TOF value was obtained at 600 °C and it reached up to 8.15 s<sup>-1</sup>. Even after 20 h of

339 catalytic test there was no significant change in the mean particle size of Co. The fresh catalyst  
340 had a mean particle size of 4.8 nm while the used catalyst had a mean particle size of 5.6 nm.  
341 Due to its higher catalytic stability and the excellent catalytic activity for the decomposition of  
342 ammonia, Co/MWCNTs catalyst could be promising for future applications.

343 Catalysts with 2 % Ru content supported on lanthania-ceria materials with different molar  
344 ratios were synthesized by Le et al. [70] to evaluate the H<sub>2</sub> production by ammonia  
345 decomposition. The catalytic activity was tested at temperature range of 300-500 °C and the  
346 Ru/La<sub>0.33</sub>Ce<sub>0.67</sub> exhibited the best catalytic performance with an ammonia conversion of 91.9  
347 % and H<sub>2</sub> formation rate of 6.2 mmol g<sub>cat</sub><sup>-1</sup> min<sup>-1</sup>. The acid-base properties of the La<sub>x</sub>Ce<sub>1-x</sub>O<sub>y</sub>  
348 supports combined with the high dispersion of Ru particles resulted in the enhanced catalytic  
349 activity. After 100 h the catalyst maintained its high catalytic activity due to its excellent  
350 stability, since fresh and used catalyst had a mean particle size of 3.3 nm and 3.6 nm  
351 respectively, showing no significant difference in the size and structural morphology of the  
352 particle.

353 Monometallic Ni, Co and bimetallic Ni-Co alloy catalysts supported on SiO<sub>2</sub> were prepared by  
354 a co-impregnation method by Wu et al [71]. Bimetallic catalysts had better catalytic  
355 performance obtaining higher ammonia conversion due to the alloy synergistic effect between  
356 Ni and Co. Among the tested catalysts, the Ni<sub>5</sub>Co<sub>5</sub>/SiO<sub>2</sub> exhibited the highest catalytic activity  
357 achieving 76.8 % NH<sub>3</sub> conversion and H<sub>2</sub> formation rate of 25.71 mmol g<sub>cat</sub><sup>-1</sup> min<sup>-1</sup> under  
358 GHSV of 30,000 mL h<sup>-1</sup> g<sub>cat</sub><sup>-1</sup> at 550 °C. The effect of GHSV was also examined showing that  
359 the increase of GHSV resulted the conversion decrease. With lower GHSV of 6000 mL h<sup>-1</sup> g<sub>cat</sub><sup>-1</sup>  
360 the catalyst achieved 94.7 % NH<sub>3</sub> conversion. Further enhancement on the conversion (78.1  
361 %) was observed when K was added during the Ni<sub>5</sub>Co<sub>5</sub>/SiO<sub>2</sub> synthesis (K/(Ni + Co) molar ratio  
362 of 1:10) indicating that alkali act in favour of the catalytic decomposition of ammonia. The  
363 Ni<sub>5</sub>Co<sub>5</sub>/SiO<sub>2</sub>-K was evaluated for its stability for 30 h where it showed negligible decrease in  
364 conversion and thus excellent stability.

365 Studies have reported that the stronger basicity of the support the more efficient is the catalyst  
366 and thus promoting the catalytic decomposition of ammonia. Therefore, Podila et al. [72]  
367 utilized different Mg oxide systems (MgAl, MgCe and MgLa) as supports for cobalt catalysts  
368 (5 wt% Co) with Mg to X (X = Al, Ce, La) ratio of 2. Among these three, 5CMLa-2 presented  
369 the highest activity. The 5CMAI-2 and the 5CMCe-2 catalysts had lower activities. La-  
370 containing catalysts were further studied with different Mg/La molar ratios (Mg/La = 1, 2, 3, 5, 9

371 and 14). All the catalysts were active even at lower temperatures with 5CMLa-5 being the most  
 372 active. The higher activity of the 5CMLa-5 catalyst might be due to the increased surface area,  
 373 higher metal dispersion and the presence of basic sites that favour the ammonia decomposition.  
 374 It was concluded that Mg-La is a promising support for the reaction of ammonia  
 375 decomposition.

376 Pinzón et al. [73] developed Co catalysts supported on  $\beta$ -SiC for the H<sub>2</sub> production by ammonia  
 377 decomposition at reaction temperatures below 500 °C. The catalysts were modified with  
 378 different metals (K, Cs, Ca, Mg, La and Ce) to study the effect of promoters. The catalysts with  
 379 the addition of 1 % of Cs, Mg, Ca or Ce showed poorer performance while the catalysts loaded  
 380 with K or La enhanced the catalytic activity due their electron-donor properties that modified  
 381 the electronic structure of Coactive sites. A conversion of 97.3 % and H<sub>2</sub> production rate of  
 382 69.3 mmol H<sub>2</sub> g<sub>Co</sub><sup>-1</sup> min<sup>-1</sup> was obtained by the 1K-Co/SiC catalyst (4.1 wt % Co) at 450 °C.  
 383 Different K loadings were also studied, and results showed that the increase of metal loading  
 384 above 1% decreased the conversion of ammonia because the excess amount of metal blocked  
 385 the active sites of the cobalt catalysts. Lastly, the stability of the catalyst was tested for over 24  
 386 h at 400 °C and 83 % conversion of ammonia was reached providing excellent stability.

387 Table 1. Heterogeneous catalysts used for the ammonia decomposition.

Catalyst	Temperature (°C)	Conversion (%)	TOF (1/s)	Reference
Ni/MgAl <sub>2</sub> O <sub>4</sub> – LDH	600	88.7	2.18	[58]
Co/NC-600	500	80		[59]
Ru/SmCeOx	400	74.9	25.81	[60]
35Co/BHA	500	87.2		[61]
2.5Ru/10C-rGO	400	96	75.4	[62]
CoRe <sub>1.6</sub>	500	~90		[63]
K <sup>+</sup> -Fe/C	470	20	~0.5	[64]
Ru/Al <sub>2</sub> O <sub>3</sub>	580		6.85	[65]
Ni/Al <sub>2</sub> O <sub>3</sub>	580		4.21	[65]
Co-containing CNTs	700	~100		[66]
Fe-containing CNTs	700	76		[66]
(SA-600A)/RuCl <sub>3</sub> .nH <sub>2</sub> O/LiOH·H <sub>2</sub> O (40:5:3)	490	99.9		[67]
$\alpha$ -FeO <sub>2</sub> O <sub>3</sub> -50@pSiO <sub>2</sub>	800	100		[68]
10% Co/MWCNTs	600		8.15	[69]
Ru/La <sub>0.33</sub> Ce <sub>0.67</sub>	450	91.9	11.4	[70]
Ni <sub>5</sub> Co <sub>5</sub> /SiO <sub>2</sub>	550	76.8		[71]
5CMLa-5	550	82.7		[72]
1%K-Co/SiC	350	33.1	9.3	[73]
1%K-Co/SiC	450	97.3		[73]

388 As observed from Table 1, the temperature ranges from 400 to 800 °C because ammonia  
389 requires higher temperatures for its effective decomposition. At higher temperatures the  
390 conversion is higher and in some cases the catalysts achieve almost complete conversion. Even  
391 though Ru is a precious and expensive metal, many studies have focused on Ru catalysts due  
392 to their excellent catalytic properties [60], [62], [65], [67], [70]. However, other novel catalysts  
393 are investigated with promising results for future experiments [58], [61], [63], [66], [73].  
394 Supporting materials are also studied because of their properties for enhanced catalytic  
395 operation as they can offer higher surface area, chemical stability and mechanical strength [74].  
396 Generally, the most common ones are alumina and silica [65], [71], but other materials are used  
397 as well [59–62], [69], [73].

#### 398 **4.1.1 Structural and physicochemical properties of heterogeneous catalysts**

399 It's necessary to consider any chemical and physical transformation that will occur during the  
400 development process of efficient catalysts. The structure and properties of the catalysts play a  
401 significant role for the decomposition of any reaction. It is well known that the catalytic  
402 decomposition of ammonia is structure sensitive and strongly depends on the size, shape and  
403 properties of the catalyst. Mazzone et al. [75] synthesised unpromoted and sodium promoted  
404 Ru particles supported on carbon xerogels. The purpose of this study was to investigate the  
405 behaviour of the catalysts with support and with or without the promoter. During the second  
406 reaction run the un-promoted catalysts exhibited higher reaction rates compared with the first  
407 reaction run. The authors explained that the higher reaction rates are due to the formation of  
408 B5 sites after the catalyst was exposed at 600 °C. The B5 sites work in favour of the  
409 decomposition reaction, speeding up the N desorption. Sodium as a promoter had a positive  
410 effect on the performance of the catalyst preventing the sintering of the Ru particles since the  
411 catalyst before and after five runs had the same average particle size for all tested catalysts. In  
412 contrast, the un-promoted catalysts presented a slight increase in the mean particle size, e.g.,  
413 from 1.9 nm to 2.5 nm due to the sintering of Ru particles from high temperatures. The support  
414 was either activated with carbon dioxide or doped with nitrogen and both treatments had a  
415 positive impact on the catalytic performance.

416 The effect of particle size was examined by El-Shafie et al. [76] using two different diameters  
417 of alumina particles size (1 and 2 mm) for the decomposition of ammonia assisted by dielectric  
418 discharge plasma (DBD). The conversion rates and H<sub>2</sub> concentration were measured at different

419 ammonia flow rates and plasma voltage. Conversion rates of 83.2 and 80.4 % were obtained  
420 by Al<sub>2</sub>O<sub>3</sub> particle sizes of 1 and 2 mm respectively. Moreover, particle size of 1 mm resulted  
421 in higher H<sub>2</sub> concentration. The higher conversion and H<sub>2</sub> concentration are attributed to the  
422 higher surface area in the smaller particle and thus, longer residence time for the decomposition  
423 reaction. Therefore, it was concluded that the particle size is a significant factor for this  
424 catalytic decomposition.

425 Cobalt catalysts in the form of cobalt oxide (II III) promoted with calcium, aluminium and  
426 potassium oxides were developed with precipitation method by Czekajło et al. [77]. With the  
427 increase in the precipitation process temperature, it was observed that the size of Co<sub>3</sub>O<sub>4</sub>  
428 crystallites was reduced leading to a decrease of the efficiency process. The ZBAP1-C catalyst  
429 that was promoted with calcium, potassium, and aluminium oxides obtained the highest  
430 catalytic activity with a decomposition degree of 100 % at 525 °C. The addition of alumina had  
431 a positive effect on a shift of the maximum conversion of ammonia towards lower reaction  
432 temperatures. The ZBAP1-B catalyst had the lowest surface area value impregnated only with  
433 oxides of calcium and potassium while the ZBAP1-C catalyst showed higher resistance in  
434 sintering indicating that the addition of aluminium has a positive impact on the stability of the  
435 surface structure as well.

