

1 **Excess pressure as an analogue of blood flow velocity**

2 Matthew K. Armstrong^a, Martin G. Schultz^a, Alun D. Hughes^b, Dean S. Picone^a, J. Andrew
3 Black^c, Nathan Dwyer^c, Philip Roberts-Thomson^c, James E. Sharman^a

4 ^a*Menzies Institute for Medical Research, University of Tasmania, Australia*

5 ^b*Institute of Cardiovascular Science, University College London, London, United Kingdom*

6 ^c*Department of Cardiology, Royal Hobart Hospital, Australia*

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21 **Corresponding author:**

22 James E. Sharman

23 Menzies Institute for Medical Research, University of Tasmania

24 Private Bag 23, Hobart, 7000, AUSTRALIA.

25 Phone: +61 3 6226 4709 Fax: +61 3 6226 7704

26 Email: James.Sharman@utas.edu.au

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Introduction: Derivation of blood flow velocity from a blood pressure waveform is a novel technique which could have potential clinical importance. Excess pressure, calculated from the blood pressure waveform via the reservoir-excess pressure model, is purported to be an analogue of blood flow velocity, but this has never been examined in detail, which was the aim of this study.

Methods: Intra-arterial blood pressure was measured sequentially at the brachial and radial arteries via fluid filled catheter simultaneously with blood flow velocity waveforms recorded via Doppler ultrasound on the contralateral arm (n=98, aged 61±10, 72% male). Excess pressure was derived from intra-arterial blood pressure waveforms using pressure-only reservoir-excess pressure analysis.

Results: Brachial and radial blood flow velocity waveform morphology were closely approximated by excess pressure derived from their respective sites of measurement (median cross-correlation coefficient $r=0.96$ and $r=0.95$ for brachial and radial comparisons respectively). In frequency analyses, coherence between blood flow velocity and excess pressure was similar for brachial and radial artery comparisons (brachial and radial median coherence=0.93 and 0.92 respectively). Brachial and radial blood flow velocity pulse heights were correlated with their respective excess pressure pulse heights ($r = 0.53, p <0.001$ and $r = 0.43, p <0.001$ respectively).

Conclusion: Excess pressure is an analogue of blood flow velocity, thus affording the opportunity to derive potentially important information related to arterial blood flow using only the blood pressure waveform.

Key words: Hemodynamics, Pulse wave analysis, Invasive

Introduction

55
56 Continuous non-invasive recording of blood pressure (BP) and flow is valuable in the settings
57 of anaesthesiology, cardiology and emergency care for the hemodynamic assessment and
58 management of the critically ill. Several methods exist for recording continuous non-invasive
59 BP, many of which are straightforward to apply and nondemanding for the operator [1].
60 Continuous non-invasive measures of blood flow velocity and volumetric flow are also
61 possible via Doppler ultrasound. However, Doppler-capable devices can be prohibitively
62 expensive and require the presence of a skilled operator to hold the transducer at a fixed angle
63 over the artery. Given the interdependence of BP and blood flow, methods have been proposed
64 whereby volumetric blood flow may be estimated via analysis of the BP waveform (e.g. pulse
65 contour analysis), thus circumventing the challenges posed by conventional blood flow
66 assessment [2–5]. Yet, methods utilising pulse contour analysis have been shown to be
67 inaccurate during hemodynamic instability [6].

68 The reservoir-excess pressure model is a heuristic model of arterial hemodynamics that
69 separates the measured BP waveform into reservoir pressure and excess pressure components.
70 [7,8] These components can be derived from peripheral arterial BP waveforms recorded
71 invasively or non-invasively [9,10]. In their original study outlining the reservoir-excess
72 pressure model, Wang et al. [7] demonstrated striking similarities between the shape of the
73 excess pressure and volumetric flow waveforms in the dog aorta. More recently, excess
74 pressure derived from non-invasively acquired carotid artery waveforms closely approximated
75 aortic volumetric flow in humans. [11] Thus, excess-pressure represents a potential opportunity
76 to measure clinically relevant information related to both BP and flow from only the arterial
77 BP waveform and without the requirement for specialised flow-monitoring equipment.
78 However, the equivalency of excess pressure to blood flow velocity has never been
79 simultaneously compared using invasive BP and direct measurement of blood flow velocity in
80 humans, which was the aim of this study.

