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9 Raw material optimisation and stone tool engineering in the Early Stone Age of
10 Olduvai Gorge (Tanzania)
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25 **Abstract**

26 For >1.8 million years hominins at Olduvai Gorge were faced with a choice: whether to use lavas,
27 quartzite or chert to produce stone tools. All are available locally and all are suitable for stone tool
28 production. Using controlled cutting tests and fracture mechanics theory we examine raw material
29 selection decisions throughout Olduvai's Early Stone Age. We quantify the force, work and material
30 deformation required by each stone type when cutting, before using these data to compare edge
31 sharpness and durability. Significant differences are identified, confirming performance to depend on
32 raw material choice. When combined with artefact data, we demonstrate that hominins optimised raw
33 material choices based on functional performance characteristics. Doing so flexibly: choosing raw
34 materials dependent on their sharpness and durability, alongside a tool's loading potential and
35 anticipated use-life. In this way, we demonstrate that early lithic artefacts at Olduvai Gorge were
36 engineered to be functionally optimised cutting tools.
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1 Introduction

2 Olduvai Gorge in northern Tanzania has a near continuous record of hominin occupation spanning >1.8
3 million years. Stone tool artefacts constitute a major source of evidence supporting this extended period
4 of habitation and visitation ¹⁻⁵. Hominins produced a variety of stone technologies at Olduvai during
5 Beds I and II (c. 1.85 – 1.2 million years ago), including tools from the Oldowan and Acheulean ¹.

6 Each recovered artefact provides behavioural evidence relating to the individual who produced it.
7 Perhaps the most obvious behaviour-related feature is the type of material a stone tool is made from.
8 Indeed, where multiple suitable raw materials exist in a landscape, tool producers made a decision
9 (conscious or otherwise) to use one material over another. The decision processes underlying raw
10 material selection behaviours represents a major element of Palaeolithic research ⁶⁻⁹, and is often vital
11 to interpreting the behaviour and cognitive capabilities of early hominins ¹⁰⁻¹².

12 Olduvai Gorge has three main raw material groups suitable for producing stone tools; lavas, chert, and
13 quartzite ² (Fig. 1). Each was used by hominins, but their selection varies chronologically, between
14 sites, and is dependent on the tool type produced. Chert, available from a few localised sources, was
15 primarily only accessible by hominins in Lower and Middle Bed II ^{7,13-15}. However, whenever it was
16 available, hominins selected and exploited this material for flakes and retouched tools ^{7,14,16,17}; although
17 tools and cores tended to be relatively small in size due to available blank dimensions ^{13,14,16,17}. The
18 other two raw materials, lavas and quartzite, were continuously available to hominins for stone tool
19 production ^{2,15,18}. Lavas, available in river channels across the Olduvai paleo-basin, were used to
20 produce flakes, cores and large cutting tools (LCTs), including handaxes, and are abundant in Oldowan
21 and Acheulean sites. When smaller lava tools were made there is a notable disparity between the number
22 of cores and flakes present at sites ^{7,14,16,19-23}. Quartzite, mostly sourced from the Naibor Soit inselberg
23 ~3 km north of the confluence of the Main and Side Gorges, was extensively used at Olduvai;
24 predominantly for the production of small flakes (debitage) which frequently (but not always ²⁴)
25 outnumber their lava counterparts ^{1,2,7,14,16-19,22,23,25}. Quartzite LCTs are also well represented at many
26 Acheulean sites, although notable inter-site variation in LCT raw material composition exists
27 ^{7,15,18,19,21,24-26}.

28 Why Olduvai hominins preferentially chose one raw material over another, in these variable ways, has
29 puzzled archaeologists for >60 years. Proposed hypotheses explaining these phenomena include their
30 disparate suitability for knapping (size, shape and material properties), edge functionality (durability,
31 retouch frequency), production efficiency and expediency, cultural differences, and their relative
32 accessibility or availability for hominins ^{1,2,7,14-19,22,27-30}. Given that some stone types available to
33 hominins such as lavas and quartzite remained relatively consistent through time, it is possible that a
34 single unifying factor could help explain the raw material selection behaviours of hominins at Olduvai
35 Gorge. Yet, to date, no single factor is able to satisfactorily explain raw material selection decisions
36 over the Oldowan and Acheulean. Here, we put forward the hypothesis that the sharpness and durability
37 of a raw material's cutting edge, and in turn their relative functional performance, may provide a
38 unifying explanation.

39 Only recently have archaeologists started to investigate the attribute of edge sharpness empirically ³¹⁻³⁴.
40 Controlled cutting tests have previously been used to record mechanical definitions of this attribute on
41 lithic objects ^{32,33}, following techniques regularly applied within fracture mechanics research ³⁵⁻³⁷. Here,
42 we apply a similar experimental procedure that allows the force (N), work (J) and material deformation
43 (mm) required for a stone edge to initiate cuts in a material to be recorded. Using these data, we address
44 whether the sharpness and durability of raw materials from Olduvai Gorge can explain their selection
45 and use by hominin species across nearly a million years of the Oldowan and the Acheulean.

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1 **Methods**

2 Fracture mechanics research regularly utilises controlled cutting experiments during investigations of
3 edge sharpness, blunting rates, and the impact of edge geometry on cutting mechanics^{e.g. 35,37,52,54}. Only
4 recently has archaeological literature utilised similar techniques to answer Palaeolithic questions^{32,33}.
5 Here, we adapt the techniques used during fracture mechanics research^{35,37}, and improve on those used
6 previously for archaeological purposes³², to compare the sharpness and durability of the three raw
7 materials used to produce stone tools at Olduvai Gorge.

8 *Raw material selection*

9 The three raw materials used in this study, quartzite, lava and chert, dominate the archaeological
10 record of Beds I and II of Olduvai Gorge².