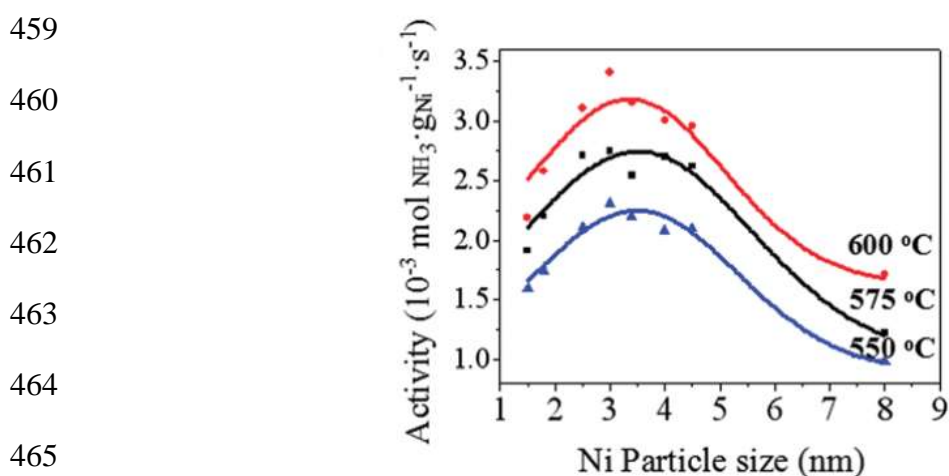
436 Fly ash (FA), a waste material, was used as support for Ru catalysts for H<sub>2</sub> production by  
437 ammonia decomposition by Li et al. [78]. The FA samples were acid treated and heat treated,  
438 and results showed that treatment enhanced the surface area and pore volume. Ru impregnation  
439 further increased the surface area and pore volume on the heat treated and untreated FA samples  
440 but decreased on the acid treated samples. From the catalysts used, Ru/FA-800 had the highest  
441 conversion of ammonia due to high Ru dispersion, less acid sites and stronger NH<sub>3</sub> adsorption.

442 Lenzion-Bielun et al. [79] examined the effect of different promoters (CaO, Al<sub>2</sub>O<sub>3</sub> and, K<sub>2</sub>O)  
443 and also the addition of manganese and chromium on the structure of cobalt catalysts for  
444 ammonia decomposition. Sintering of pure cobalt was noticed at a temperature of 600 °C, but  
445 with the addition of the oxides as promoters the surface area of the catalysts was stabilized.  
446 The catalytic tests showed that the unpromoted Co catalyst has the lowest activity due to a very  
447 low surface area. The Co(0) catalyst that was promoted with the oxides (2.6 wt % Al<sub>2</sub>O<sub>3</sub>, 1.5  
448 wt % CaO, 0.5 wt % K<sub>2</sub>O and 95.4 wt % Co) presented the highest activity at temperatures of  
449 500 and 550 °C with NH<sub>3</sub> conversion up to 40.1 and 50 % respectively. Even though an addition



450 of chromium and manganese lead to an enhancement on the surface area of the catalyst, the  
451 activity was decreased.

452 To investigate the influence of particle size, Li et al. [80] developed Ni particles supported on  
453 MCF-17 with particle range size from 1.5 to 8.0 nm. The ammonia decomposition reaction was  
454 affected by the particle size of the catalysts especially with small Ni particles. Moreover, the  
455 particle size effect was studied at various temperatures and a volcano relationship between the  
456 particle size and the catalytic activity was obtained (Fig. 3) proving that the catalysts are  
457 structural sensitive. The Ni/MCF-17 catalyst with an average of 3.0 nm particle size exhibited  
458 excellent catalytic performance at all temperatures.



466 Fig. 3. Effect of the particle size at different reaction temperatures [80].

467 Besides the correlation between the particle size of catalysts and the catalytic activity, the  
468 structure/morphology of the support is important to be explored. Huang et al. [81] studied  
469 cobalt catalysts supported on three kinds of CeO<sub>2</sub> supports, 3D ordered mesoporous (3DOM),  
470 nanotubes (NT) and nanocubes (NC). The Co/CeO<sub>2</sub>-3DOM catalyst exhibited the best catalytic  
471 performance with 4.2 mmol H<sub>2</sub> min<sup>-1</sup> g<sub>cat</sub> H<sub>2</sub> production rate at 500 °C. According to different  
472 characterization techniques that were used in the experiment it was concluded that the particle  
473 size was not the main factor to influence the reaction but the different morphologies of the  
474 support. The morphology of the Co/CeO<sub>2</sub>-3DOM catalyst was favourable for construction of  
475 more active sites and thus the better catalytic performance.

## 476 4.2 Photocatalysis and Electrocatalysis of Ammonia

477 Photocatalytic decomposition is considered a promising system for the H<sub>2</sub> production because  
478 it can be operated at ambient temperature conditions, and the reaction can be easily controlled

479 by switching on and off the light irradiation [82–85]. TiO<sub>2</sub> photocatalysts were developed by  
480 Abdul Razak et al. [86] that were impregnated with Pd and Cu respectively for enhancement  
481 of the photocatalytic activity. After 3 h of light irradiation Pd/TiO<sub>2</sub> exhibited the highest  
482 activity producing 65 μmol of H<sub>2</sub> while Cu/TiO<sub>2</sub> and TiO<sub>2</sub> showed almost no production of H<sub>2</sub>.  
483 For the investigation of the stability of the photocatalysts in alkaline conditions, different NH<sub>3</sub>  
484 concentrations were investigated. With a concentration up to 19.1 g/L yield was enhanced up  
485 to 30.4 μmol but further increase of NH<sub>3</sub> resulted in a decline of the H<sub>2</sub> production rate.  
486 Dimethyl sulfoxide (DMSO) was also added as hydroxyl scavenger in ammonia further  
487 enhancing the H<sub>2</sub> yield to 121 μmol and was continuously increasing in the first cycle reaction.  
488 However, the rate of H<sub>2</sub> production was reduced with the subsequent reaction cycles and during  
489 the photocatalytic decomposition with DMSO methane gas was detected.

490 Apart from catalysis and photocatalysis, electrochemical decomposition of ammonia has a high  
491 potential for supply of CO<sub>x</sub>-free energy. Fig. 4 demonstrates a typical ammonia electrolytic cell  
492 for hydrogen generation. The most active catalyst for this reaction is Pt and thus lots of research  
493 was carried out with Pt catalysts. However, it is very expensive so recent studies are focused  
494 on Pt-free catalysts [87–89]. Binary alloy electrocatalysts based on Ni such as Ni-Co, Ni-Mo,  
495 Ni-Fe, and Ni-Ce deposited on nickel foam were synthesized by Jiang et al. [90] for the  
496 electrochemical generation of H<sub>2</sub> by ammonia. From all the electrodes investigated, Ni-Co in  
497 the form of nanoneedle resulted in an impressive electrochemical performance. For further  
498 improvement the Ni-Co catalyst was introduced to nitrogen doping and ammonia annealing  
499 treatment to obtain NiCo<sub>2</sub>N electrodes. The activity was dramatically increased demonstrating  
500 a superior HER electrocatalytic performance. The NiCo<sub>2</sub>N electrocatalysts also showed an  
501 excellent stability as there was no significant change after 10 h of catalytic process. Moreover,  
502 it was concluded that the electrolysis potential in ammonia (0.71 V) was much lower than the  
503 water splitting suggesting that ammonia electrolysis can replace water electrolysis for H<sub>2</sub>  
504 production. Table 2 summarises the results from photocatalysis and electrocatalysis of  
505 ammonia.

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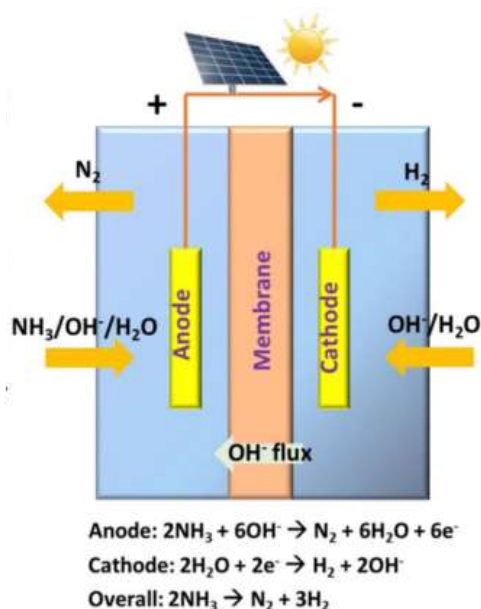
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515 Fig. 4. A typical cell of ammonia electrolysis for hydrogen production [89].

516 Table 2. Photocatalysts and Electrocatalysts used for ammonia decomposition.

Photocatalysis				
Catalyst	H <sub>2</sub> Yield (μmol)			Reference
Pt/TiO <sub>2</sub>	160			[82]
Pt/Fe-TiO <sub>2</sub>				[83]
Ce/TiO <sub>2</sub>	80			[84]
Pd/TiO <sub>2</sub>	65			[86]
Pd/TiO <sub>2</sub> -DMSO	121			[86]
Electrocatalysis				
Catalyst	System	Onset Potential	Current Density (mA cm <sup>-2</sup> )	Reference
NiCu/C	55mM NH <sub>4</sub> Cl + 0.5 NaOH	0.47 V vs Ag/AgCl	52	[87]
Ni <sub>98</sub> Pd <sub>2</sub>	1M NaNO <sub>3</sub> + 200mM NH <sub>4</sub> NO <sub>3</sub> + NaOH	1.25 V vs Hg/HgO	~2	[88]
NiCo <sub>2</sub> N	1M KOH + 1M NH <sub>3</sub> .H <sub>2</sub> O	100x10 <sup>-3</sup> V vs RHE	100	[90]

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## 5 Hydrous Hydrazine Decomposition as a sustainable hydrogen production method

### 5.1 Heterogeneous Catalysis of Hydrous Hydrazine Decomposition

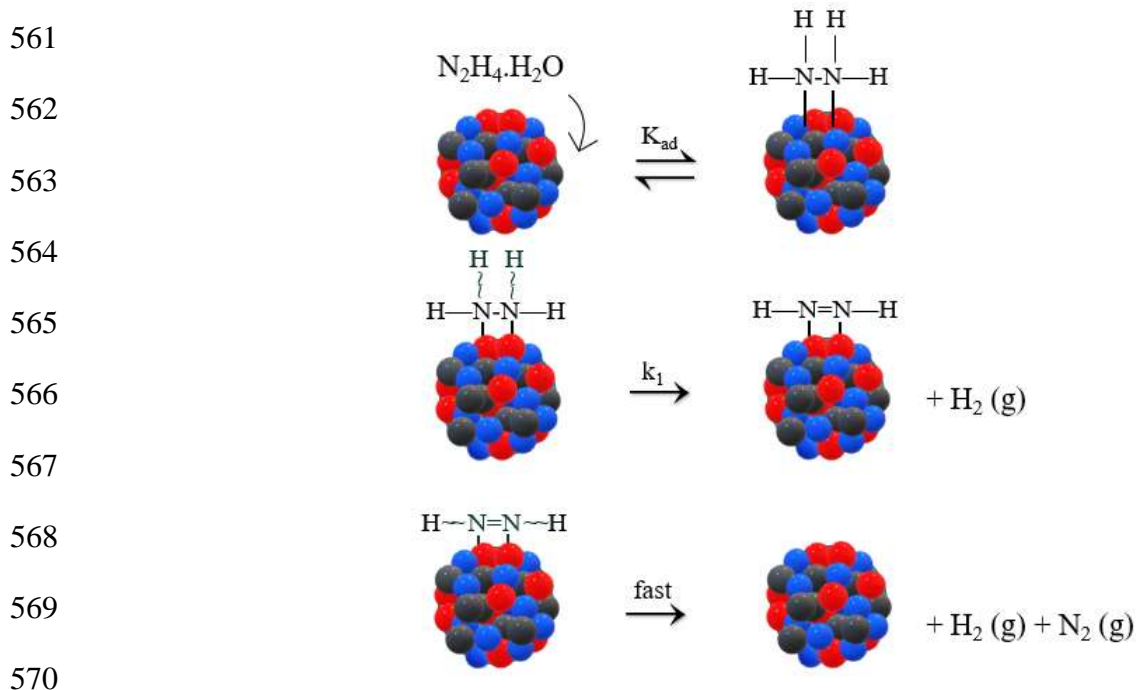
In recent years, the development of efficient catalysts for the decomposition of hydrous hydrazine for H<sub>2</sub> generation has been the focus of many studies. Ni particles were found to be a preferable choice and its alloying with noble metals such as Ir, Pt, Pd and Rh result in a noteworthy improvement on the H<sub>2</sub> selectivity and the catalytic performance due to the alloy synergistic effect [91–93]. Unfortunately, their applications are limited due to the high cost of noble metals. Therefore, it is essential to develop non noble metal containing catalysts. Until now, many studies have reported the decomposition of hydrous hydrazine with noble-metal-free catalysts. Different types of catalysts that were used for the decomposition of hydrous hydrazine are displayed in Table 3.