Methods

81
82 **Participants.** A total of 146 individuals were approached for inclusion in the study at the Royal
83 Hobart Hospital (Hobart, Australia) prior to elective coronary angiography. Study exclusion
84 criteria included inter-arm cuff systolic and/or diastolic BP difference >5 mmHg (n=5), the
85 presence of aortic stenosis or arrhythmias (n=8), arterial access only available via the femoral
86 artery (n=7) and technical or medical issues arising that prevented the measurement of study
87 variables (n=13). Additionally, data capture was unsuccessful at the brachial and radial arteries

88 in 5 and 9 individuals respectively, and 6 individuals declined study participation. Reservoir-
89 excess pressure model analysis failed to meet pre-specified quality control ($P_{\infty} > 0$ and
90 $<$ diastolic BP) in 14 individuals (brachial $n=5$, radial $n=9$), so complete data were available for
91 97 brachial and 89 radial comparisons of flow velocity with excess pressure. Participants'
92 clinical history (hypertension, smoking and hyperlipidaemia status) and anthropometric
93 measurements were obtained from coronary angiography pre-assessment documentation.
94 Clinical information was collected from the hospital digital health records. All participants
95 gave written informed consent and ethical approval was granted by the University of Tasmania
96 Human Research Ethics Committee.

97 **Blood flow velocity and intra-arterial blood pressure acquisition.** Methods relating to the
98 recording of intra-arterial BP have previously been published. [12] Intra-arterial BP was
99 recorded using a fluid filled catheter with intra-arterial access via the right radial artery. Blood
100 flow velocity was recorded using two-dimensional pulsed Doppler ultrasound with 12 MHz
101 linear-array transducer (Vivid i, GE Healthcare, Chicago, IL, USA; Figure 1). Pulsed wave
102 Doppler flow velocities were recorded at a transmission frequency of 12 MHz, with a fixed
103 angle of insonation of 60 degrees and sample volume encompassing the lumen cross-section.
104 The envelope of peak instantaneous blood flow velocity was derived offline using EchoPAC
105 software (GE Healthcare, Chicago, IL, USA; Figure 1) and converted to text format for analysis
106 using automated line tracing software. Immediately following completion of the coronary
107 angiography procedure, the catheter was positioned in the right mid-brachial artery and
108 continuous intra-arterial BP was recorded. Simultaneously with intra-arterial brachial BP
109 recordings, blood flow velocity was recorded from the mid-brachial artery on the contralateral
110 arm. Following successful data capture at the brachial artery, the intra-arterial catheter was
111 pulled back to the radial artery and intra-arterial radial BP was recorded simultaneously with
112 radial blood flow velocity recorded on the contralateral arm. Intra-arterial BP was recorded at
113 a sampling frequency of 1000 Hz. Continuous intra-arterial BP and blood flow velocity
114 waveforms were then ensemble averaged using up to 7 cardiac cycles (no less than 4) and the
115 ensembled waveforms were cropped to the shortest cardiac cycle. The ensemble averaged
116 waveforms were used for analysis.

117 **Derivation of excess pressure waveform.** Analysis of the ensemble averaged BP waveforms
118 was performed using custom-written scripts in MATLAB (The MathWorks Inc, USA).
119 Reservoir pressure (P_{res}) was estimated from:

$$\frac{dP_{res}}{dt} = ks(P - P_{res}) - kd(P_{res} - P_{\infty}) \quad (1)$$

120 where P is the total measured pressure, ks is the systolic rate constant, kd is the diastolic rate
 121 constant and P_{∞} is the arterial asymptotic pressure. This first-order linear differential equation
 122 was solved as:

$$P_{res} = e^{-(ks+kd)t} \int_0^t P(t')e^{(ks+kd)t'} dt' + \frac{kd}{ks + kd} \times (1 - e^{-(ks+kd)t})P_{\infty} \quad (2)$$

123 The diastolic parameters, kd and P_{∞} were estimated by fitting an exponential curve to P during
 124 diastole, and ks was estimated by minimizing the sum of squares of error between P and P_{res}
 125 obtained over diastole. To calculate the excess pressure, P_{res} was subtracted from P . Derivation
 126 of P_{res} , excess pressure, ks and kd from the BP waveform can be seen in Figure 1.

127 **Additional processing.** Excess pressure and flow velocity waveforms were zero normalised
 128 and temporally aligned by cross-correlation. Prior to normalising, the pulse height of blood
 129 flow velocity and excess pressure waveform was calculated by subtracting the minimum value
 130 from the maximum value (e.g. maximum flow velocity – minimum flow velocity).