11 Quartzite blocks were collected from the primary source at Olduvai, the Naibor Soit Inselberg, located
12 north of the confluence of the Main and Side Gorges. This quartzite is of metamorphic origin, is
13 coarse grained and possessed micaceous layers which are foliated and lineated^{2,15}. The lava at
14 Olduvai originated from the surrounding volcanic outcrops^{2,27}, however, is abundant in the seasonal
15 rivers and streams present today and during Beds I and II. A variety of different lavas would have
16 been available to Beds I and II hominins, including trachyte, phonolite, and basalt². For this study
17 only basalt was used. The chert at Olduvai is formed through the precipitation of sodium silicate
18 minerals from the saline, alkaline Olduvai lake during Bed II, over a short period of time (<10ka)^{2,13}.
19 The chert is fined grained with a chalk cortex and the nodules possess an irregular shape, which vary
20 greatly in size. All chert flakes used in this study were produced from nodules collected in the primary
21 known chert source at Olduvai, the Main Chert Unit at MNK¹³.

22 *Flake selection*

23 Two nodules of quartzite, basalt, and chert were reduced by one of us (TP) to produce the flakes used
24 in this experiment (Fig. 2). Each was flaked using hard hammer percussion, with the sole intention of
25 producing edges suitable for cutting. Between 50 and 70 flakes were produced for each raw material.
26 These stone types do display compositional variation, which could influence their cutting performance.
27 These differences will, however, likely be subtle relative to any differences observed between the three
28 distinct raw material types examined here. From each raw material 30 flakes were selected on the basis
29 of displaying straight, homogenous and relatively acute cutting edges. Each length of cutting edge was
30 required to be greater than 15mm. A 10mm segment of this edge was clearly marked and assigned as
31 the portion applied during the cutting tests.

32 Edge angle is known to significantly impact the performance of stone tools during cutting tasks³². To
33 control for its influence here, edge angle was consistent between the three raw materials. Using the
34 'caliper method'⁵⁵, edge angle measurements were recorded at depths of 2mm and 4mm away from the
35 edge apex, at three locations on the predetermined length of cutting edge (at 0mm, 5mm, and 10mm).
36 The mean of these six measurements was the recorded 'edge angle' for each tool. The 30 edge angle
37 measurements for each raw material were normally distributed (Shapiro-Wilk tests; $p = .500 - .895$),
38 and were statistically compared for differences using t -tests ($\alpha = .050$). No significant differences were
39 identified between the three raw material samples ($p = .066 - .546$). Mean edge angle values for each
40 material ranged between 31-35°.

41 For the cutting tests, each flake was secured into a wooden block measuring 116 x 30 x 22 mm using a
42 commercially available polyurethane adhesive. Each flake was orientated such that the predetermined
43 cutting edge was parallel to the motion of cutting.

1 *Recording sharpness and durability through controlled cutting tests*

2 The sharpness of a stone cutting edge can be defined geometrically or mechanically³¹. Geometric
3 definitions of sharpness rely on the measurement of tip radius at the apex of an edge⁵². A first attempt
4 to record this edge-form attribute on stone tools was recently performed by Stemp et al.³⁴, who used
5 multiple high-powered 3D microscopy techniques and tip curvature algorithms to examine geometric-
6 sharpness on five stone tools. Here, we follow Schuldt et al.³⁷, Key et al.³² and others^{33,36,35,51-54} by
7 using a mechanical definition of sharpness. That is, sharpness “refers to the ability of a blade to initiate
8 a cut at low force and deformation”³⁷. Previous research has repeatedly confirmed that comparative
9 measurements of force (N), work (J), and material deformation (mm) at the point of cut initiation can
10 provide accurate measures of sharpness^{35-37,51,54}. An Instron 3345 tensile testing machine is used here
11 to record these attributes, at a rate of 20 hertz (Hz) (i.e. 20 readings per second).

12 Tensile testing machines allow the movement of a cutting edge in a vertical plane, such that it can be
13 lowered onto a worked material. Here, the wooden blocks containing the stone flakes were secured into
14 the upper grip of the Instron device. Thus, the flake’s cutting edge was able to be lowered onto a worked
15 material; in this case, polyvinyl chloride (PVC) tubing with a diameter of 2 mm. PVC tubing provides
16 increasing resistance to a cutting edge as it is deformed prior to a cut initiation (as similarly observed
17 in soft-solid bio-materials [e.g. muscular tissue]), while also maintaining identical material conditions
18 for each cutting test. Previous experiments using similar materials have proven its efficacy for sharpness
19 tests^{32,33,54}. Tubing was secure using a steel frame and pulled taut (but not stretched) perpendicular to
20 the flake’s cutting edge.

21 Each flake’s cutting edge was aligned with the surface of the PVC tubing prior to the start of the cutting
22 test, at which point ‘loading’ measures on the Instron were balanced and ‘distance moved’ records were
23 zeroed. Subsequently, flakes were lowered into the PVC at a rate of 20mm/minute until the cutting edge
24 created stress enough to fracture the tubing and a cut formed (Fig. 2). Force (N) and material
25 deformation (mm) at the point of cut initiation were recorded; as was the area under each cutting test’s
26 stress-strain curve, which was required to calculate the work (energy [J]) required for cut initiations.
27 Identical material conditions between cutting tests produced matching stress-strain curve shapes
28 between samples. This allowed the area under each curve to be treated as a triangle (Supplementary
29 Figure 3), such that a curve area (a) equalled half the force (N) required multiplied by the distance
30 moved (m) (i.e. $a = (F \times m) \times 0.5$).

31 Relative edge durability between the three raw materials was investigated by comparing reductions in
32 performance across the duration of a known cutting task. In theory, more durable edges should better
33 retain a relatively acute edge and small edge apex radius, and in turn, their capacity to cut efficiently³¹.
34 A randomly selected sample of 15 flakes from each raw material performed five longitudinal cutting
35 strokes on an oak branch (with the bark already removed), which in turn created six ‘durability
36 conditions’ (i.e. condition one was a fresh flake, condition two was after one cut, and condition three
37 was after two cuts, etc.). In addition to the initial cutting test performed by each flake prior to use (see
38 above), another five identical cutting tests were performed for each flake, one after each cutting stroke.
39 Hence, each durability condition had its own record of force, work, and material deformation. It was,
40 therefore, possible to calculate edge performance, and in turn edge durability, for each of these raw
41 materials in the face of a cutting activity likely to cause edge attrition and blunting.