Noble-metal-free Ni-Fe particles supported on CeZrO<sub>2</sub> were synthesised by Zoo et al. [94]. The Ni-Fe/CeZrO<sub>2</sub> alloy catalyst with Ni/Fe molar ratio of 8:2 (9.11 wt % Ni and 2.41 wt % Fe) had a TOF value of 119.2 h<sup>-1</sup> and 100% H<sub>2</sub> selectivity in the presence of NaOH and temperature of 343 K. The catalyst exhibited high stability showing negligible decrease on the H<sub>2</sub> selectivity after five runs. The mean particle size of the Ni-Fe/CeZrO<sub>2</sub> catalyst was 5.2 ± 0.8 nm while after five runs was 5.3 ± 1.2 nm. Other supports as LaZrO<sub>2</sub> and NdZrO<sub>2</sub> also presented excellent catalytic properties. Ni-Co, Ni-Cu and Co-Fe supported on CeZrO<sub>2</sub> were also examined and exhibited lower selectivity towards H<sub>2</sub> concluding that NiFe is a highly efficient candidate for the replacement of noble metal catalysts for the hydrous hydrazine decomposition.

Liu et al. [95] synthesized Ni-Mo particles supported on TiO<sub>2</sub> for the catalytic decomposition of hydrous hydrazine. The Ni<sub>0.16</sub>Mo<sub>0.04</sub>/TiO<sub>2</sub> catalyst with 22.6 wt % Ni and 9.23 wt % Mo exhibited a TOF value of 484 h<sup>-1</sup> and 100 % H<sub>2</sub> selectivity. Further increase of the support content decreased the catalytic performance, After, 10 cycles the selectivity remained 100% but the TOF decreased to 138 h<sup>-1</sup>. Ni-Cu/TiO<sub>2</sub>, Ni-Fe/ TiO<sub>2</sub>, and Ni-Co/TiO<sub>2</sub> catalysts were also prepared for investigation of doping other metals and results showed that the catalytic performances of these catalysts were inferior to Ni-Mo/TiO<sub>2</sub> concluding that Mo doping

547 improves the dispersion and modifies the geometric and electronic structure of the catalyst  
548 facilitating the  $N_2H_4$  decomposition.

549 Mono-, bi- and tri-metallic noble and noble-metal free catalysts were prepared by Al-Thubaiti  
550 et al. [96] to investigate their catalytic activity in the dehydrogenation of hydrous hydrazine.  
551 Monometallic Ag, Ni, Pd, Fe and Cu particles were inactive while the activity of bimetallic  
552 catalysts was higher. The most active catalyst was the trimetallic Ni/Fe/Pd catalyst that  
553 contained 28.7 wt % Ni, 23.5 wt % Fe and 47.7 wt % Pd and average size of 20 nm. It exhibited  
554 excellent selectivity towards  $H_2$  and therefore was used for further experiments. After five  
555 continuous runs the catalytic activity of the catalyst remained the same. It was concluded by  
556 the authors that adding a third metal in a bimetallic catalyst with a specific combination has a  
557 positive impact on the selectivity of  $H_2$ . Fig. 5 shows the proposed mechanism for the  
558 decomposition of ammonia on the surface of the Ni/Fe/Pd catalyst. Moreover, new catalysts  
559 can be developed with different metal plating order for the decomposition of hydrazine for  $H_2$   
560 production.



571 Fig. 5. Decomposition mechanism of hydrous hydrazine on the surface of the trimetallic  
572 Ni/Fe/Pd catalyst [96].

573 Different elements (Rh, Co, Ru, Ir, Cy, Ni, Fe, Pt, Pd NPs) were studied as catalysts for the  
574 decomposition of hydrous hydrazine for  $H_2$  production by Sanjay et al. [97]. It was found that  
575 the catalytic activity and the selectivity were depended on the catalyst used. Rh was the most

576 active catalyst whereas Cu, Ni, Fe, Pt and Pd were inactive for the reaction in aqueous solution  
577 even though they were active in the reaction that took place in the gas-phase. In the case of Co,  
578 Ru and Ir the selectivity towards H<sub>2</sub> was very low. The reason this is happening is because Co,  
579 Ru and Ir nanoparticles prefer the activation of the N-N bond which is forming ammonia. In  
580 comparison Rh particles prefer the activation of N-H bond and that's why they are highly  
581 active. Moreover, it was observed that the catalytic activity was enhanced when the Rh particles  
582 were reduced with NaBH<sub>4</sub> in the presence of hexadecyltrimethyl ammonium bromide  
583 concluding that the modification of nanoparticles during their preparation could affect their  
584 efficiency.

585 Motta et al. [98] investigated the catalytic performance of Ir/CeO<sub>2</sub> as catalyst for the  
586 decomposition of hydrous hydrazine to generate H<sub>2</sub>. Parameters such as stirring speed, mass of  
587 catalyst, NaOH concentration and reaction temperature were studied to find the optimal  
588 conditions for the reaction with respect on the activity and selectivity of the catalytic  
589 decomposition. Stirring rate affected both the reaction rate and the selectivity and it was found  
590 that with lower stirring rate the H<sub>2</sub> yield was also lower. The optimum stirring rate was 1050  
591 rpm and was used for the following tests. The mass of the catalyst did not affect the yield of  
592 the reaction but there was an increase in the activity for molar ratios between 125:1 and 250:1  
593 and the latter were selected for the further catalytic tests. With an increase of the NaOH  
594 concentration there was an increase in H<sub>2</sub> yield and 0.5 M NaOH was chosen as the optimal  
595 value. Lastly, with an increase in the temperature the selectivity decreased in contrast with the  
596 activity of the catalyst that was increased so the value of 50 °C was chosen because of the  
597 intermediate values of activity and selectivity that exhibited. The fresh catalyst had a mean  
598 particle size of  $0.9 \pm 0.2$  nm and after five uses  $1.2 \pm 0.4$  nm where the difference was in the  
599 range of the error analysis.

600 Kang et al. [99] developed Ni/CeO<sub>2</sub> catalysts for the decomposition of hydrous hydrazine. A  
601 solution combustion synthesis (SCS) varying different parameters was used to synthesize the  
602 catalysts and catalytic tests were run under 50 °C. It was obtained that catalysts with smaller  
603 Ni size particle and larger pore size act in favour of the decomposition resulting in a good  
604 catalytic performance. 6 wt % Ni/CeO<sub>2</sub> catalysts with 14.7 nm mean particle size and 18.8 nm  
605 pore size, exhibited a H<sub>2</sub> selectivity of 100 %, N<sub>2</sub>H<sub>4</sub>.H<sub>2</sub>O conversion of 50 % at 17.7 min  
606 corresponding to a TOF value of 34.0 h<sup>-1</sup>. Moreover, the formation of Ni-O-Ce solid promoted  
607 the reaction for H<sub>2</sub> generation, but higher concentrations decreased the catalytic activity. A 30-

608 fold increase of the reaction rate was obtained when increasing the temperature from 30 to 90  
609 °C but the selectivity dropped at 93 %. Lastly, for comparison purposes, Ni-based catalysts  
610 developed with different methods were tested and even though a high number of parameters  
611 need to be considered, it was concluded that the catalysts created by the SCS method had better  
612 catalytic performance.

613 An alloy of Ni-Pd nanoparticles ( $\text{Ni}_{1-x}\text{Pd}_x$ ) were synthesized by Singh et al. [100] and were  
614 examined under mild reaction conditions. The  $\text{Ni}_{0.60}\text{Pd}_{0.40}$  catalyst exhibited the highest  
615 selectivity (82 %) among the others tested. To test the effect of alloy, a physical mixture of Ni  
616 and Pd was tested and performed poor catalytic activity compared with the alloy catalyst  
617 indicating that the modified catalyst surface favours this reaction. The combination of Pd with  
618 other metals (Fe, Co and Cu) resulted poor catalytic performance (or inactive) as well as  
619 implying that the presence of Ni has a positive effect on the decomposition of hydrous  
620 hydrazine.

621 He et al. [101] developed Ni-based catalysts by using Ni-Al hydrotalcite-like compound as  
622 precursors. A conversion of 100 % was exhibited with a  $\text{H}_2$  selectivity of 93 % at 30 °C and 70  
623 min reaction time. The high selectivity can be attributed to the small Ni particles and strong  
624 basic sites. When the temperature increased up to 80 °C, the reaction time decreased at 5 min  
625 and the selectivity was reduced to 82 %. A Ni/ $\text{Al}_2\text{O}_3$ -IMP catalyst was also tested for the  
626 decomposition of hydrous hydrazine and compared with Ni- $\text{Al}_2\text{O}_3$ -HT. A lower activity was  
627 noticed by the Ni/ $\text{Al}_2\text{O}_3$ -IMP catalyst with  $\text{H}_2$  selectivity at 66 % and 440 min of reaction time  
628 due to the poor Ni dispersion.

629 Amorphous catalytic Co-Pt particles induced on  $\text{CeO}_x$  were developed by Song-Il et al. [102].  
630 It was discovered that the  $\text{CeO}_x$  plays a crucial role in the transformation of the crystalline  
631 phase to the amorphous one. The highest catalytic performance among the catalysts tested was  
632 achieved by the  $\text{Co}_{0.65}\text{Pt}_{0.30}(\text{CeO}_x)_{0.05}$  nanoalloy, at 25 °C with  $\text{H}_2$  selectivity of 72.1 % in 3.5  
633 min and TOF value of  $194.8 \text{ h}^{-1}$  which is even higher than that of the crystalline phase catalyst.  
634 Therefore, it was concluded by the authors that  $\text{Co}_{0.65}\text{Pt}_{0.30}(\text{CeO}_x)_{0.05}$  exhibited the most  
635 optimum performance encouraging its practical use for the decomposition of  $\text{N}_2\text{H}_4 \cdot \text{H}_2\text{O}$  to  
636 produce  $\text{H}_2$ .

637 Several studies used Rh-Ni alloy catalysts supported on different materials for the  
638 decomposition of hydrous hydrazine. Zhang et al. [103] developed  $\text{CeO}_x$ -doped Rh-Ni particles  
639 supported on reduced graphene oxide (rGO). The  $\text{Rh}_{0.8}\text{Ni}_{0.2}@ \text{CeO}_x/\text{rGO}$  catalyst completely

640 decomposed  $\text{N}_2\text{H}_4$  at room temperature in 33 min with a TOF value of  $36.4 \text{ h}^{-1}$ . Further increase  
641 in the temperature at  $60 \text{ }^\circ\text{C}$ , catalysed the reaction in 3.0 min giving a TOF value of  $400.0 \text{ h}^{-1}$ .  
642 Other studies used MOFs for the support of catalytic materials and therefore RhNi@MIL-101  
643 [104] and Ni-Rh/NPC-900 [105] were developed and tested at  $50 \text{ }^\circ\text{C}$  and alkaline conditions  
644  $0.5 \text{ NaOH}$ . High TOF values of  $344 \text{ h}^{-1}$  and  $156 \text{ h}^{-1}$  were exhibited respectively with  $100 \text{ } \%$   $\text{H}_2$   
645 selectivity. Other supports that were used in these studies presented inferior catalytic  
646 performance.