131 **Statistical analysis.** Unless stated otherwise, data are expressed as mean \pm SD or n (%). All
 132 statistical analyses were performed in R, version 3.5.3 for Windows (R Foundation for
 133 Statistical Computing, Vienna, Austria). Cross-correlation (via the *ccf* function) and
 134 magnitude-squared coherence (via the *spec.pgram* function) were used to compare agreement
 135 between excess pressure waveforms and blood flow velocity waveforms in the time and
 136 frequency domain respectively. In time domain analyses, values of coherence were quantified
 137 between 0 and 1 and interpreted in a similar manner to the Pearson's R coefficient. Specifically,
 138 a coherence value of 0 indicates no causal relationship between excess pressure and flow,
 139 whereas a coherence value of 1 indicates a linear frequency response between excess pressure
 140 and flow. To reduce the influence of noise (from high frequencies), the mean of coherence
 141 values up to 10Hz were calculated. Zou's confidence interval was used to determine differences
 142 in cross-correlation coefficients between groups [13,14]. Linear regression and Pearson's r
 143 were used to examine associations of continuous variables after the assumption of linearity was
 144 confirmed by examination of residuals. Read re-read reliability of flow velocity and BP

145 measures was determined by two-way mixed model analysis and summarized by the intraclass
146 correlation.

147 **Results**

148 **Clinical characteristics.** Clinical characteristics of study participants are presented in Table 1.
149 Participants were middle to older age and consisting of mostly males and often with coronary
150 artery disease defined by mild to severe narrowing in at least one coronary vessel.
151 Hemodynamic variables of study participants are presented in Table 2.

152 **Comparison of excess pressure with blood flow velocity.** Comparisons of blood flow
153 velocity and excess pressure waveforms can be seen in Figure 2. Brachial artery blood flow
154 velocity was highly cross-correlated with excess pressure derived from brachial BP waveforms
155 (Table 3, cross-correlation coefficient range = 0.72 to 0.99). Similarly, radial artery blood flow
156 velocity was highly cross-correlated with excess pressure derived from radial artery BP
157 waveforms (Table 3, cross-correlation coefficient range = 0.81 to 0.99). In frequency analyses,
158 coherence between blood flow velocity and excess pressure was similar for brachial and radial
159 artery comparisons (brachial median coherence = 0.93 and radial median coherence = 0.92).
160 32% of brachial artery excess pressure and flow comparisons had coherence values ≥ 0.95 and
161 73% had coherence ≥ 0.90 . 27% of radial artery comparisons had coherence values ≥ 0.95 and
162 70% had coherence values ≥ 0.90 . Mean square error was 0.09 ± 0.07 for brachial waveform
163 comparisons and 0.11 ± 0.09 for radial waveform comparisons. Root mean square difference
164 for blood flow velocity and excess pressure were 0.29 ± 0.11 and 0.32 ± 0.13 for brachial and
165 radial artery comparisons respectively. Brachial blood flow velocity pulse height was linearly
166 associated with excess pressure pulse height ($r = 0.52$, $p < 0.001$). Similarly, radial blood flow
167 velocity pulse height was associated with excess pressure pulse height ($r = 0.43$, $p < 0.001$).
168 Comparisons of wave intensity patterns using measured flow velocity and excess pressure are
169 provided in the supplemental material.

170 **Differences in cross-correlation coefficient between groups.** There was no difference in
171 brachial cross-correlation coefficient between individuals stratified by sex (95% confidence
172 interval[CI] = -0.047, 0.062), hypertension status (95%CI = -0.035, 0.078), presence of
173 coronary artery disease (95%CI = -0.053, 0.049), hyperlipidaemia (95%CI = -0.026, 0.086),
174 smoking status (95%CI = -0.050, 0.058) or type 2 diabetes status (95%CI = -0.0650, 0.0158).
175 Similarly, there were no differences in radial cross-correlation coefficients between groups.

176 **Read re-read analysis.** Intraclass correlation coefficient for peak blood flow velocity was 0.99
177 (95%CI = 0.99 to 0.99). Intraclass correlation coefficient for peak excess pressure was 0.99
178 (95%CI = 0.99 to 1).