42 *Raw material comparisons*

43 Sharpness was compared between the three raw materials using the force, work and material
44 deformation records produced from the full 90 flake sample (i.e. prior to any wood cutting activities).

1 In this way, sharpness is recorded from each material in its sharpest state, immediately after being
2 flaked. Shapiro-Wilk tests revealed force, work and material deformation values to contain a mix of
3 normally distributed and non-normally distributed data ($p = <.000 - .469$). In turn, *Mann-Whitney U*
4 tests were used to examine differences in these sharpness metrics between the three raw materials ($\alpha =$
5 $.050$).

6 Raw material durability was examined through relative changes in performance across the six controlled
7 cutting tests. First, this was examined through percentage changes in mean force, work, and material
8 deformation from each flake's initial controlled cutting test, through to their sixth ($n = 15$ in all
9 instances). Subsequently, *Mann-Whitney U* tests examined whether individual abrasive cutting strokes
10 were enough to cause significant reductions in performance in durability conditions one through to six,
11 and how this varied between the three raw materials. These tests were performed sequentially, such that
12 sharpness measures from cutting test one was compared to test two, while test two was compared to
13 test three, and so on.

14

15 **Results**

16 *Sharpness*

17 Chert and quartzite from Olduvai Gorge are demonstrated to be significantly sharper than basalt
18 collected from the same location. This result is consistent for the three sharpness metrics recorded here;
19 the force (N), work (J), and material deformation (mm) required to cut (Table 1). Mean values
20 emphasise the scale of these differences, with basalt's force and material deformation results being at
21 least twice as great as the other raw materials (Table 2; Fig. 1). This difference increases substantially
22 for work (energy) values (Table 2; Fig. 1). Quartzite is marginally sharper than chert in all instances;
23 these differences are not, however, significant (Table 1).

24 *Durability*

25 Edge durability was first assessed through percentage changes in force, work, and material deformation,
26 from each material's initial sharpness, through five separate use events. Basalt consistently returned the
27 lowest levels of change ($\leq 25\%$), and therefore displays the most durable edges (Supplementary Table
28 1). Chert returned lower percentage change values relative to quartzite (Supplementary Table 1).
29 Differences between the chert and quartzite flakes were reduced relative to the basalt comparisons.
30 Mean force, work, and material deformation values across the six durability conditions support these
31 results (Supplementary Table 2; Supplementary Figure 1).

32 *Mann-Whitney U* tests for each sharpness metric between sequential durability conditions (i.e. $0 \leftrightarrow 1$,
33 $1 \leftrightarrow 2$, etc.) similarly identified basalt as the most durable raw material at Olduvai. Significant
34 differences were only identified between conditions zero and one; supporting previous work identifying
35 the earliest stages of blunting to have the proportionately greatest impact on stone tool performance. It
36 was, however, only chert and quartzite that returned significant changes in force, work, and material
37 deformation. Basalt did decrease in sharpness, but this was never to a significant extent.

38 It should be noted, however, that the cutting performance of chert, quartzite and basalt recorded here
39 are specific to Olduvai Gorge, and caution is necessary before applying these results to similar raw
40 materials (particularly quartzite) from other locations.

41

42 **Discussion**

1 For every stone tool produced at Olduvai Gorge, a decision of which raw material to use had to be
2 made. Here, we demonstrate that edge sharpness and durability, and in turn functional performance,
3 varies significantly between chert, basalt and quartzite. These substantive differences had potential to
4 impact raw material selection-related behaviours throughout the Early Stone Age at Olduvai. Quartzite
5 is identified as the sharpest raw material, requiring significantly less force and energy to use relative to
6 basalt. Chert is nearly as sharp quartzite, but exhibits more durable edges. Basalt is confirmed as being
7 substantially more durable than both chert and quartzite, but has significantly lower initial sharpness.
8 Therefore, not only do raw materials at Olduvai Gorge display disparate performance characteristics *cf.*
9 ³⁸, each has advantages and could have been preferentially chosen dependent on a tool's context of use.

10 These fundamental differences would have remained consistent throughout the Early Stone Age at
11 Olduvai. Thus, functional pressures should have equally affected the behaviour of Oldowan and
12 Acheulean populations. The question of whether raw material selection decisions were optimised
13 according to their respective performance characteristics is, therefore, applicable to the potentially
14 different human species that produced stone tools at Olduvai Gorge, including smaller brained hominins
15 with a diminutive stature (e.g. *H. habilis*) and larger brained species with more modern human-like
16 anatomy (e.g. *H. erectus s.l.*).

17 As the sharpest raw material, quartzite required hominins to input the lowest force and energy levels
18 during cutting activities. The 'ease' with which cuts are created is, then, greatest in this raw material.
19 This difference applies equally to all tools made from quartzite. Why, then, did Oldowan and Acheulean
20 hominins at Olduvai preferentially select quartzite for flake tools (debitage), chert whenever available,
21 and lavas/quartzite disproportionately at different sites for LCTs? We propose that, in addition to stone
22 sourcing distance factors, these choices reflect flexible, functionally-related raw material selection
23 decisions by Olduvai hominins; different stone types were selected according to not only their initial
24 sharpness, but the durability and longevity of their edges, and possibly the anticipated loading potential
25 and use-life of tools.