647 Dai et al. [106] synthesized bimetallic Ni-Ir alloy nano-catalysts supported on  $\text{CeO}_2$  for the  
648 decomposition of hydrous hydrazine for  $\text{H}_2$  production. The catalyst showed great catalytic  
649 activity and high  $\text{H}_2$  selectivity. Further increase on the Ir content ( $\text{Ni}_{91}\text{Ir}_9/\text{CeO}_2$ ) resulted in an  
650 optimal catalytic performance and was further investigated. The decomposition rate of hydrous  
651 hydrazine increased with increasing the reaction temperature. Also, the catalyst was submitted  
652 to cyclic usage, and it was found that it retains  $100 \text{ } \%$   $\text{H}_2$  selectivity even after 15 cycles but  
653 the catalytic activity was decreasing after cycle.

654 Nickel particles were prepared by encapsulation in the channel of TNTs (Ni@TNTs) and  
655 deposition on the surface of TNTs (Ni/TNTs) by Wang et al. [107]. Ni@TNTs exhibited high  
656 catalytic activity than the Ni/TNTs catalyst and nearly  $100 \text{ } \%$   $\text{H}_2$  selectivity at  $333 \text{ K}$ . The TOF  
657 value of this reaction was  $96.0 \text{ h}^{-1}$ . The encapsulation of Ni particles led to a small particle size  
658 of  $2.7 \text{ nm}$ , large pore size of  $10.2 \text{ nm}$  and high dispersion ( $28.2 \text{ } \%$ ) resulting in more active  
659 sites. Moreover, after six continuous catalytic runs the catalyst did not have any significant loss  
660 in its catalytic activity due to the prevention of nickel particles leaching during the catalysis,  
661 since the particle size had a small increase of  $3.5 \text{ nm}$ . In contrary, Ni particles on Ni/TNTs  
662 increased from  $2.4$  to  $8.9 \text{ nm}$  indicating that aggregation is occurring without the TNTs  
663 constraining the Ni particles.

664 Rh nanoparticles modified with Molybdenum Oxide ( $\text{MoOx}$ ) were prepared by Yao et al. [108]  
665 with different metal compositions for the catalytic decomposition of hydrous hydrazine and  
666 hydrazine borane. Various reaction temperatures were studied and at temperature of  $323 \text{ K}$  and  
667 the presence of  $\text{Rh}_{0.5}(\text{MoOx})_{0.5}$ ,  $\text{N}_2\text{H}_4$  was completely decomposed to  $\text{H}_2$  and  $\text{N}_2$  with  $100\%$   $\text{H}_2$   
668 selectivity and TOF value of  $750 \text{ h}^{-1}$ . The catalyst had an average mean particle size of  $3.8 \pm$   
669  $0.8$  and its composition was  $10.05 \text{ wt } \%$  Rh and  $8.92 \text{ wt } \%$  Mo. It was concluded that the  
670 increased catalytic performance obtained by the Rh-based catalysts might encourage the  
671 utilisation of hydrous hydrazine as  $\text{H}_2$  storage material.



673 Table 3. Heterogeneous catalysts utilised for the hydrous hydrazine decomposition.

Catalyst	Temperature (°C)	Conversion (%)	TOF (1/s)	Reference
Ni <sub>0.8</sub> Fe <sub>0.2</sub> /CeZrO <sub>2</sub>	70		0.033	[94]
Ni <sub>0.16</sub> Mo <sub>0.04</sub> /TiO <sub>2</sub>	70	~100	0.134	[95]
Ni/Fe/Pd	40		0.007	[96]
Ir/CeO <sub>2</sub>	50	~100	~0.028	[98]
6 wt% Ni/CeO <sub>2</sub>	50	50	0.009	[99]
Ni <sub>0.60</sub> Pd <sub>0.40</sub>	50			[100]
Ni-Al <sub>2</sub> O <sub>3</sub> -HT	30	100		[101]
Co <sub>0.65</sub> Pt <sub>0.30</sub> (CeOx) <sub>0.05</sub>	25		0.054	[102]
Rh <sub>0.8</sub> Ni <sub>0.2</sub> @CeOx/rGO	60	100	0.111	[103]
RhNi@MIL-101	50		0.095	[104]
NiRh/NPC-900	50	>50	0.043	[105]
Ni <sub>91</sub> Ir <sub>9</sub> /CeO <sub>2</sub>	50	100		[106]
Ni@TNTs	60	~100	0.026	[107]
Rh <sub>0.5</sub> (MoOx) <sub>0.5</sub>	50	100	0.208	[108]

674 Comparing with the temperature range of the ammonia decomposition, as seen from Table 3  
675 that hydrous hydrazine decomposition is more favored at lower temperatures (30-70 °C). The  
676 most studied temperature is 50 °C giving almost total conversion of hydrous hydrazine [98–  
677 100], [104–106], [108]. Nickel is a promising catalyst for this decomposition and by alloying  
678 it with other elements, many studies give positive results [94], [95], [99], [101], [107].  
679 However, noble metals are often used for the alloys, limiting their application [96], [100], [103–  
680 106]. Still research needs to be done though, considering the low TOF values.

### 681 5.1.1 Structural and physicochemical properties of heterogeneous catalysts

682 While the majority of studies are focused on the structure of the catalysts there was no in-depth  
683 study of the insights of the microstructure transformations during the synthesis of catalysts  
684 which are a key point for the catalytic activity for the hydrous hydrazine decomposition.  
685 Therefore Qiu et al. [109] synthesised Ni@Ni-Ir/meso-CeO<sub>2</sub> catalysts for the investigation of  
686 the catalytic properties that may be affected by the composition of the surface. Ni@Ir/ meso-  
687 CeO<sub>2</sub> resulted from the formation of the Ir surface layer on the Ni particles and with calcination  
688 treatment the targeted Ni@Ni-Ir/meso-CeO<sub>2</sub> alloy catalyst was synthesized. The post-treated  
689 alloy exhibited excellent activity with a reaction rate of 343 h<sup>-1</sup> and H<sub>2</sub> selectivity (100 % H<sub>2</sub>)  
690 at 50 °C, in contrast with the as-prepared catalyst that had lower selectivity and catalytic

691 performance. It was concluded that the calcination treatment had a positive impact since the  
692 Ni@Ir alloy enhanced both the selectivity and catalytic activity.

693 Shi et al. [110] studied in detail the formation mechanism of the bimetallic Ni<sub>50</sub>Pt<sub>50</sub>/CeO<sub>2</sub> alloy  
694 for the investigation of the influence of preparation process to the structure of the catalyst and  
695 thus, the impact on catalytic activity. It was discovered that during the synthesis process the  
696 formation of [(CH<sub>3</sub>)<sub>4</sub>N]<sub>2</sub>PtCl<sub>6</sub> took place during the co-precipitation step. While increasing the  
697 aging time crystalline [(CH<sub>3</sub>)<sub>4</sub>N]<sub>2</sub>PtCl<sub>6</sub> disappeared due to the conversion to metallic Pt which  
698 was found to have a major impact on the composition and microstructure of the catalyst. As a  
699 result, the catalytic performance of the Ni<sub>50</sub>Pt<sub>50</sub>/CeO<sub>2</sub> catalyst was different depending on the  
700 aging time. After 5-12 h of aging time the reaction rate was 465-500 h<sup>-1</sup> at 30 °C which was 2.5  
701 times higher than the reaction time of the catalysts with aging time of 0-1 h.

702 In another study by Shi et al. [111], noble metal free Ni-W-O alloy nano-catalysts  
703 (Ni<sub>4</sub>W/WO<sub>2</sub>/NiWO<sub>4</sub>) were synthesised with a hydrothermal process and different reduction  
704 temperatures to investigate any changes in the microstructure of the catalysts. Results showed  
705 that increasing the annealing treatment temperature the catalytic properties are increased as  
706 well. The reduction at 350 °C showed both low selectivity and reaction rate while at 400 °C  
707 selectivity was 99 % and the reaction rate up to 33 h<sup>-1</sup> with a complete decomposition of  
708 hydrazine at 50 °C and reaction time of 18 min. Further increase of the annealing treatment  
709 temperature reduced the efficiency of the catalyst. Moreover, different characterization  
710 analyses were used to better understand if the increased catalytic properties were correlated  
711 with the temperature treatment. A decrease on the specific surface area was obtained with the  
712 increased reduction temperature that led to the enhanced catalytic performance.

713 A Ni-Pt/La<sub>2</sub>O<sub>3</sub> catalyst was synthesised by Zhong et al. [112] combining alloying and  
714 immobilization strategies. The targeted Ni@Ni-Pt/La<sub>2</sub>O<sub>3</sub> contained a Ni core and Ni-Pt alloy  
715 shell and exhibited 100 % H<sub>2</sub> selectivity. A key factor to achieve great catalytic performance  
716 is the formation of the bimetallic alloy therefore the study was not only focused on the catalytic  
717 activity of the particles but also the physicochemical surface composition and structure. The  
718 excellent catalytic properties were correlated with the electronic and geometric structures  
719 changes during the Ni-Pt formation. Moreover, the catalysts were subjected into a second time  
720 replacement and calcination treatment under 350 °C, and it was observed that both activity and  
721 selectivity towards H<sub>2</sub> were increased. It was found that not proper control of the calcination  
722 temperature can drastically reduce the performance of the catalyst. In general, there was a

723 remarkable improvement after the treatment but still the reason behind the enhancement and  
724 the dependence of the treatment needs to be further studied.

### 725 **5.1.2 NH<sub>3</sub> Formation**

726 As it was mentioned hydrous hydrazine can be decomposed by two pathways resulting in the  
727 undesirable ammonia production. Thus is a necessity to develop effective catalyst with high  
728 selectivity towards H<sub>2</sub>. Ni catalysts alloyed with noble metals were a preferred choice by many  
729 researchers due to their remarkable enhancement of catalytic properties that resulted from the  
730 alloy synergy effect. For example, Singh et al. [93] developed bimetallic Ni-Pt alloy nano-  
731 catalysts to enhance the selectivity of Ni nanoparticles that was around 33 % at 323 K. By  
732 alloying Ni with Pt content as low as 1 mol % (Ni<sub>0.99</sub>Pt<sub>0.01</sub>), a complete conversion of N<sub>2</sub>H<sub>4</sub>.H<sub>2</sub>O  
733 was obtained in 120 min at 323 K. Further increase of the temperature at 333 K caused a  
734 reduction on the reaction time at 70 min with 100 % H<sub>2</sub> selectivity. Authors concluded that the  
735 Ni alloying with low Pt content and moderate temperatures are promising for the development  
736 of low-cost and high efficiency catalysts for H<sub>2</sub> production by hydrous hydrazine  
737 decomposition.