179 **Discussion**

180 The aim of the present study was to determine the relationship of excess pressure to blood flow
181 velocity derived from brachial and radial artery waveforms. Our main finding was that the
182 envelope of excess pressure derived from either brachial or radial artery waveforms
183 corresponded closely to the measured blood flow velocity envelope at each arterial site. These
184 findings highlight that important information about the blood flow waveform may be derived
185 from assessment of the BP waveform alone, which may be adapted for use in the clinical setting.
186 We envision our findings may provide useful information for continuous hemodynamic
187 monitoring and may facilitate more detailed BP waveform analysis which require measured
188 flow, such as wave intensity and wave separation analyses. Nevertheless, future studies are
189 needed to determine the usefulness of our findings for these purposes.

190 A continuous, non-invasive and operator independent method for accurate assessment
191 of stroke volume is highly sought after for improving clinical decisions in the critical care
192 setting. Pulse contour analysis is a method whereby stroke volume is estimated from the BP
193 waveform and has been the focus of numerous investigations [15]. Several techniques
194 employing pulse contour analysis have attempted to exploit the relationship between the
195 windkessel-related BP and blood flow to estimate stroke volume. [15,16] However, these
196 methods require individual patient calibration with a reference standard to achieve accurate
197 absolute values of stroke volume. In this regard, calibration is often performed via
198 transpulmonary thermodilution which necessitates intra-arterial access to the pulmonary artery.
199 Additionally, calibration methods assume fixed arterial properties, but these change over time,
200 ultimately resulting in inaccurate estimates and a requirement for frequent re-calibration.
201 [17,18] Interestingly, Kamoi et al. [19] used a porcine model to show that the estimation of
202 stroke volume may be optimised via the application of the reservoir-excess pressure model by
203 reducing the number of fixed assumptions in the derivation of the windkessel pressure. They
204 went on to show that the excess-pressure model in combination with pulse-wave velocity
205 measures may facilitate more precise estimates of vessel dimensions and further improve
206 estimates of stroke volume from the BP waveform alone. [20] Furthermore, a quantitative
207 estimate of flow velocity may be achieved by scaling the peak of the excess pressure waveform
208 to 1m/s, which, based on recent large population studies in Norway and Korea, seems a

209 reasonable estimate for an assumed peak velocity. [21–23] This may facilitate the estimation
210 of parameters such as stroke distance (analogous to stroke index) and minute distance
211 (analogous to cardiac index). Yet, this method provides only an approximate estimation of a
212 quantitative flow velocity waveform and as a result, its clinical value will be greatly restricted.

213 As a result of the inverse relationship between the absolute magnitude of flow and
214 characteristic impedance, surrogate flow waveforms for use in wave separation analysis do not
215 require calibration. [3,24] Thus, previous investigators have employed a triangular flow
216 approximation method for pressure only wave separation analysis, where flow in the aorta is
217 assumed to be triangular in shape. [2,3] However, a more physiologically representative blood
218 flow waveform, such as we have examined in this current study for excess pressure, may
219 provide better results for the purpose of wave separation analysis. [24–26] Furthermore, in a
220 recent study it was shown that aortic wave intensity analysis performed using excess pressure
221 as a surrogate flow velocity waveform provides reasonable estimates of wave intensity
222 parameters. The concordance between excess pressure and flow velocity observed in the
223 present study indicate that excess pressure derived from peripheral artery BP waveforms may
224 also prove useful for wave intensity analysis. Yet, among some individuals the concordance
225 between excess pressure and flow velocity was poor and the implications of this for wave
226 separation and wave intensity analyses need to be determined. Future work should aim to
227 identify appropriate cut-off values for what constitutes good agreement between excess
228 pressure and flow velocity. As it stands, excess pressure may provide a reasonable surrogate
229 waveform for wave separation and intensity analysis, in most, but not all, individuals. [21,24]

230 In the aorta, wave intensity is dominated by a forward traveling compression wave in
231 early systole followed by a forward travelling decompression wave immediately preceding
232 diastole. Waves (forward and backward traveling) are present throughout the entire cardiac
233 cycle but the intensity of backward traveling waves in the aorta during diastole is minimal.
234 [27–29] Under these conditions, the excess pressure waveform is analogous to the blood flow
235 velocity waveform being related to it through the characteristic impedance of the aorta. [30]
236 However, in the peripheral arteries the contribution of backward traveling waves to the
237 measured BP waveform is larger due to proximity to sites of impedance mismatch. [31,32]
238 Indeed, reflected waves explain at least in part why the contribution of excess pressure to the
239 BP waveform increases moving distally from the aorta. [10] In this regard, the concordance of
240 excess pressure (wave related pressure) with directly measured flow velocity measured from
241 peripheral artery waveforms, may deviate due to the contribution of backward traveling waves.

