

1 **The Effects of Ultrasound Pressure and Temperature Fields in Millisecond**

2 **Bubble Nucleation**

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7 **Keywords:** Bubble Nucleation; HIFU; Histotripsy; Cavitation; Boiling.

8 **Declaration of interest:** none.

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10 **Abstract**

11 A phenomenological implementation of Classical Nucleation Theory (CNT) is employed to investigate the
12 connection between high intensity focused ultrasound (HIFU) pressure and temperature fields with the energetic
13 requirements of bubble nucleation. As a case study, boiling histotripsy in tissue-mimicking phantoms is
14 modelled. The physics of key components in the implementation of CNT in HIFU conditions such as the
15 derivation of nucleation pressure thresholds and approximations regarding the surface tension of the liquid are
16 reviewed and discussed. Simulations show that the acoustic pressure is the ultimate trigger for millisecond
17 bubble nucleation in boiling histotripsy, however, HIFU heat deposition facilitates nucleation by lowering
18 nucleation pressure thresholds. Nucleation thus occurs preferentially at the regions of highest heat deposition
19 within the HIFU field. This implies that bubble nucleation subsequent to millisecond HIFU heat deposition can
20 take place at temperatures below 100 °C as long as the focal HIFU peak negative pressure exceeds the
21 temperature-dependent nucleation threshold. It is also found that the magnitude of nucleation pressure
22 thresholds decreases with decreasing frequencies. Overall, results indicate that it is not possible to separate
23 thermal and mechanical effects of HIFU in the nucleation of bubbles for timescales of a few milliseconds. This

24 methodology provides a promising framework for studying time and space dependencies of the energetics of
25 bubble nucleation within a HIFU field.

26 **1. Introduction**

27 In recent years, an important shift in perspective has changed the way that cavitation is regarded in biomedical
28 ultrasound. Bubble activity induced by high intensity focused ultrasound has been shown to cause repeatable
29 mechanical disintegration of soft-tissue [1,2]. This method is termed histotripsy, where the growth and violent
30 collapse of vapour/gas bubbles fragments soft tissue into subcellular debris. Histotripsy has found potential
31 applications for the treatment of benign prostatic hyperplasia (BPH), liver and kidney tumours, enhancement of
32 anti-tumour immune response, tissue decellularisation and cell therapy [2,3].

33 Consequently, some research activity has shifted from designing protocols free from bubble activity [4-7] to
34 those which will take advantage of its bioeffects to perform non-invasive tissue disintegration [2]. There are
35 two traditional modes for the initiation of bubbles in histotripsy: cavitation-cloud histotripsy (CCH) [8,9], and
36 boiling histotripsy (BH) [10,11]. Both approaches use periodic pulses of ultrasound irradiation, but differ in
37 pulse duration and pulse repetition frequency (PRF).

38 In boiling histotripsy, pulse durations are usually of the order of 10 – 20 ms and low PRFs are employed. The
39 pulse duration is n cycles at the source frequency, and the PRF is the number of pulses delivered per second.
40 Non-linear propagation effects distort the acoustic waves, resulting in the formation of shocks at the HIFU
41 focus. The higher harmonics in these shockwaves are readily absorbed by the medium, causing intense heat
42 deposition until a vapour bubble is created at high temperatures. Conversely, in cavitation-cloud histotripsy, the
43 pulse durations are shorter ($1 \mu\text{s} - 1 \text{ms}$), but delivered more frequently. This ensures that no significant heat
44 deposition happens so that bubble nucleation is caused exclusively by the ultrasound tensile pressures or by the
45 interaction of incoming waves and those reflected from possible pre-existing bubbles. When bubble nucleation
46 can be repeatedly obtained with short ultrasound pulses, histotripsy is referred to as intrinsic histotripsy [2].

47 The extent of mechanical damage in histotripsy lesions has been argued to depend ultimately on the mechanical
48 properties of the target tissue subjected to bubble activity [12,13]. This places histotripsy as a potential form of
49 controlled, self-limiting therapy whose destructive action depends on the structural properties of tissue and the

50 onset of cavitation. However, a significant drawback in the clinical use of ultrasound-induced cavitation relates
51 to the highly uncertain character of bubble nucleation in acoustic fields [14]. Such uncertainty could arguably
52 have been responsible for the slower development and clinical application of ultrasonic therapies that use bubble
53 activity compared to those only using thermal effects. Currently, most Food and Drug Administration (FDA)
54 approved modes of ultrasound therapy use thermal modes of HIFU only [14]. Indeed, the controlled nucleation
55 of bubbles in living tissue has been regarded as one of the central challenges in the biomedical applications of
56 ultrasound [15,16].