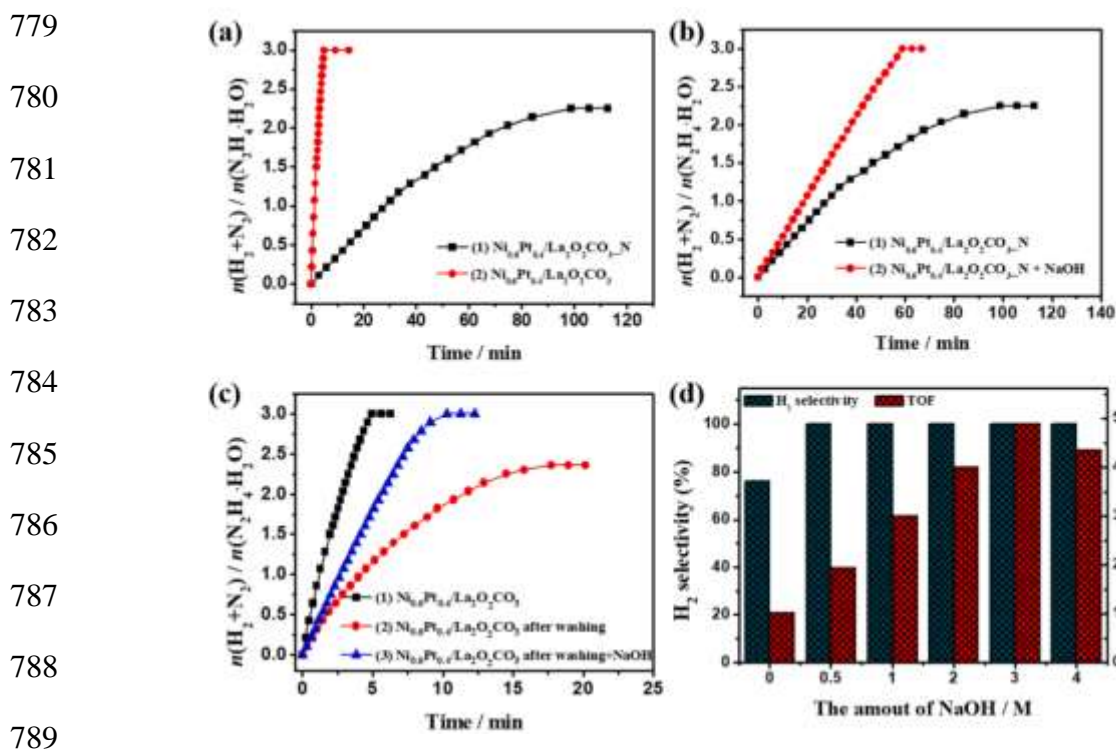
738 Ni-Ir alloy catalysts supported on Al<sub>2</sub>O<sub>3</sub> were investigated by He et al. [113] to compare its  
739 activity and selectivity with monometallic Ir/Al<sub>2</sub>O<sub>3</sub> and Ni/Al<sub>2</sub>O<sub>3</sub> catalysts. NiIr<sub>0.016</sub>/Al<sub>2</sub>O<sub>3</sub> (2.0  
740 wt % Ir, 36.8 wt % Ni and 6.1 wt % Al<sub>2</sub>O<sub>3</sub>) increased the selectivity up to 99 % and the reaction  
741 rate was 6.3 h<sup>-1</sup>. Increasing the Ir molar ratio to Ni up to 0.059, the reaction rate was enhanced  
742 at 12.4 h<sup>-1</sup> and selectivity remained higher than 98%. The stability of the NiIr<sub>0.059</sub>/Al<sub>2</sub>O<sub>3</sub> was  
743 tested at 10 consecutive cycles at 30 °C. The reaction rate decreased to 9.2 h<sup>-1</sup> but the H<sub>2</sub>  
744 selectivity remained over 98%. Reduction of the catalyst at high temperatures resulted in a  
745 decreased selectivity and catalytic activity. Moreover, modified Au and Pt Ni/Al<sub>2</sub>O<sub>3</sub> catalysts  
746 were developed for comparison purposes. NiPt<sub>0.027</sub>/Al<sub>2</sub>O<sub>3</sub> exhibited high selectivity while  
747 NiAu<sub>0.020</sub>/Al<sub>2</sub>O<sub>3</sub> resulted in a lower selectivity and reaction rate as low as 2.0 h<sup>-1</sup>.

748 Furthermore, experiments showed that alkaline conditions lead to improved H<sub>2</sub> selectivity.  
749 Bimetallic nano-catalysts were developed by alloying Ni and Fe with different Ni/Fe molar  
750 ratios by Singh et al. [114] to investigate their catalytic performance for the decomposition of  
751 hydrous hydrazine. Even though the catalyst exhibited excellent catalytic activity, the  
752 selectivity towards H<sub>2</sub> was only 81 %. With an addition of 0.5 M NaOH the selectivity was  
753 enhanced at 100%. The addition of NaOH also improved the selectivity of the Ni<sub>45</sub>Pt<sub>55</sub> and

754 Ni<sub>50</sub>Ir<sub>50</sub> catalysts from 61 to 86 % and from 7 to 95 % respectively. It was suggested by the  
755 authors that the basicity of the NaOH makes the surface of the catalyst basic preventing the  
756 formation of NH<sub>3</sub> by the incomplete decomposition of hydrazine and thus promoting the first  
757 pathway. Weaker bases such as ammonia and sodium acetate were also examined. Results  
758 showed that the addition of these bases had no effect on the catalytic activity and selectivity of  
759 the catalysts.

760 Ni particles were synthesised from the reduction of triangular Ni(HCO<sub>3</sub>)<sub>2</sub> nanosheets and were  
761 used as catalysts to produce H<sub>2</sub> by hydrous hydrazine by Wang et al [115]. For the restraint of  
762 the NH<sub>3</sub> formation as a side reaction, the effect of NaOH concentration was tested. It was found  
763 that with the absence of NaOH the selectivity towards H<sub>2</sub> was 64.5 %. With 0.5M of NaOH,  
764 the selectivity was up to 100 % and remained unchanged with further increase of the NaOH  
765 concentration. Alkaline conditions speed up the rate determining step of the hydrous hydrazine  
766 decomposition and OH<sup>-</sup> ions inhibit the formation of ammonia obtaining 100 % H<sub>2</sub> selectivity.

767 Ni-Pt alloy nanoparticles supported on La<sub>2</sub>O<sub>2</sub>CO<sub>3</sub> were developed via an alkali assisted  
768 reduction by Yao et al [116]. Among the catalysts tested the Ni<sub>0.6</sub>Pt<sub>0.4</sub>/La<sub>2</sub>O<sub>2</sub>CO<sub>3</sub> (2.8 nm)  
769 obtained the best catalytic performance with a TOF number of 490 h<sup>-1</sup> and 100 % H<sub>2</sub> selectivity.  
770 After five rounds, the catalyst showed a good stability with only a slight aggregation of 3.4 nm.  
771 Further tests were conducted for the evaluation of NaOH effect at the synthesis of the catalysts  
772 and during the catalytic process. The catalyst prepared without the addition of NaOH exhibited  
773 much lower selectivity and catalytic performance even though NaOH was added during the  
774 decomposition reaction. Moreover, the catalyst was synthesised at different NaOH  
775 concentrations (0-4 M) and results showed that the efficiency of the catalyst increased until the  
776 NaOH concentration was 3 M. These results suggest that NaOH affects both the catalytic  
777 process and the preparation of the catalysts. The effect of the NaOH addition at the preparation  
778 step of the catalyst and during the process are presented below (Fig. 6).



790 Fig. 6. The effect of NaOH addition in the catalytic decomposition of  $\text{N}_2\text{H}_4 \cdot \text{H}_2\text{O}$  [116].

791 Huang and Liu [117] examined both the synergistic effect from an Ni alloy and the addition of  
 792 NaOH to generate  $\text{H}_2$  from hydrous hydrazine. Ni-Pt/C catalysts were synthesised with various  
 793 Pt/Ni molar ratios. The optimal catalytic activity was displayed by  $\text{Ni}_8\text{Pt}_1/\text{C}$  and used for further  
 794 studies with respect to different catalyst concentrations, initial  $\text{N}_2\text{H}_4$ , temperature and NaOH  
 795 concentration. With an increase on the catalyst concentration and initial  $\text{N}_2\text{H}_4$  the  
 796 dehydrogenation rate also increased. The catalytic activity slightly decreased after 5 catalytic  
 797 runs and characterization results showed that the average grain size of the reused catalyst  
 798 increased from 2.5 nm to 3.8 nm. At higher temperatures a higher TOF value was obtained.  
 799 Lastly, with an addition of 0.5 M NaOH, a TOF value of  $2640.5 \text{ h}^{-1}$  and 100 %  $\text{H}_2$  selectivity  
 800 were obtained at  $50^\circ\text{C}$ , while with no addition of the alkaline solution the TOF value was  $627.5$   
 801  $\text{h}^{-1}$ .

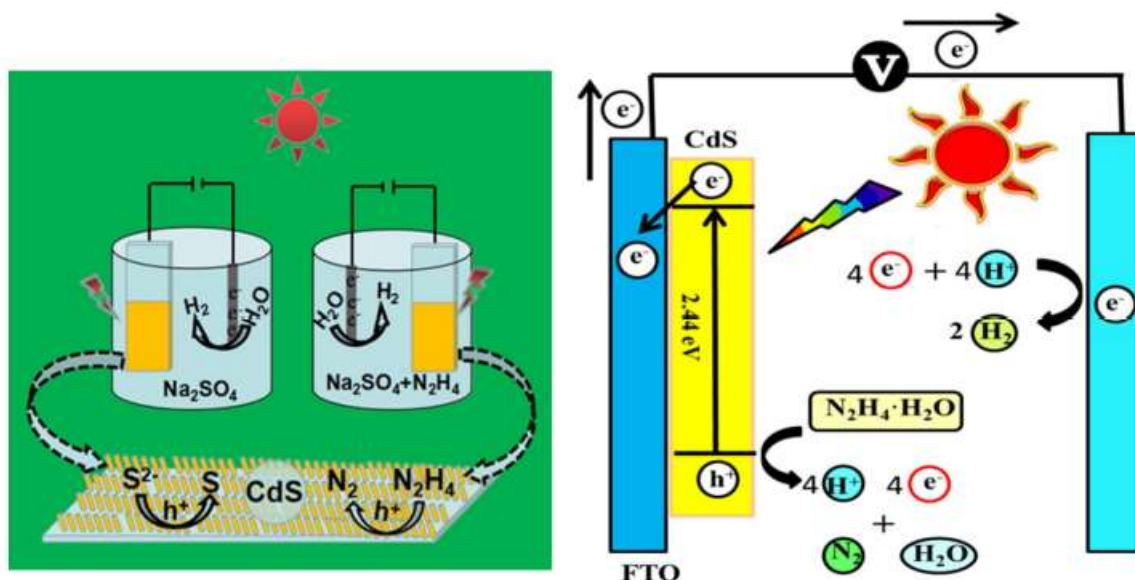
## 802 5.2 Photocatalysis and Electrocatalysis of Hydrous Hydrazine

803 The catalytic decomposition of hydrous hydrazine for the generation of  $\text{H}_2$  is well investigated,  
 804 but its photocatalytic decomposition still needs lots of research for the discovery of efficient  
 805 photocatalysts.  $\text{TiO}_2$  modified with deposition of noble metals is found to be very promising  
 806 as for the photocatalytic oxidation of hydrazine and its derivatives [118, 119].  $\text{TiO}_2$

807 nanoparticles modified with rhodium were developed by Kumar et al. [120] for the  
808 photocatalytic decomposition of hydrous hydrazine under visible light irradiation. Unmodified  
809 TiO<sub>2</sub> particles exhibited a H<sub>2</sub> production of 83 μmol g<sup>-1</sup> cat and formation rate of 6.9 μmol g<sup>-1</sup>  
810 cat h<sup>-1</sup> while TiO<sub>2</sub>-Rh had a H<sub>2</sub> production of 413 μmol g<sup>-1</sup> cat and rate formation 42.0 μmol g<sup>-1</sup>  
811 cat h<sup>-1</sup> after 12 h of visible light irradiation. The photocatalyst was still efficient after five  
812 subsequent runs and the H<sub>2</sub> yield was 384 μmol g<sup>-1</sup> cat but it was noticed a slight decrease in  
813 the photoactivity due to leaching of the Rh from the TiO<sub>2</sub> surface. After the five cycles, the  
814 value of Rh was 0.14 wt %, slightly lower than that of the fresh catalyst (0.16 wt %).

815 Noble metals such as Pt, Pd and Au were used as electrodes for the electrooxidation of  
816 hydrazine to N<sub>2</sub> and H<sub>2</sub> but their high price makes them not practical to use for further  
817 applications [121, 122]. Silver nano-catalysts Ag@C<sub>60</sub> were synthesised by Narwade et al.  
818 [123] to investigate the electrocatalytic activity for the oxidation of hydrazine for H<sub>2</sub>  
819 production. The electrocatalyst was also tested for its efficiency in a range of pH solutions. The  
820 best electrochemical performance and long-term stability was exhibited by the Ag@C<sub>60</sub>  
821 catalyst in a 0.5 M KOH solution. It was concluded that the enhanced electrocatalytic activity  
822 of the Ag@C<sub>60</sub> is a result of the synergistic effect of Ag nanoparticles and C<sub>60</sub>.