242 [33] There was some evidence for this in our wave intensity analyses using measured flow
243 velocity (supplemental material, Figure S1). In the 75th percentile example (i.e. good
244 concordance), there was minimal backward wave activity. Whereas, in the 25th percentile
245 example (i.e. poor concordance) there was noticeably greater backward wave activity. The
246 overall importance of this in practice remains to be comprehensively determined, certainly we
247 still observed strong relationships on average between excess pressure and blood flow velocity
248 at peripheral arterial sites. In this regard, when using excess pressure as a flow surrogate for
249 wave intensity analyses, we observed that the forward compression wave was somewhat
250 comparable to that obtained by wave intensity analyses using the measured flow velocity.
251 Nevertheless, we also observed that backward wave activity was not reproducible when using
252 excess pressure as a flow surrogate, as evidenced by the median and 25th percentile examples
253 in Figure S1. Therefore, caution should be exercised before employing peripheral artery excess
254 pressure for the purposes of wave intensity analysis and more detailed studies are needed to
255 confirm the usefulness of our findings for these envisioned applications.

256 Previous studies have shown that excess pressure derived from peripheral artery BP
257 waveforms is associated with cardiovascular events and impaired kidney function independent
258 of conventional risk factors. [9,34,35] A numerical analysis of the reservoir-excess pressure
259 model posits that excess pressure represents the additional work performed by the heart above
260 the minimum required work. [36] This suggests that excess pressure may be a marker of
261 circulatory inefficiency. This current study extends previous findings of the equivalency of
262 aortic blood flow velocity with excess pressure to brachial and radial arteries. In this regard,
263 excess pressure may facilitate more detailed BP waveform analyses, such as wave intensity
264 analysis, which could provide useful clinical information for deeper BP phenotyping and risk
265 stratification beyond excess pressure alone. [37] Altogether, when derived from peripheral
266 artery BP waveforms, excess pressure may be considered a cardiovascular risk marker
267 encompassing information on cardiovascular efficiency and local blood flow dynamics.

268 **Limitations**

269 Due to the nature of the clinical setting and procedure from which the data were collected, it
270 was not possible to acquire simultaneous intra-arterial BP and blood flow velocity in the same
271 arm. Thus, it is assumed that hemodynamics between arms are comparable, an assumption that
272 may not be true for all individuals. However, inter-arm cuff systolic BP differences >5 mmHg
273 was a study exclusion criterion and may have lessened the potential influence of inter-arm
274 hemodynamic variability. Additionally, our study sample included mostly older people who

275 were undergoing coronary angiography and is not representative of young, healthy individuals
276 nor critical care patients for whom comprehensive hemodynamic monitoring is most valuable.
277 Future studies should determine if the findings of the present study are generalisable to young,
278 healthy individuals and patients in the surgical or intensive care settings. Finally, we provide
279 some hypothesis generating discussion on the potential usefulness of our findings and though
280 there was good agreement between excess pressure and flow velocity among many individuals,
281 in others there are clear differences, which may have important implications for the envisioned
282 applications of our findings. In future studies it would be valuable to identify potential
283 predictors of poor concordance between excess pressure and flow to help refine this method.

284 **Conclusion**

285 Excess pressure derived via the pressure only reservoir-excess pressure model may represent a
286 useful method for assessment of arterial hemodynamics and circulatory function. Previous
287 studies have shown that aortic excess pressure is proportional to aortic volumetric flow. In the
288 present study, excess pressure derived from peripheral artery BP waveforms corresponded
289 closely to the measured flow velocity waveform. This is of potential clinical importance as
290 continuous non-invasive recording of peripheral artery BP waveforms is easy to perform and
291 thus, removes barriers associated with conventional methods of blood flow assessment. Indeed,
292 many non-invasive continuous hemodynamic monitoring systems seek to estimate
293 hemodynamic indices from the peripheral artery BP waveform, including finger, radial and
294 brachial BP waveforms. [38] Therefore, our findings could have implications for the clinical
295 assessment of hemodynamic parameters and may provide important information for improving
296 continuous, non-invasive and operator independent hemodynamic monitoring.