57 Research into vapour-phase nucleation and bubble activity in water has mostly involved simulations of bubble
58 dynamics [17-19]. This methodology relies on the assumption that stabilised gas pockets nucleate spontaneously
59 at some time before HIFU sonication and survive in body fluids [20,21]. The main issue with this hypothesis is
60 the very slim chances of survival of unstabilised microbubbles in such media. Gas bubbles in liquids tend to
61 dissolve away due to Laplace pressure in the absence of a stabilising force [20-24]. Furthermore, assuming the
62 existence of stabilised bubbles in soft-tissue also proposes that the content of body fluids is comparable to that
63 of untreated water systems. In untreated water systems, preferential nucleation sites are normally hydrophobic
64 crevices where gas is trapped or free-flowing gas bubbles [23,25]. However, review of a number of studies
65 concluded that no hydrophobic crevices had ever been observed in tissues or capillaries [23].

66 Despite the availability of sophisticated methods for modelling the interactions between acoustic fields and
67 bubbles [26,27], there still remain unknowns regarding the thermodynamic conditions needed for the onset of
68 cavitation in HIFU. Similarly, the specific contributions of both temperature and pressure to this process and
69 their own interactions are unexplored. Such gaps in the understanding of HIFU-induced nucleation hinders the
70 ability to control and predict the spatial extent of the mechanical effects of HIFU bubbles, as much as estimating
71 the timescales at which bubble-mediated phenomena take place.

72 One possibility for investigating bubble formation in HIFU fields is to use classical nucleation theory. The
73 classical theory has been put aside in the field of biomedical ultrasound due to overestimated predictions for
74 pressure thresholds under poor physical assumptions. Nevertheless, it has been recently shown that ultrasound
75 cavitation can be modelled with the aid of CNT provided that the surface tension of water is corrected to an

76 effective value [15,28,29]. A similar approach has been successfully applied to therapeutic ultrasound [15]. This
77 resulted in the development of what is referred to as the intrinsic threshold for cavitation in HIFU [29].

78 HIFU pressure and temperature fields are a unique scenario to study bubble nucleation. The possibility of
79 subjecting small focal volumes to very negative pressures during short time intervals reduces the probability
80 that minute impurities will affect the nucleation threshold [30]. The latter would be a case of heterogeneous
81 nucleation (HEN). In HEN, impurities locally change the surface tension of the liquid and nucleation pressure
82 thresholds often differ to those predicted by theoretical approaches. It is important to point out that, contrary to
83 common belief, heterogeneous nucleation is not a phenomenon that necessarily reduces nucleation pressure
84 thresholds. It has been argued in the literature that impurities can be of the destabilising type, which reduces
85 nucleation pressure thresholds, or of the stabilising type, which increases these thresholds [28,31,32].

86 In this work, classical nucleation theory is employed to investigate the connection between the ultrasound
87 protocol with the energetic requirements of bubble nucleation in HIFU and the thermodynamic properties of
88 newly nucleated bubbles. As a case study, boiling histotripsy in tissue-mimicking phantoms is modelled [33].
89 Nonetheless, this methodology can be extended to the study of HIFU-induced bubble nucleation in most systems
90 with high water content given appropriate parametrisation. Such a fundamental approach was chosen due to the
91 unsuitability of macro-scale fluid dynamics to explain bubble formation, leaving reasonably complicated
92 experiments as the only source of insight into HIFU-induced bubble nucleation [15,28,29]. Likewise,
93 understanding the thermodynamics of bubble nucleation in HIFU pressure and temperature fields is arguably a
94 key component in the planning of HIFU protocols in terms of defining safety windows and establishing best
95 practices.