26 The Oldowan is often considered an expedient cutting technology at Olduvai ^{1,14,24} and other Early Stone
27 Age sites ^{39,40}, and thus the preferential selection of quartzite for flake tools is expected. It represents
28 the most effective and efficient raw material for short-term cutting activities, where its initially greater
29 edge sharpness maximises functional output (i.e. cut material volume) while minimising energy
30 expenditure and loading (cutting force) requirements. Within this functional context there would be no
31 substantive need for a more durable edge; although the harder the cut material, the briefer quartzite's
32 benefits would have been ^{32,41}. Chert displays benefits to its use – increased edge durability and
33 longevity – relative to quartzite, but no demonstrative cost to the initial sharpness, and therefore
34 efficiency, of tools. Given potentially high raw material transportation costs ²⁹ and a palaeo-
35 environment where tools may be required for longer than initially predicted or used to cut hard
36 materials, chert represents an enhanced raw material. This explains the preferential selection of chert
37 during its limited period of availability. The relative increased prevalence of retouch on chert tools (e.g.
38 at HWK EE retouched chert artefacts make up 12.9% of the total chert assemblage compared to 0.5%
39 of the quartzite assemblage ¹⁷) can similarly be associated with the exploitation of a superior raw
40 material over extended durations or multiple tool-use events ^{14, 16, 21}. Basalt would have represented a
41 comparatively poor choice for expedient cutting tools; particularly those used for cutting activities
42 involving highly extensible or flexible materials ³¹. Our results do not mean that basalt is not effective
43 at cutting, but that it is significantly less efficient relative to quartzite and chert in the earliest stages of
44 an edge's use.

45 Over extended periods of use stone edges wear down ^{42,43}, become blunter (i.e. less sharp), and require
46 greater force and energy inputs to perform a cut ^{32,33,44}. Confirming early experimental work by Jones
47 ¹⁹, we demonstrate that basalt edges are significantly more durable than quartzite and chert, meaning
48 that relative differences in performance between these stone types reduces over time. At a point basalt

1 would not just display similar sharpness and cutting performance as quartzite and chert, but would likely
2 overtake them (Supplementary Figure 4). Recent experimental work¹¹ suggests that this point may not
3 be reached until after a substantial number of cutting strokes (perhaps > 300). For tools with long use-
4 lives basalt would, therefore, represent the superior raw material choice at Olduvai.

5 Handaxes and other LCTs are thought to have displayed (relatively) long use-lives and/or were used
6 during heavier duty cutting activities that cause increased blunting^{19,39,45-47}. Moreover, their larger size
7 and longer cutting edges facilitate the exertion of greater cutting forces^{45,48,49} and cutting stroke
8 velocities^{31,42,48,50} (respectively), which help counteract increased force requirements caused by reduced
9 sharpness^{41,44,50,51}. Within this functional context basalt (and other lavas) should represent the optimal
10 raw material at Olduvai. Some Acheulean sites do display proportionately high numbers of lava LCTs
11^{7,24}, which could potentially suggest the preferential selection of this raw material based on functional
12 performance attributes. These factors alone, however, cannot explain assemblages displaying equal or
13 greater proportions of quartzite LCTs³.

14 We do not necessarily interpret such occurrences as the production of sub-optimal cutting implements
15 by Acheulean individuals. Certainly, for short term heavy-duty cutting behaviours quartzite LCTs could
16 have been more efficient and thus favoured. We do, however, suspect that such occurrences also reflect
17 the functional and landscape- based complexities at Olduvai, as previous research highlights the impact
18 that other raw material-related factors, such as transportation distances and available core sizes/shapes
19^{15,17,18,24,29}, likely had on assemblage composition. These factors and others⁸ need to be considered
20 alongside the data reported here to fully understand all Olduvai raw material selection behaviours across
21 the Early Stone Age. Moreover, observed differences in artefact transportation distances, function, and
22 technological features at Olduvai, and how they relate to raw material factors (including between
23 Oldowan and Acheulean sites), can now consider the potential influence of cutting performance
24 differences; in turn, increasing our understanding of other behavioural elements.

25 Sharpness and durability data can, however, help decipher lava flake and core production as many
26 Olduvai sites display disproportionate numbers of flake scars relative to flakes^{14,17,18,20,22}, suggesting
27 dynamic input and output of artefacts at assemblages. This has been interpreted as lava flakes either
28 being preferentially removed for cutting activities away from the gorge, potentially suggesting extended
29 use durations, or the active movement of lava core tools within the gorge for ‘heavy-duty’ cutting
30 behaviours^{14,22}. Our data cannot distinguish between these options as the use of lava in both contexts
31 is advantageous; however, it helps explain why only lavas display this phenomenon. Future works
32 investigating these and other raw material-related behaviours, such as core reduction intensity and
33 efficacy^{7,14,16-19,22}, retouching frequency^{13,16,17,24}, tool function^{19,21,28} and transportation distances
34^{8,15,22,29}, may similarly profit from the data provided here at Olduvai and elsewhere [e.g. 56, 57].

35 Together, experimental and archaeological evidence indicates that Olduvai hominins may have
36 optimised raw material selection behaviours to maximise the efficiency and/or longevity of their stone
37 cutting-tools, as indicated by the preferential use of chert whenever available and quartzite for flake
38 (debitage) tools. LCT artefacts, however, underscore the complex decision processes faced by Olduvai
39 hominins, whereby multiple functional and non-functional considerations affected raw material
40 selection behaviours. When combined with earlier work¹¹, our data demonstrates that Early Stone Age
41 hominins at multiple east African locations selected stone tool raw materials based on functional
42 considerations. Such capabilities may, therefore, be more widespread during this period than currently
43 recognised. Olduvai data however go further, demonstrating that a tool’s loading potential, anticipated
44 use-life, and required force and energy expenditure were likely influencing the raw material related
45 decisions practiced over an extended archaeological sequence. This represents previously unseen
46 complexity in how raw material functional considerations were flexibly managed by multiple hominin
47 species. Although Pleistocene individuals may not have been aware of doing so, a series of mechanical
48 principles routinely applied during the design of modern metal cutting tools were being exploited to

1 maximise each tool's functional potential and ease of use^{37,42,44,52}. In this way, stone tools at Olduvai
2 Gorge were engineered, functionally optimised cutting implements.