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TABLE 1. Clinical characteristics of study participants

Variable	Mean \pm SD or n (%)
Age (years)	61.1 \pm 10.4
Sex (male)	70 (72)
Height (cm)	170.1 \pm 10.8
Weight (kg)	87.4 \pm 16.5
BMI (kg/m ²)	30.2 \pm 4.5
Family history of CVD	55 (60)
Hypertension	37 (41)
Current smoker	18 (19)
Hyperlipidaemia	65 (70)
Type 2 diabetes mellitus	28 (30)
Coronary artery disease	71 (76)

n = 97. CVD, cardiovascular disease; SD, standard deviation.

TABLE 2. Hemodynamic variables of study participants

Variable	Mean±SD
Brachial	
Invasive SBP (mmHg)	135.7 ± 23.5
Invasive DBP (mmHg)	66.5 ± 10.5
Invasive mean arterial pressure (mmHg)	94.3 ± 13.0
Peak flow velocity (cm/s)	68.1 ± 18.6
Mean flow velocity (cm/s)	9.1 ± 4.3
Heart rate (bpm)	62.8 ± 10.9
Peak excess pressure (mmHg)	41.4 ± 13.5
Excess pressure integral (mmHg)	
Radial	
Invasive SBP (mmHg)	141.8 ± 24.7
Invasive DBP (mmHg)	66.8 ± 10.6
Invasive mean arterial pressure (mmHg)	94.2 ± 13.2
Peak flow velocity (cm/s)	50.6 ± 16.3
Mean flow velocity (cm/s)	8.5 ± 5.4
Heart rate (bpm)	61.9 ± 10.7
Peak excess pressure (mmHg)	48.5 ± 14.7
Excess pressure integral (mmHg)	8.05 ± 3.5

n = 97. BP, blood pressure; SD, standard deviation.

TABLE 3. Cross-correlation coefficients (r value) of flow velocity with excess pressure derived from brachial and radial arteries

Arterial site	25th percentile	Median	75th percentile
Brachial	0.94	0.96	0.97
Radial	0.92	0.95	0.96

Figure legends

Figure 1. Example of reservoir-excess pressure parameters derived from an ensemble averaged brachial blood pressure waveform (left panel). Measurement of brachial artery Doppler ultrasound flow velocity (right panel).

Figure 2. Comparisons of flow velocity (solid line) with excess pressure (dashed line) and respective blood flow velocity-excess pressure loop. Xcor is the cross-correlation coefficient. Figures represent typical examples of excess pressure and flow velocity comparisons in 75th percentile, median and 25th percentile of cross-correlation value. Coherence was 0.98 (minimum = 97) for the 75th percentile example, 0.94 (minimum = 89) for the median example, and 0.86 (minimum = 71) for the 25th percentile example.

Figure 3. Radial blood flow velocity and excess pressure (A) with associated first derivatives (B) and frequency coherence (C). Complex blood flow velocity waveform morphology was well matched by excess pressure and maximum coherence occurred at a frequency of 0.7 Hz.