823 A new method studied recently is the photoelectrocatalysis, a combination of photocatalysis  
824 and electrocatalysis. Thus, photoelectrochemical (PEC) H<sub>2</sub> production from N<sub>2</sub>H<sub>4</sub>.H<sub>2</sub>O was  
825 studied by Yan et al. [124] using CdS nanorod arrays as the photoelectrode. The proposed  
826 mechanism is presented below in Fig. 7. Under visible-light irradiation the photoelectrode in  
827 electrolytes with N<sub>2</sub>H<sub>4</sub>.H<sub>2</sub>O presented great stability after 100 h of the reaction while when  
828 there were no electrolytes the persistence of the device was less than 100 s. Moreover, the  
829 efficiency of the photoelectrode remained the same with a H<sub>2</sub> selectivity over 90 %. The results  
830 that were obtained from the CdS photoelectrode promote the PEC H<sub>2</sub> production for further  
831 studies and applications. Table 4 summarises the results from the experiments mentioned  
832 above.



833 Fig. 7. Proposed mechanism of the photoelectrochemical decomposition on CdS nanorod  
 834 catalysts [124].

835 Table 4. Photocatalysts and Electrocatalysts used for hydrous hydrazine decomposition.

Photocatalysis				
Catalyst	H <sub>2</sub> Yield (μmol)	Reference		
Au/TiO <sub>2</sub>	48.5	[118]		
Pd/SiO <sub>2</sub>	1.5	[119]		
TiO <sub>2</sub> -Rh		[120]		
Electrocatalysis				
Catalyst	System	Onset Potential	Current Density (mA cm <sup>-2</sup> )	Reference
Ni <sub>60</sub> Co <sub>40</sub>	1.0 M KOH + 0.1 M N <sub>2</sub> H <sub>4</sub> ·H <sub>2</sub> O	1.56 V vs RHE		[121]
Ni/CB	0.1 M NaOH + 0.1 M N <sub>2</sub> H <sub>4</sub>	0.9245 V vs RHE		[122]
Ag@C <sub>60</sub>	0.5 M KOH + 0.5 mL N <sub>2</sub> H <sub>4</sub>	0.8 V vs SCE	112	[123]
Photoelectrocatalysis				
CdS NRs	0.1 M Na <sub>2</sub> SO <sub>4</sub> + 0.378 M N <sub>2</sub> H <sub>4</sub> ·H <sub>2</sub> O	1.23 V vs RHE	7.6	[124]

836

## 837 **6 Reactors for NH<sub>3</sub> decomposition**

### 838 **6.1 Membrane reactors**

839 Catalytic membrane reactors (CMRs) are frequently used for the decomposition of ammonia  
840 because they offer several advantages. They shift the thermodynamic equilibrium due to the  
841 removal of H<sub>2</sub> allowing the process to proceed at lower temperatures reaching full conversion.  
842 Moreover, they do not require an additional separation unit, since separation and purification  
843 occur in a single unit, lowering the cost of the system and providing pure H<sub>2</sub>. The process is  
844 usually assisted by an inert sweep gas that might dilute H<sub>2</sub> stream, which is unwanted. The  
845 most suitable materials are Palladium or/and its alloys but their challenging scale-up and high  
846 cost limit this technology and therefore new materials must be explored [125].

847 Numerical simulations for ammonia decomposition in a catalytic membrane reactor filled with  
848 Ni/Al<sub>2</sub>O<sub>3</sub> catalytic particles were studied by Di Carlo et al [126]. The focus of the study was  
849 the evaluation of the improvement of the ammonia decomposition with the use of Pd coated  
850 membranes. Firstly, a 2D study was investigated without membranes and results showed that  
851 at temperature of 550 °C, pressure of 0.2 MPa and low flow velocity of 2cm/s the ammonia  
852 conversion was extremely good with a residual NH<sub>3</sub> of only a few ppm. The 3D simulations  
853 were studied with the addition of Pd-membranes at 1MPa and temperature range of 500-600  
854 °C. At 550 °C NH<sub>3</sub> conversion was 99.9% improving almost 18 % the conversion rate that was  
855 obtained without the membranes.

856 A tube-wall catalytic membrane reactor containing a Pd membrane alloyed with Ag (Pd<sub>77</sub>Ag<sub>23</sub>)  
857 was developed by Itoh et al. [127] for the decomposition of ammonia at temperatures below  
858 400 °C. A Ru catalyst was used, and the optimal loading was 2 wt % due to the high dispersion  
859 on the surface area. A 2 wt % Ru/Al<sub>2</sub>O<sub>3</sub> packed bed reactor was compared with the membrane  
860 reactor loaded with 2 wt % of Ru and it was found that the latter achieved a higher conversion  
861 (about 15% higher) because of the larger heat flux in the tube reactor. The reactor with 2 mm  
862 thick Pd membrane achieved 100 % NH<sub>3</sub> conversion at 375 °C and ammonia feed rate of 10  
863 mL/min.

864 Abashar et al. [128] simulated multi-stage Pd-Ag membrane reactors for the generation of ultra-  
865 pure H<sub>2</sub>. In comparison with a single stage reactor that achieved 29.49 % ammonia conversion  
866 the seven-stage membrane reactor exhibited complete conversion of ammonia at 40 bar.

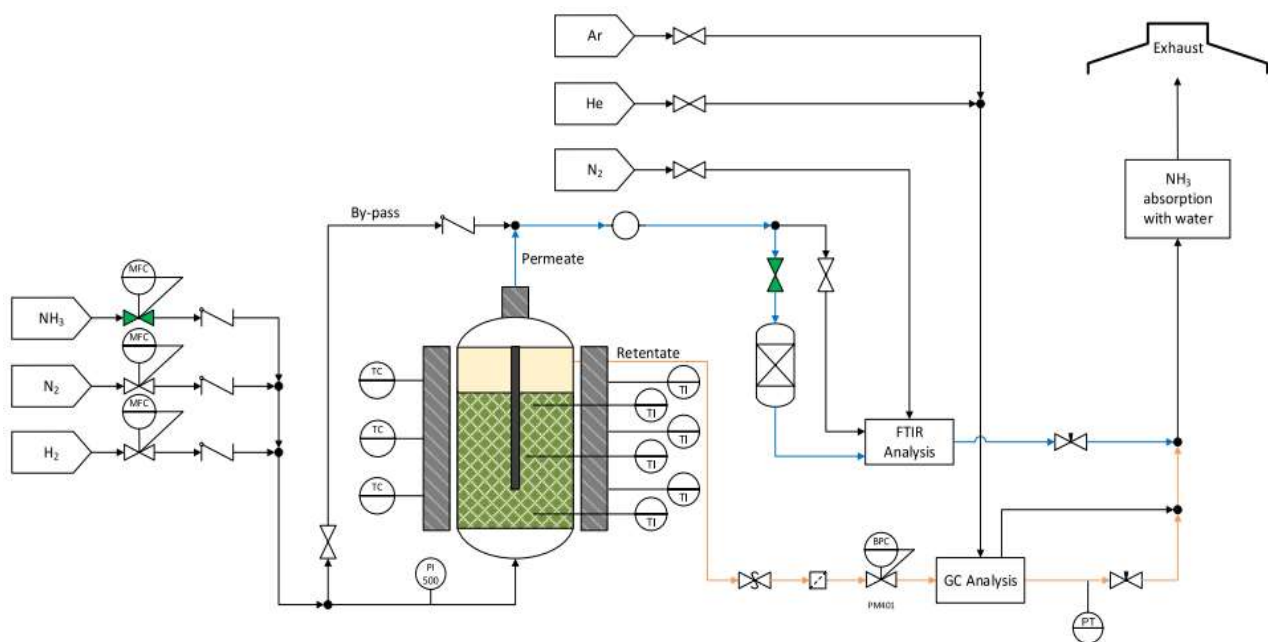


867 Moreover, a multi-stage fixed bed reactor was modelled under the same conditions and the exit  
868 ammonia conversion was 92.37 % suggesting that a multi-stage membrane reactor is superior.  
869 The numerical results demonstrated a promising performance of the membrane reactor and  
870 even though they were not confirmed experimentally they might have fundamental importance  
871 for further design and optimization of the reactor and the process.

872 Co-based catalysts combined with Pd-Au alloy membranes were demonstrated by Cerrillo et  
873 al. [129] for the decomposition of ammonia to the production of high purity H<sub>2</sub>. Experiments  
874 were carried out with and without the addition of the membrane and results showed that the  
875 membrane drastically enhances the conversion of NH<sub>3</sub>. The purity of H<sub>2</sub> was > 99.97 % for  
876 over 1000 h of running stream. Moreover, the ammonia conversion increased when the  
877 temperature, pressure and contact time increased.

878 Cechetto et al. [130] experimentally demonstrated ammonia decomposition in a catalytic  
879 membrane reactor (Fig. 8). The catalyst was Ru-based with double-skin Pd-based membranes.  
880 The main focus of the experiments was the purity of H<sub>2</sub> produced in the membrane reactor  
881 technology. Results showed that with an increase of the thickness of the membrane above 6  
882 μm ultra-pure H<sub>2</sub> can be generated. Also, a small purification unit can be installed as a more  
883 economic feasible solution in contrast with the increase of the membrane thickness. More  
884 specifically, a bed of 13X zeolite was tested and it was concluded that it's a suitable sorbent  
885 for H<sub>2</sub> purification.

886



887 Fig. 8. Process flow diagram of the experimental setup [130].

888 In addition to that, membranes are required to be free of defects to achieve high H<sub>2</sub> purity.  
889 Alternative materials to Pd that have been already used are Vanadium, and Ni alloys. A 3D  
890 CFD model was developed by Shwe Hla and Dolan [131] for the examination of the  
891 performance of a Vanadium-based alloy membrane reactor for H<sub>2</sub> generation and separation  
892 by ammonia decomposition. At 30 L/min NH<sub>3</sub> inlet flow rate, pressure of 7.8 bar<sub>a</sub> and 300 °C,  
893 a conversion of 90 % NH<sub>3</sub> was achieved and H<sub>2</sub> yield over 95 % within a shorter distance along  
894 membrane tubes. As expected, at lower inlet flow rates, H<sub>2</sub> yield was higher due to a longer  
895 residence time. The effects of the membrane permeability on the H<sub>2</sub> yield were tested under  
896 different percentages of the original value. At only 50 % functionality the H<sub>2</sub> yield was similar  
897 with that obtained at 100 % membrane permeability.

898 A double layered Nd<sub>5.5</sub>Mo<sub>0.5</sub>W<sub>0.5</sub>O<sub>11.25-δ</sub> (NMW)/ Nd<sub>5.5</sub>Mo<sub>0.5</sub>W<sub>0.5</sub>O<sub>11.25-δ</sub>-Ni (NMW-Ni)  
899 membrane was synthesised by Cheng et al. [132] for the on-site H<sub>2</sub> production by catalytic  
900 ammonia decomposition. NMW-NiO layer served as the catalytic reaction site while the NMW  
901 layer provided the separation of H<sub>2</sub>. A sweep gas of N<sub>2</sub> was used and NH<sub>3</sub> conversion of 99 %  
902 was obtained at 750 °C, 24% higher than that of a packed bed reactor that was achieved under  
903 the same conditions, given to the simultaneous removal of the H<sub>2</sub>. Moreover, the highest  
904 conversion may be attributed to the longer length of the membrane reactor. It was noticed that  
905 NH<sub>3</sub> conversion was higher at lower NH<sub>3</sub> flow rates in the feed stream due to a higher residence  
906 time of ammonia in the reactor, whereas H<sub>2</sub> production was small due to a slower composition  
907 rate, indicating the need to improve ammonia decomposition at high feed flow rates. After 75  
908 h of reaction at 750 °C, the membrane reactor maintained a high conversion of 91 % achieving  
909 high long-term stability.