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1 **Tables**

		Raw Material	
		Basalt	Chert
Force (N)	Chert	<.0001	-
	Quartzite	<.0001	.141
Work (J)	Chert	<.0001	-
	Quartzite	<.0001	.222
Material Deformation (mm)	Chert	<.0001	-
	Quartzite	<.0001	.246

2

3 **Table 1:** *Mann-Whitney U* tests between the Olduvai raw materials and the three metrics used to
 4 investigate edges sharpness.

5

	Raw Material		
	Basalt	Chert	Quartzite
Mean Force (N)	88.1	41.1	33.4
Mean Work (J)	1.60	0.36	0.24
Mean Material Deformation (mm)	35.3	15.0	13.1

6

7 **Table 2:** Mean force (newtons [N]), work (joules [J]), and material deformation (millimetres [mm])
 8 measures for the three Olduvai raw materials during each of the six durability conditions. These
 9 sharpness metrics detail how easily the three raw material types can initiate a cut in the PVC tubing.

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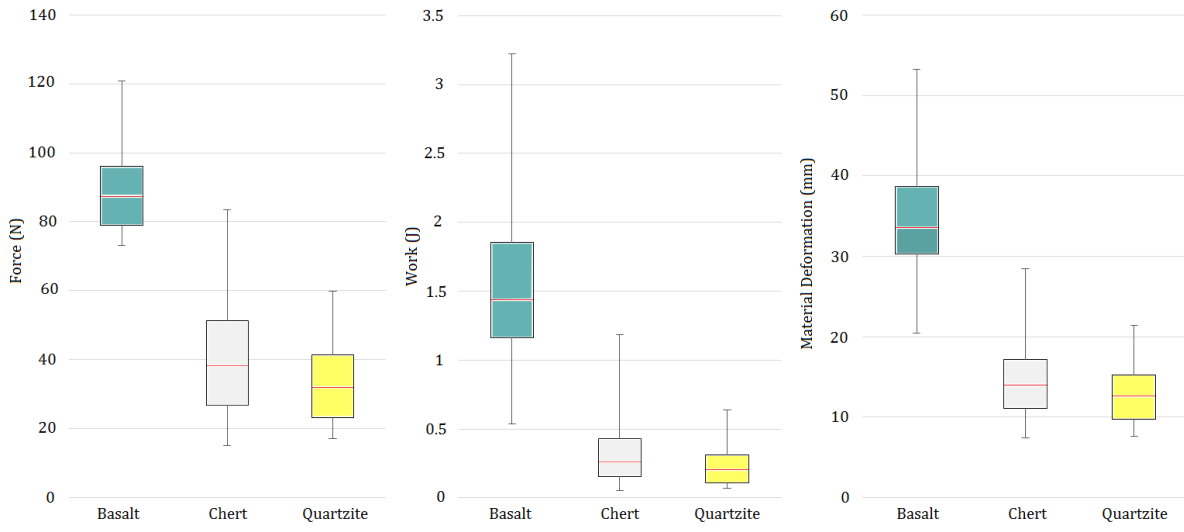
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1 **Figures**

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4 **Figure 1:** Force (N), work (J), and material deformation (mm) values for each Olduvai raw material
5 plotted against each other (n = 30 for basalt and chert, while quartzite is represented by 28 flakes [two
6 edges crushed during the first cutting test]). A consistent pattern emerges for all sharpness measures,
7 in which basalt is the poorest in terms of performance.

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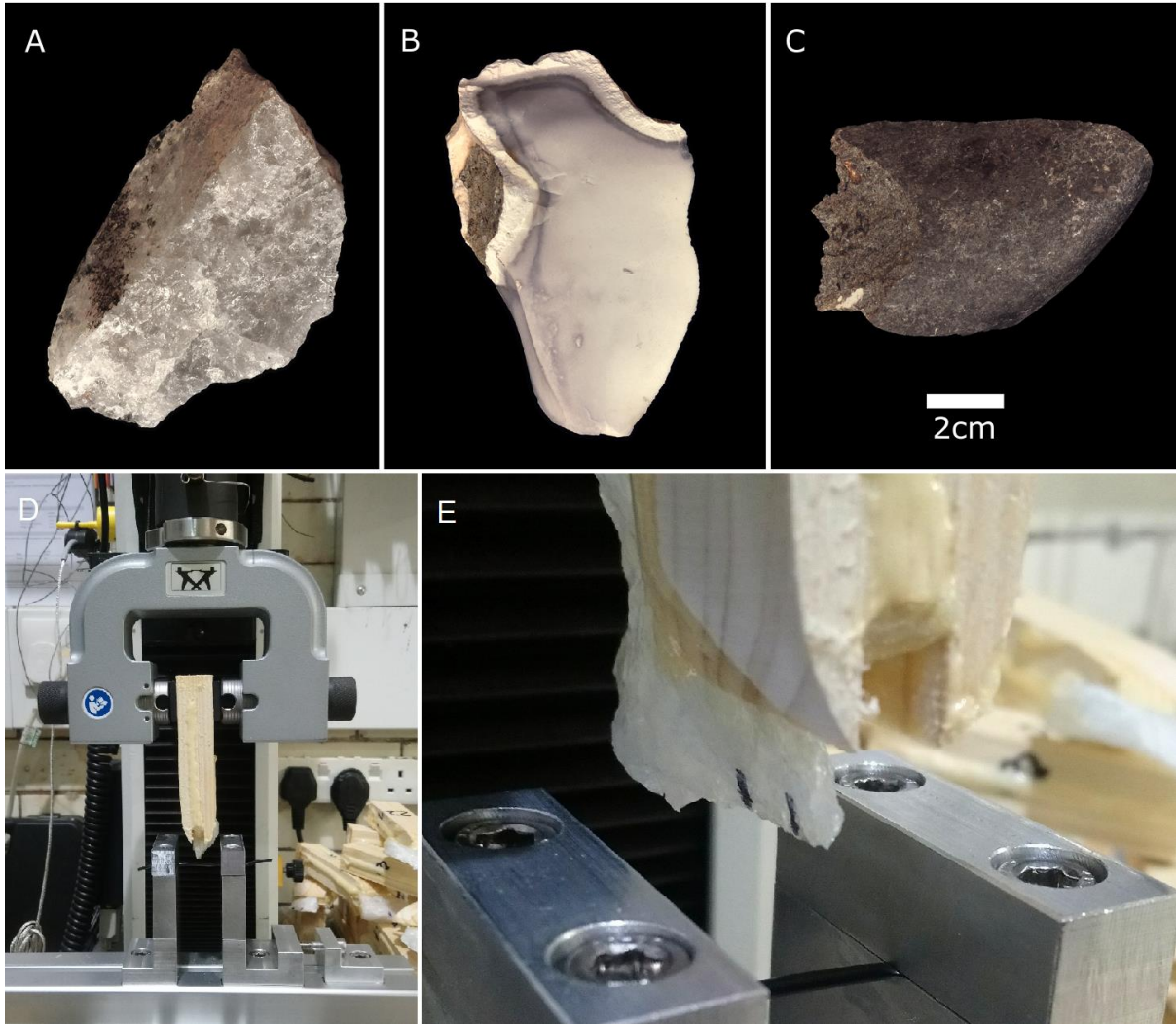
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Figure 2: Representative flakes made from (left to right) quartzite (A), chert (B) and basalt (C) at Olduvai Gorge, Tanzania. The Instron 3345 tensile testing machine used during the controlled cutting tests (D, E). A quartzite flake, prior to being used to cut, is clearly depicted, along with the metal framework and PVC tubing.