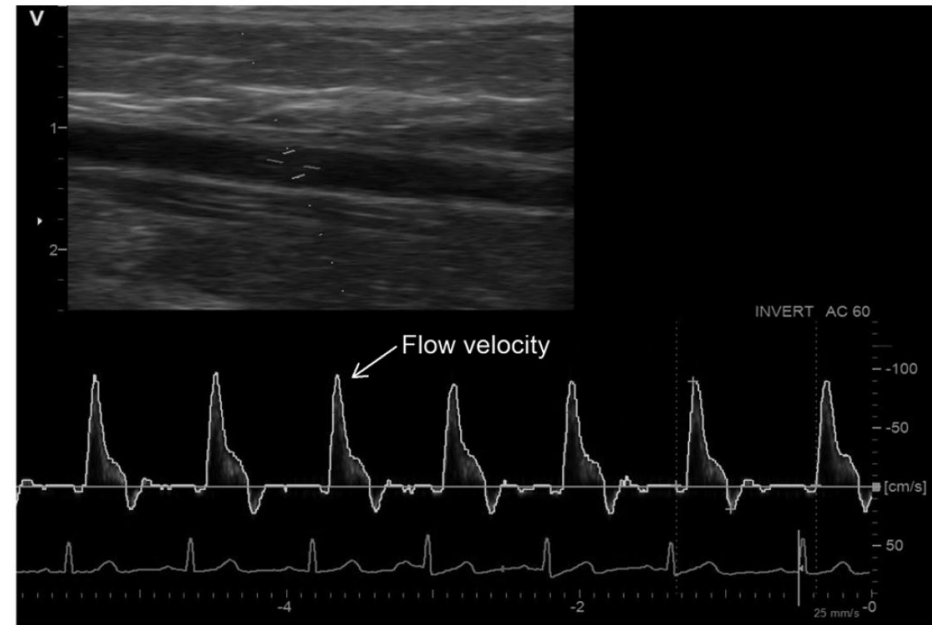
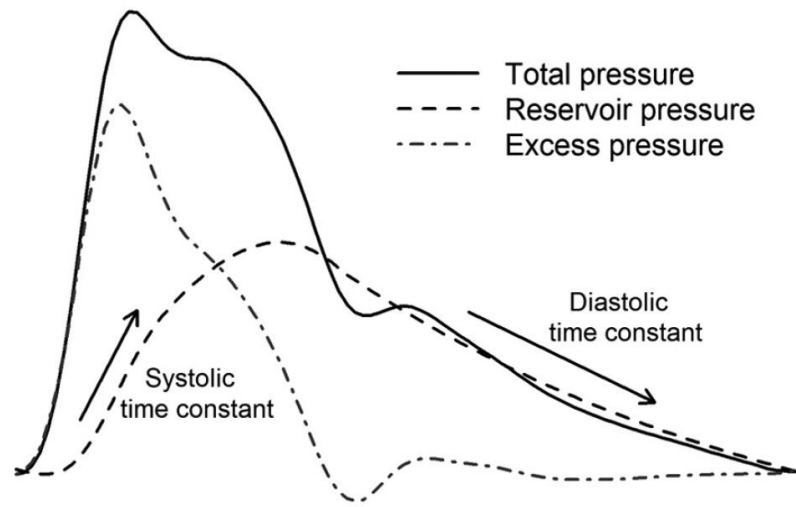