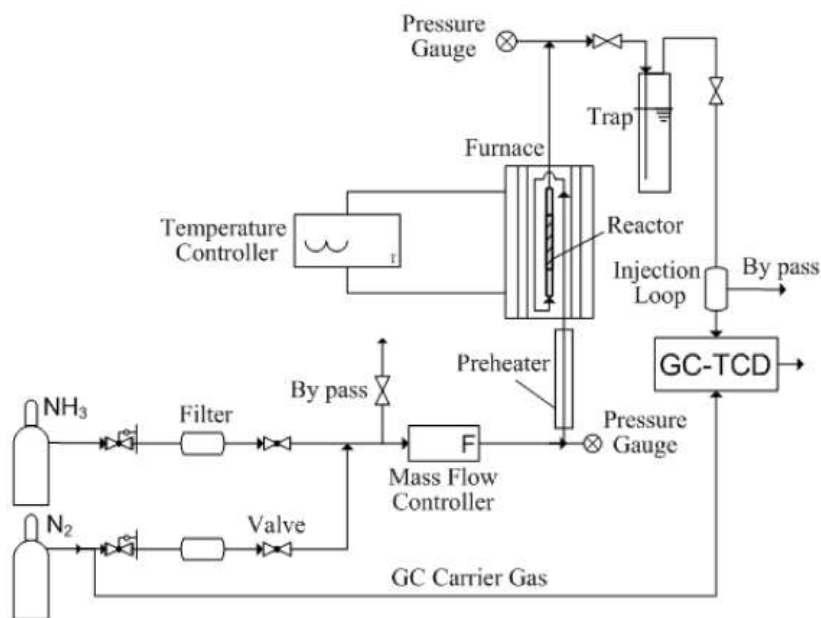
910 Ru particles dispersed on yttria-stabilized zirconium (YSZ) coated by a Pd film, were  
911 developed by Zhang et al. [133] to utilize them for H<sub>2</sub> production by the decomposition of NH<sub>3</sub>.  
912 The reaction took place in a catalytic membrane reactor. Different parameters such as  
913 temperature, pressure and inlet flow were tested to evaluate the reactor performance. An  
914 addition of Cs promoter caused complete decomposition of NH<sub>3</sub> at temperatures of 400 °C and  
915 volumetric H<sub>2</sub> productivity of 31.6 mol m<sup>-3</sup> s<sup>-1</sup>. Both the catalyst and the membrane were found  
916 to eliminate any transport resistances resulting in a decreased operation temperature, reduced  
917 catalyst content and higher H<sub>2</sub> productivity in contrast with a PBMR. Also, a reactor model  
918 was developed to better understand the performance of the reactor. The experimental results

919 were in a great agreement with the model at all conditions, validating the first-order kinetics  
920 and the efficiency of the CMR.

## 921 **6.2 Fixed Bed Reactors**

922 Fixed bed reactors (FBRs) have many large-scale applications in the industry. One great  
923 advantage is that the catalyst is immobilized, and the reactant mixture is technically forced to  
924 be in contact with it. Though, due to its poor mixing properties large temperature gradients  
925 occur and therefore, the extent of the ammonia decomposition can be reduced [134].

926 Commercial 5 wt% Ru/C catalyst on different promoter Cs loadings was studied  
927 experimentally by Chen et al. [135] in a fixed bed reactor for the decomposition of ammonia.  
928 The experimental setup that was used in this work is demonstrated in Fig. 9. The optimum  
929 Cs/Ru molar ratio was 4.5 and further increase than that resulted in a decrease on the conversion  
930 of ammonia. At 400 °C ammonia conversion was nearly 100 %.



940 Fig. 9. Schematic diagram of the process for ammonia decomposition in a fixed bed reactor  
941 [135].

942 Gu et al. [136] developed Ni-based catalysts supported in porous alumina (Ni@Al<sub>2</sub>O<sub>3</sub>) via a  
943 simple one-pot method for the decomposition of ammonia. The Ni content was adjusted from  
944 5 at.% to 25 at.% and the reaction took place in a fixed bed reactor. The catalyst with the highest  
945 nickel content (25 at. %) exhibited the highest ammonia conversion of 93.9 % at 600 °C and  
946 almost full conversion (99.1 %) at 650 °C. H<sub>2</sub> formation rate reached up to 7.8 mmol gcat<sup>-1</sup>

947  $\text{min}^{-1}$  at 450 °C. There was an increase in the crystallite size of Ni particles from 1 nm (fresh)  
948 to 6 nm (used) due to high reaction temperature. The high catalytic performance could be  
949 attributed by the strong interaction amongst the mesoporous alumina matrix and nickel  
950 particles that can prevent the metallic Ni from sintering into large aggregates and the high  
951 dispersion of Ni particles.

952 A fixed bed plug flow reactor was used by Morlanés et al. [137] for the decomposition of  
953 ammonia by Ba-CoCe catalysts with various Co/Ce molar ratios. When catalysts were prepared  
954 by impregnation it was noticed that above 20 % of Co loading decreased the conversion of  
955 ammonia, while when they were prepared via coprecipitation the opposite trend was found  
956 since 30 % Co content catalysts showed higher activity. The high activity could be attributed  
957 to the coprecipitation method that allowed higher amounts of Co incorporated in the catalyst.  
958 The optimum performance was from the 0.5Ba/CoCe(80/20) catalyst with 41.4 wt % Co, 23.5  
959 wt % Ce and 0.45 wt % Ba, whose catalytic activity was comparable with Ru-based catalysts.  
960 At 450 °C it exhibited a conversion little bit lower than 80 %. Ce as a promoter, increased Co  
961 dispersion and prevented sintering and aggregation.

962 Ru nanoparticles were supported on alkali silicates ( $\text{Ru}/\text{A}_2\text{SiO}_3$ , A = Li, Na and K) by Zhiqiang  
963 et al. [138] The catalytic reaction occurred in a fixed bed reactor at atmospheric pressure.  
964  $\text{Ru}/\text{K}_2\text{SiO}_3$  (3.21 wt % Ru) showed the best catalytic performance with an  $\text{NH}_3$  conversion of  
965 60.5 %,  $\text{H}_2$  formation rate of  $20.3 \text{ mmol g}_{\text{cat}}^{-1}\text{min}^{-1}$  and TOF value of  $2.03 \text{ s}^{-1}$  at 450 °C. A series  
966 of K- promoted catalysts were prepared to evaluate the effect of the K content but results  
967 showed that the highest ammonia conversion was the one already exhibited by  $\text{Ru}/\text{K}_2\text{SiO}_3$ . In  
968 comparison with other works that used Ru particles supported on other silicon materials at the  
969 same conditions,  $\text{Ru}/\text{K}_2\text{SiO}_3$  achieved higher performance due to a better promotion effect of  
970 the alkali metal silicates. It was concluded by the authors that the formation of oxygen  
971 vacancies on the alkali metal silicates can stabilize the Ru nanoparticles with strong metal  
972 support interactions that results in an increase of the number of active sites.

973 Ni-Ru/ $\text{CeO}_2$  catalysts with several metal loadings were prepared by Lucentini et al. [139] and  
974 tested for the  $\text{H}_2$  generation from the decomposition of ammonia. The catalytic tests were  
975 carried in a fixed bed reactor and results showed that the best catalytic performance was  
976 observed by 0.4-0.6 wt% Ru and 2.4-5.0 wt % Ni. After 100 h of continuous operation the  
977 catalysts exhibited excellent long-term stability. At 400 °C, TOF values exceeding  $2 \text{ s}^{-1}$  were  
978 obtained. With the use of Langmuir-Hinshelwood-Hougen-Watson approach, a kinetic model

979 was developed for the simulation of the H<sub>2</sub> production rate under different parameters. Lastly,  
980 it was concluded that the limiting step for the reaction is the dehydrogenation of ammonia  
981 adsorbed on the surface of the catalysts.

982 In addition to the previous research Lucentini et al. [140] continued the investigation on the  
983 decomposition of ammonia on Ni-Ru catalysts supported on 3D-printed CeO<sub>2</sub> structures in a  
984 fixed bed reactor. The Ni<sub>0.5</sub>Ru<sub>0.1</sub> catalyst achieved the best catalytic performance and therefore  
985 was used for the rest of the study. Moreover, a 1D mathematical model was developed over the  
986 3D-printed catalytic structure loaded with Ni-Ru catalysts. A comparison between the  
987 experimental results and the simulation validated the model that was developed. For the  
988 optimisation of the catalytic structure, a series of simulations were performed with different  
989 geometric parameters to examine their effect on the catalytic performance in ammonia  
990 decomposition. Specifically, the geometric parameters that were optimized were the wall  
991 thickness, the number and width of channels for better and more efficient usage of the reactor  
992 with the intention of on-site generation H<sub>2</sub> and usage in a PEM-type fuel cell.

993 Co<sub>3</sub>Mo<sub>3</sub>N and  $\gamma$ -Mo<sub>2</sub>N catalysts were synthesised with the use of citric acid as a chelating agent  
994 by Jolaoso et al. [141]. The catalytic tests were performed in a fixed bed quartz tube reactor at  
995 atmospheric pressure, a temperature range of 300-600 °C and constant GHSV of 6000 h<sup>-1</sup>. At  
996 550 °C,  $\gamma$ -Mo<sub>2</sub>N catalyst gave 71.9 % NH<sub>3</sub> conversion while Co<sub>3</sub>Mo<sub>3</sub>N gave 97.3 % resulting  
997 in a better catalytic performance indicating that Co particles promote the ammonia  
998 decomposition. Characterization tests showed that Co<sub>3</sub>Mo<sub>3</sub>N catalyst contained 33.72 wt %,   
999 54.41 wt % and 4.03 wt % Co, Mo and N respectively. After 35 h of a continuous test the  
1000 catalyst showed no deactivation. This was validated by measuring the crystallite size of the  
1001 fresh catalyst (6.20 nm) and the used catalyst (6.19 nm) whereas no significant decrease was  
1002 obtained. Conversion of 100 % was obtained by both catalysts at 600 °C.

1003 Another study conducted in a fixed bed reactor, implemented three Ru-supported catalysts  
1004 (Ru/Al<sub>2</sub>O<sub>3</sub>, Ru/La<sub>2</sub>O<sub>3</sub>-Al<sub>2</sub>O<sub>3</sub> and Ru/La<sub>2</sub>O<sub>2</sub>CO<sub>3</sub>-Al<sub>2</sub>O<sub>3</sub>). Kim et al. [142] examined their  
1005 catalytic activity at a low temperature range of 350-500°C. The best catalytic activity was  
1006 established by Ru/La<sub>2</sub>O<sub>2</sub>CO<sub>3</sub>-Al<sub>2</sub>O<sub>3</sub> (11.5 wt % La and 0.95 wt % Ru) with 80.1 % NH<sub>3</sub>  
1007 conversion at 500 °C. Even though characterization tests showed that Ru/Al<sub>2</sub>O<sub>3</sub> had higher Ru  
1008 dispersion (27.3 %) than Ru/La<sub>2</sub>O<sub>3</sub>-Al<sub>2</sub>O<sub>3</sub> (20.6 %) it resulted in a lower catalytic activity  
1009 suggesting that the La addition promoted electron donation from La to Ru particles due to their  
1010 electronegativity difference and therefore increasing the kinetics of the reaction. Moreover, the

1011 La oxycarbonate-rich surface favoured the formation of Ru particles on the surface of the  
1012 catalyst preventing the particles to leave from the surface into the bulk phase. Thus, it was  
1013 concluded that the  $\text{La}_2\text{O}_2\text{CO}_3$  surface coating might be beneficial for catalyst synthesis when  
1014 an increased surface metal concentration is needed.