1 **Supplementary Material**

2

		Change Between Durability Conditions (%)				
		0 ↔ 1	0 ↔ 2	0 ↔ 3	0 ↔ 4	0 ↔ 5
Force (N)	Basalt	16.0	16.8	18.6	21.8	25.4
	Chert	33.7	32.6	33.9	35.4	33.0
	Quartzite	47.6	44.0	45.6	45.9	45.8
Work (J)	Basalt	39.6	40.4	51.9	51.5	63.3
	Chert	73.3	72.1	79.7	80.0	75.7
	Quartzite	182.1	148.8	145.8	154.3	156.2
Material Deformation (mm)	Basalt	17.5	18.8	24.6	23.7	30.6
	Chert	41.9	43.7	44.9	44.9	42.7
	Quartzite	72.0	65.5	63.8	66.3	66.4

3 **Supplementary Table 1:** Mean percentage increases for each sharpness metric, between the first
4 controlled cutting test, and then each sequential test after cutting a piece of wood.

5

		Durability Conditions 0 – 5					
		<i>(n = 15)</i>					
		0	1	2	3	4	5
Force (N)	Basalt	82.3	95.5	96.1	97.6	100.2	103.2
	Chert	36.9	49.3	48.9	49.4	49.9	49.1
	Quartzite	36.4	53.7	52.4	53.0	53.1	53.0
Work (J)	Basalt	1.36	1.90	1.91	2.07	2.06	2.22
	Chert	0.30	0.52	0.52	0.54	0.54	0.53
	Quartzite	0.28	0.79	0.70	0.69	0.72	0.72
Material Deformation (mm)	Basalt	32.3	37.9	38.3	40.2	39.9	42.1
	Chert	13.7	19.5	19.7	19.9	19.9	19.6
	Quartzite	14.0	24.0	23.1	22.9	23.2	23.2

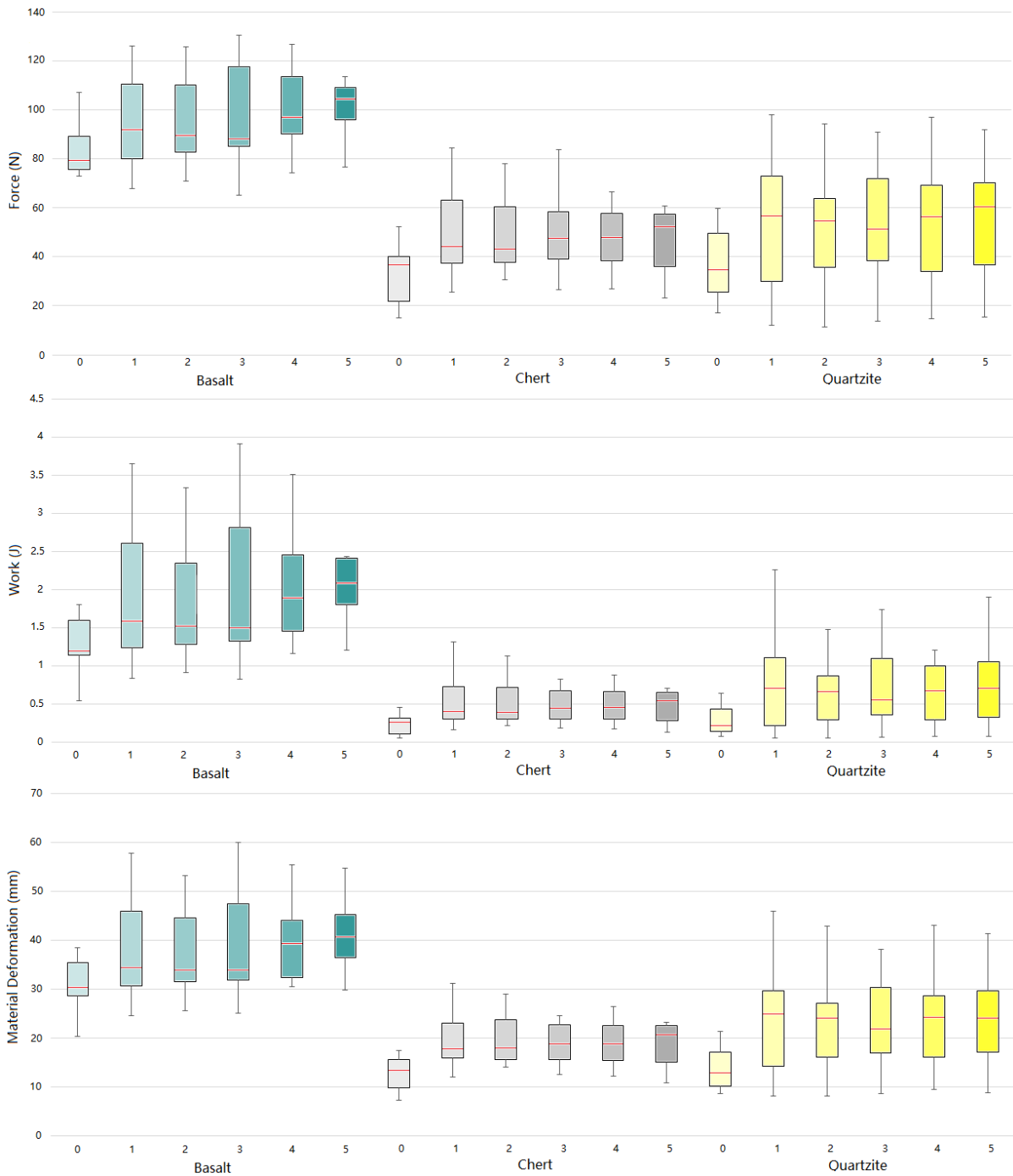
6 **Supplementary Table 2:** Mean force (N), work (J), and material deformation (mm) measures for the
7 three Olduvai raw materials during each of the six durability conditions.