Figure 1

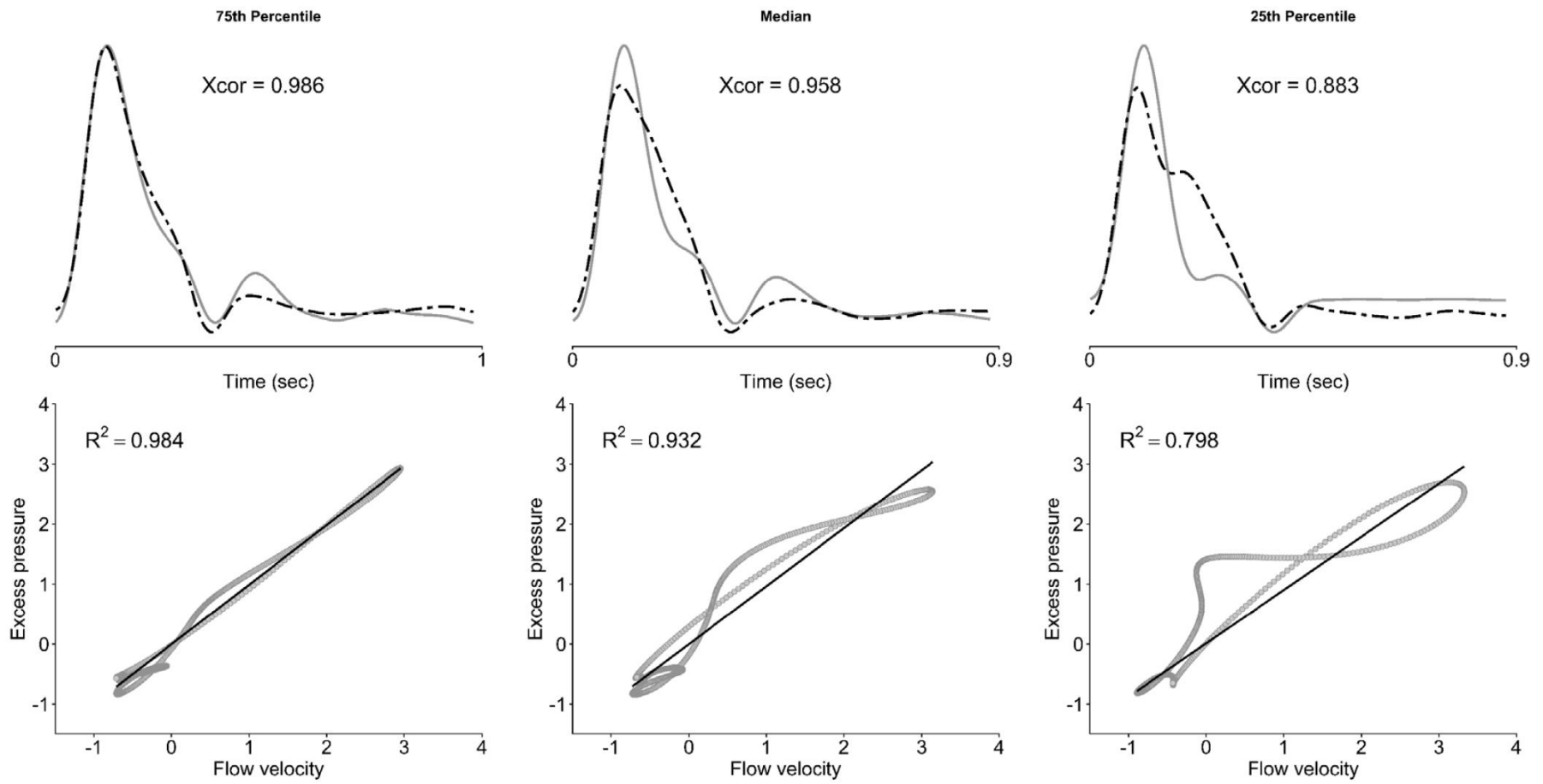


Figure 2

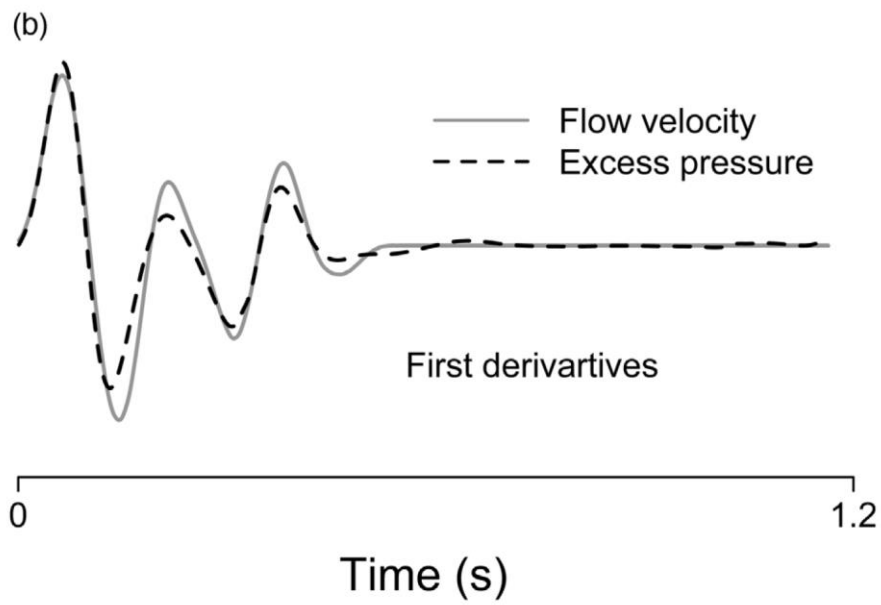
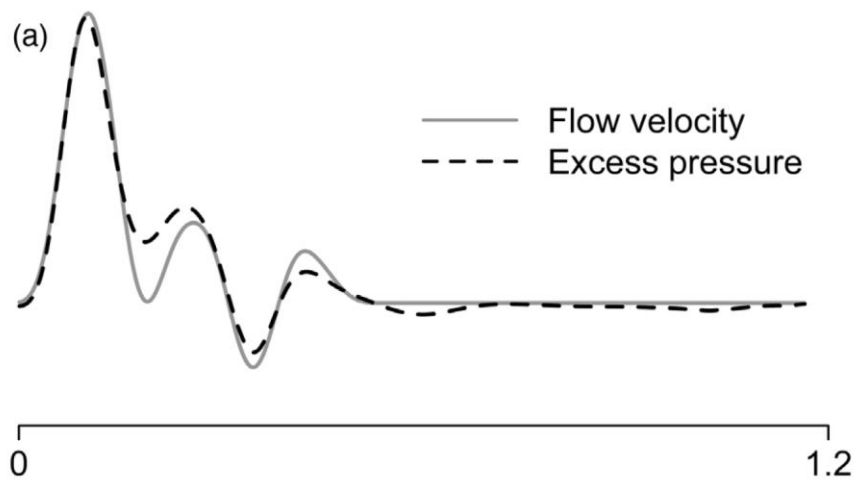


Figure 3