### 1015 **6.3 Microreactors**

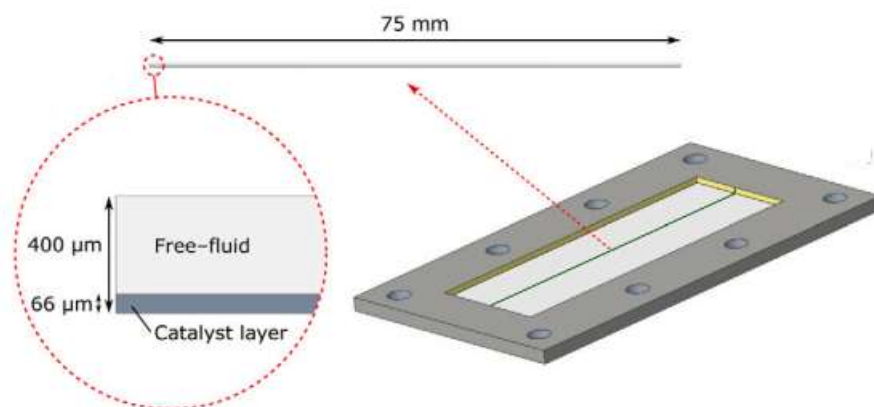
1016 Microreactors gained attention in the early 1990s marking them as a relatively new field.  
1017 Microreactor technology offers better control, high surface area ratios, high heat and mass  
1018 transfer rates and enhanced conversion efficiency. Compared with conventional reactors, micro  
1019 structured reactors exhibited higher activity towards  $\text{NH}_3$  ammonia decomposition [143].

1020 An autothermal microchannel reactor was evaluated for the decomposition of ammonia to  
1021 generate  $\text{H}_2$  and provide it for power generation systems. Engelbrecht, Chiuta and Bessarabov  
1022 [144] studied the effects of different parameters such as  $\text{NH}_3$  decomposition flow rate and  
1023 oxidation flow rate and fuel-oxygen equivalence ratio to find the optimal operation parameters.  
1024 The catalyst for decomposition was 8.5 wt %  $\text{Ru}/\text{Al}_2\text{O}_3$  and for the oxidation was 5 wt %  
1025  $\text{Pt}/\text{Al}_2\text{O}_3$ . A conversion up to 99.8% was observed with a  $\text{H}_2$  equivalent fuel power of 0.71  
1026  $\text{kWe}$ , when the decomposition flow rate was 6  $\text{NL min}^{-1}$ , the oxidation flow rate was 4  $\text{NL}$   
1027  $\text{min}^{-1}$  and the fuel-oxygen ratio was 1.4. A stability test was also carried out for 24 h in  
1028 demanding reactor conditions to determine any inconsistencies in the catalyst where results  
1029 showed that no deactivation of the catalyst occurred during reaction. It was concluded that the  
1030 performance of the reactor was good and further research might be able to up-scale this system  
1031 for multi-kW power generation systems.

1032 Based on the experimental results obtained from Engelbrecht, Chiuta and Bessarabov [144], a  
1033 3D CFD model was developed by Schumacher et al. [145] to study both steady-state and  
1034 transient regimes in a microchannel reactor to provide a suitable mathematical model. In  
1035 consideration of the wide range of ammonia decomposition and oxidation flow rates and  
1036 temperature profiles, the simulation fitted the experimental data with an acceptable accuracy.  
1037 It was found that at the microreactor inlet the highest temperature was obtained and therefore  
1038 a different solution needed to be developed to solve the model with regard in the distribution  
1039 of heat transfer. Therefore, any future reactor designs should be focused on the optimization of  
1040 the heat transfer rate.

1041 3D printed SiCN monolithic ceramic microreactors and Ru catalysts were used by Gyak et al.  
1042 [146] for ammonia decomposition at high temperature. A temperature range of 500-1000 °C  
1043 and different flow rates of 2, 4 and 8 mL min<sup>-1</sup> were the conditions for the catalytic reaction.  
1044 At 2 mL min<sup>-1</sup> and 1000 °C, ammonia was completely decomposed due to an increased  
1045 residence time. After 48 h of exposure to ammonia and 1000 °C, the ceramic microreactors  
1046 demonstrated excellent chemical resistance and heat tolerance.

1047 Maleki, Fulton and Bertola [147] designed a microreactor, both experimentally and  
1048 numerically for H<sub>2</sub> production via low temperature ammonia decomposition over  
1049 Co<sub>0.5</sub>Ce<sub>0.1</sub>Al<sub>0.4</sub>O(sa) catalyst. The geometries of the microchannel are presented in Fig. 10. Two  
1050 kinetic models were used to describe the reaction, a pseudo-first order model and a modified  
1051 Temkin-Pyzhev model that were compiled in a CFD model. The model then was solved at a  
1052 various NH<sub>3</sub> flow rates and temperatures and exhibited good agreement with the experimental  
1053 data. At a lower temperature range the Temkin-Pyzhev model had better accuracy than the first  
1054 model and therefore was selected for further study. Higher conversion rates were obtained  
1055 while increasing the temperatures whereas over 99 % was observed at temperatures of 550 °C.



1062 Fig. 10. 2D and 3D geometries of the microreactor [147].

1063 Bimetallic Ru-Fe alloy catalysts were synthesised and impregnated with carbon nanotubes by  
1064 Chen et al. [148] The experiments took place in a fixed bed microreactor at a temperature range  
1065 of 300-500 °C and atmospheric pressure. The Ru<sub>3</sub>Fe/CNTs catalyst (1.67 wt % Ru, 0.31 wt %  
1066 Fe) presented the best catalytic performance in contrast with the Ru/CNTs catalyst. At 500 °C  
1067 both catalysts resulted in a 100 % ammonia conversion. After 60 h of reaction, the activity of  
1068 Ru/CNTs was decreased by 30 % while that of Ru<sub>3</sub>Fe/CNTs decreased only 10 % exhibiting  
1069 superior stability with the addition of Ru. It was concluded that the alloy synergistic effect

1070 between Ru and Fe enhanced the catalytic activity and furthermore the addition of the non-  
 1071 noble metal Fe reduces the content of Ru resulting in a lower catalyst cost.

1072 Table 5. A summary of the type of reactors used for ammonia decomposition.

Type of reactor	Catalyst	Temperature	Conversion	Yield	TOF	Reference
Pd membrane reactor	Ni/Al <sub>2</sub> O <sub>3</sub>	550	99.9			[126]
Pd membrane reactor	2%Ru/Al <sub>2</sub> O <sub>3</sub>	375	100			[127]
Pd-Ag membrane reactor			100			[128]
Pd-Au membrane reactor	Co			99.97		[129]
Double-skin Pd membrane reactor	Ru			93.2		[130]
Vanadium alloy membrane reactor		300	90	>95		[131]
NMW/NMW-NiO	NMW-NiO powder	750	99			[132]
YSZ/Pd membrane reactor	Ru	400	93	90		[133]
Fixed bed reactor	5%Ru/C	400	~100			[135]
Fixed bed reactor	25%Ni@Al <sub>2</sub> O <sub>3</sub>	650	99.1			[136]
Fixed bed reactor	0.5Ba/CoCe(80/20)	450	74		0.602	[137]
Fixed bed reactor	Ru/K <sub>2</sub> SiO <sub>3</sub>	450	60.5		2.03	[138]
Fixed bed reactor	Ni-Ru/CeO <sub>2</sub>	400			2	[139]
Fixed bed reactor	Ni-Ru/CeO <sub>2</sub>					[140]
Fixed bed reactor	Co <sub>3</sub> Mo <sub>3</sub> N	550	97.3			[141]
Fixed bed reactor	Ru/La <sub>2</sub> O <sub>2</sub> CO <sub>3</sub> -Al <sub>2</sub> O <sub>3</sub>	500	80.1			[142]
Microreactor	8.5%Ru/Al <sub>2</sub> O <sub>3</sub>	651	99.8			[144]
Microreactor – Experimental	Ru/Al <sub>2</sub> O <sub>3</sub>	300	99.9			[145]
Microreactor – Simulation	Ru/Al <sub>2</sub> O <sub>3</sub>	300	99.9			[145]
Microreactor	Ru	1000	100			[146]
Microreactor	Co <sub>0.5</sub> Ce <sub>0.1</sub> Al <sub>0.4</sub> O(sa)	550	99			[147]
Microreactor	Ru <sub>3</sub> Fe/CNTs	500	100		86.21	[148]

1073 As seen from Table 5 membrane reactors and microreactors are superior to fixed bed reactors.  
 1074 Even though membrane reactors are well studied, the most common membrane used is Pd and  
 1075 its alloys [126–130], [133], which is rare and expensive and needs to be replaced with other  
 1076 elements that give off such high catalytic activity and selectivity. Regarding fixed bed reactors,  
 1077 a number of studies give promising results but most of them presented low conversion of  
 1078 ammonia [137–139], [142]. The need for high temperatures for the decomposition makes these  
 1079 reactors unsuitable. Studies on microreactors operating experimentally and theoretically in a



1080 large range of temperatures are limited mostly for Ru-based catalysts as they present high  
1081 catalytic activity giving the opportunity for further development of a cost-effective reactor  
1082 system [145, 146], [148].

1083

## 1084 **7 Conclusions**

1085 Green energy carriers have the potential to solve the current issues related with climate change.  
1086 An emerging energy resource is H<sub>2</sub> as an alternative to non-renewable sources such as  
1087 conventional fuels. Its physical storage though, is limiting its application. Therefore, this  
1088 review provides information about ammonia and hydrous hydrazine as possible chemical  
1089 hydrogen storage compounds. Moreover, heterogeneous catalysts utilized for the  
1090 decomposition reactions of the compounds mentioned above are reviewed in contrast with their  
1091 efficiency. An issue occurring with hydrous hydrazine decomposition is ammonia formation  
1092 that can lead to corrosion and lower selectivity regarding H<sub>2</sub>. The most promising catalytic  
1093 system for ammonia decomposition is ruthenium and its alloys but it's not methodical due to  
1094 its high price and scarcity. For hydrous hydrazine, the most active catalytic system is nickel  
1095 catalysts alloyed with noble metals that are some of the most expensive metals in the world.  
1096 Thus, there is a great need for the development of cost-effective catalytic systems for both  
1097 ammonia and hydrous hydrazine, using more abundant metals instead of precious metals with  
1098 lower metal loading and higher atom efficiency. Reactor technology used for NH<sub>3</sub>  
1099 decomposition has also been presented in this review. The most common catalyst used for this  
1100 reaction is the catalytic membrane reactor. Due to the membrane, separation and purification  
1101 can occur in a single step, giving pure H<sub>2</sub> and lowering the operation cost. Palladium  
1102 membranes were found to be the most suitable materials, but future works need to take into  
1103 consideration their high cost and therefore, explore and develop other materials with the same  
1104 efficacy. Microreactors are also an attractive option due to a high activity towards NH<sub>3</sub> with  
1105 different types of catalysts, especially ruthenium and its alloys. In contrast, fixed bed reactors  
1106 presented lower activity and further research is needed for future applications and up-scaled  
1107 production of H<sub>2</sub>. In conclusion, for on-site hydrogen production by NH<sub>3</sub> and N<sub>2</sub>H<sub>4</sub>.H<sub>2</sub>O future  
1108 research must give attention to the development of low-cost catalyst with optimum catalytic  
1109 performance and great selectivity towards H<sub>2</sub>. Furthermore, it's important to consider the  
1110 reactor technology and develop systems with low operation cost and high efficiency.

1111

1112 **References**

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