8

		Mann-Whitney U Tests Between Durability Conditions				
		<i>(α = .05)</i>				
		0 ↔ 1	1 ↔ 2	2 ↔ 3	3 ↔ 4	4 ↔ 5
Force (N)	Basalt	.106	.836	.803	.590	.507
	Chert	.038	.934	.967	.967	.967
	Quartzite	.074	1	.967	1	.868
Work (J)	Basalt	.115	.836	.901	.803	.481
	Chert	.009	1	.967	.901	1
	Quartzite	.031	.934	1	.901	.868
Material Deformation (mm)	Basalt	.171	.836	.901	.934	.534
	Chert	.003	.934	1	.967	.967
	Quartzite	.013	.803	.901	.901	.967

9 **Supplementary Table 3:** Mann-Whitney U tests between sequential durability conditions for all
10 sharpness metrics and the three raw materials.

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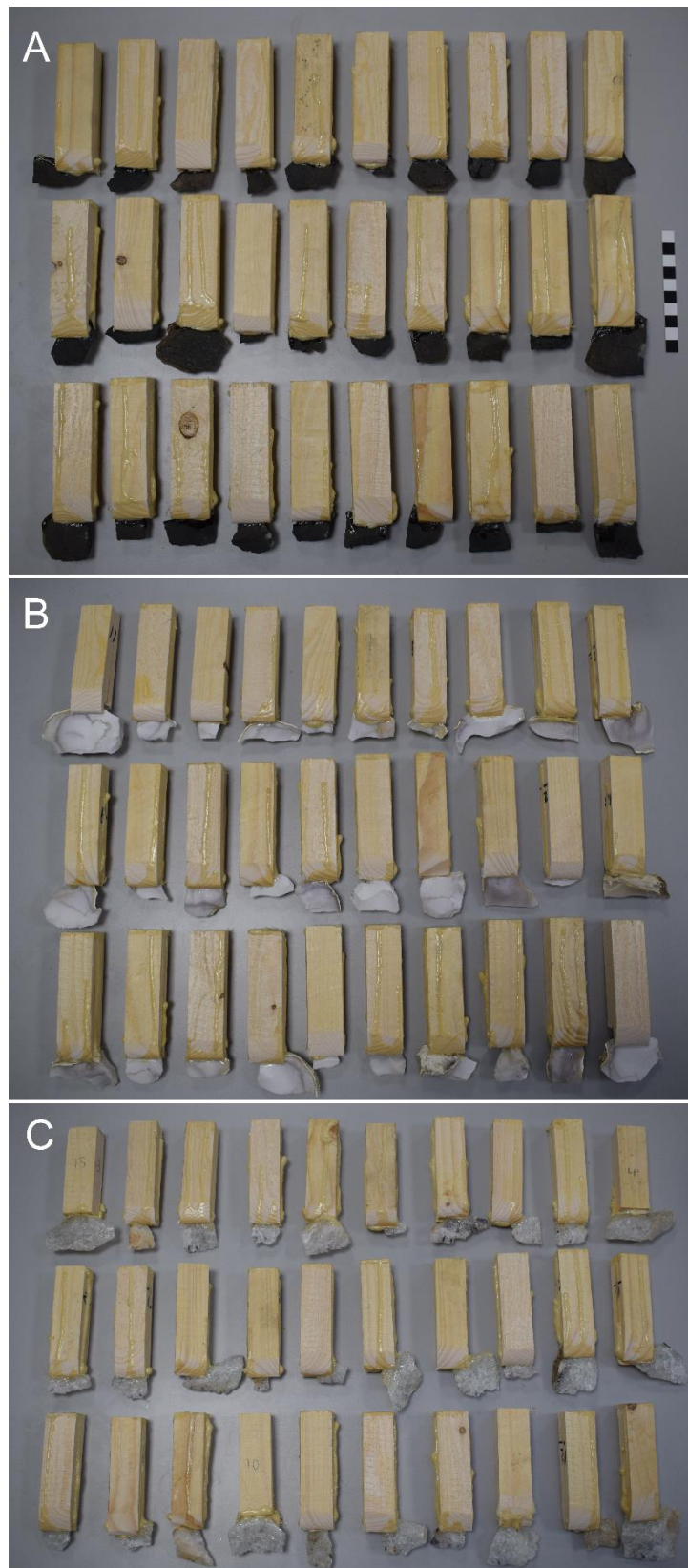
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3 **Supplementary Figure 1:** Force (N), work (J), and material deformation (mm) values for each
4 Olduvai raw material, across the six durability conditions (n = 15 for each).

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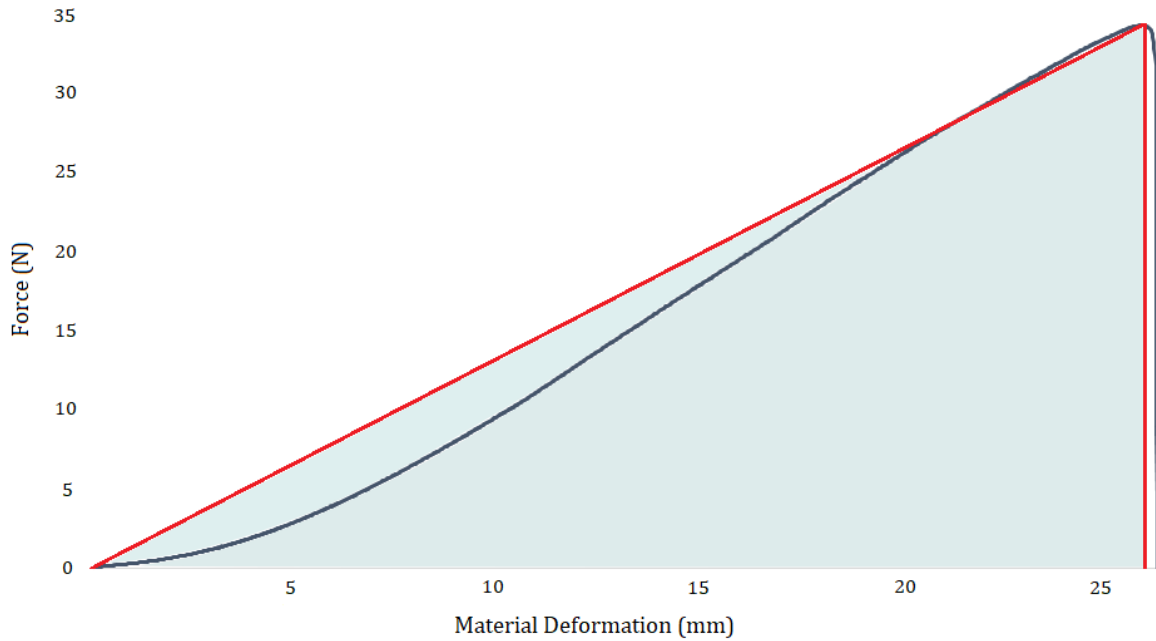
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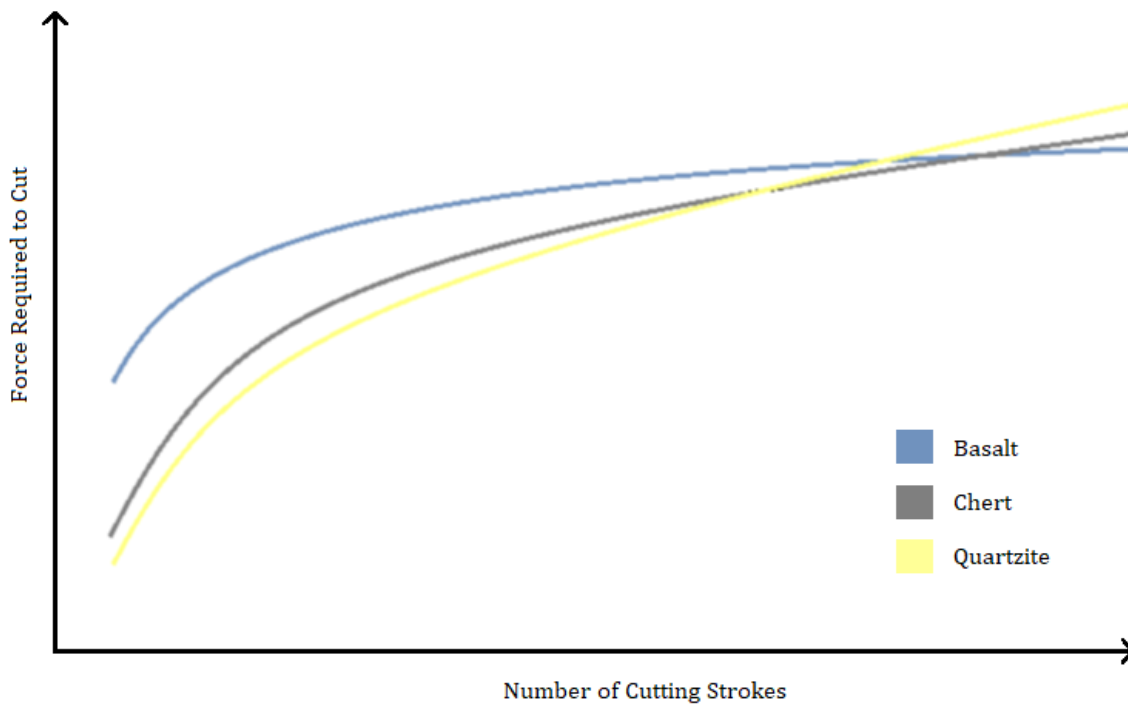
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2 **Supplementary Figure 2:** The 30 basalt (A), chert (B) and quartzite (C) stone flakes used in the
3 experiment. Here, each has been secured to the wooden blocks used to fix them to the upper arm of
4 the Instron device. Flakes with a cutting edge that is not perpendicular to the length of wood (and
5 therefore the 'standard' motion of cutting) had the block turned in the Instron's grip such that cutting
6 edges were always straight when cutting the tubing.



1

2 **Supplementary Figure 3:** An example load displacement (stress - strain) curve identifying the area
 3 used to calculate work (J) during a cut. The load displacement curve is depicted in dark blue while the
 4 idealised triangle is depicted in red. The light teal shaded area is the area used to calculate work.



5

6 **Supplementary Figure 4:** An illustration depicting how basalt would eventually overtake quartzite
 7 and chert in terms of cutting performance due to its increased edge durability. The work of Braun et
 8 al.¹¹ indicates that this point would likely be reached after a substantial number of cutting strokes had
 9 been performed, although this would be task dependent. The earliest stages of a tool's use account for
 10 the most rapid stages of blunting, before levelling off.