96 This paper addresses key components in the implementation of CNT for HIFU applications such as (a) the
97 derivation of nucleation pressure thresholds from thermodynamic principles; (b) the approximations for the
98 surface tension of the liquid; (c) the effects of ultrasound frequency and focal volume on the onset of nucleation
99 and (d) the different physical mechanisms underlying bubble nucleation at high or low temperatures, i.e. boiling
100 or cavitation respectively. Furthermore, HIFU pressure fields obtained from a Khokhlov–Zabolotskaya–
101 Kuznetsov (KZK) model and temperature fields obtained via the Pennes’ Bio-Heat Transfer Equation are
102 plugged into CNT models. This allows the estimation of the timescales of bubble nucleation in boiling

103 histotripsy, spatial maps for nucleation pressure thresholds, the size of critical bubble nuclei at the HIFU focus
104 and the prediction of the region where bubbles first nucleate.

105 **2. Theory and Methods**

106 **2.1. The Critical Work of Nucleation**

107 Liquids are notable for their ability to withstand tensile (negative) pressures before a gas phase appears, entering
108 a metastable state [34]. Metastable liquid phases are those where the fluid is stretched beyond its vapour pressure
109 or superheated above the boiling point [35,36]. In HIFU, both these mechanisms can induce liquid-phase
110 metastability at the focus. Metastability is only viable because phase transformations are delayed by the
111 energetic cost of creating an interface for a bubble in the bulk of a liquid [36]. This delay is manifested as an
112 energy barrier which needs to be overcome before phase transitions take place [37].

113 The work required for the nucleation of a bubble of radius r in a liquid is given by [36]

$$W(r) = (4\pi r^2)\sigma + \left(\frac{4\pi r^3}{3}\right)(P_L - P') + \left(\frac{4\pi r^3}{3}\right)\frac{P'}{k_B T}\Delta\mu, \quad (1)$$

114 where σ is the liquid's surface tension, P_L is the pressure in the liquid, P' is the pressure inside a newly formed
115 vapour nucleus, k_B is Boltzmann's constant, and T is the temperature in the liquid. The supersaturation of the
116 system $\Delta\mu = \mu_L - \mu_V$ is represented by the difference in chemical potentials between the liquid and vapour
117 phase. This equation is obtained under the assumption that vapours behave as ideal gases and the surrounding
118 liquid is incompressible.

119 The size-dependent work needed to nucleate a bubble increases to a maximum at the critical radius of nuclei r^* ,
120 and then starts to decrease. This is represented mathematically as $dW/dr|_{r=r^*} = 0$. At this maximum, the
121 bubble nucleus can be assumed to be in thermodynamic equilibrium with the liquid ($\Delta\mu = 0$) [38]. The critical
122 size can be obtained by applying these conditions to Eq. 1, resulting in a Young-Laplace-type equation:

$$r^* = \frac{2\sigma}{P' - P_L}. \quad (2)$$

123 The critical work of nucleation W^* can then be derived by replacing r^* in Eq. 1 and considering thermodynamic
 124 equilibrium ($\Delta\mu = 0$):

$$W^* = \frac{16\pi}{3} \frac{\sigma^3}{(P' - P_L)^2}. \quad (3)$$

125 **2.2. Nucleation Rates**

126 The critical work for nucleation is used to predict the nucleation rate. This is the net rate at which bubbles reach
 127 the critical size and is proportional to the difference between the forward rates of vaporisation and the backward
 128 rates of condensation [39]. At sufficiently high nucleation rates, the control volume under consideration cannot
 129 be considered a single-phase volume anymore. The pressure and temperature in the liquid at this point can be
 130 seen as the nucleation threshold of this system.

131 Assuming that the timescales of nucleation are much shorter than the tensile period of the ultrasound wave, the
 132 nucleation rate can be approximated as a stationary quantity. This is an equilibrium average in time and space
 133 for the number of critical nuclei formed in the system under consideration. At the critical size, the steady-state
 134 nucleation rate is usually represented as [31]

$$J_S = J_0 \exp(-W^*/k_B T). \quad (4)$$

135 In this equation, the pre-exponential term J_0 accounts for the average kinetic and spatial properties of nucleation.
 136 It also defines, mathematically, an upper bound for the nucleation rate since $J_S \rightarrow J_0$ for $W^* \rightarrow 0$. On the other
 137 hand, the exponent is a thermodynamic term, describing the non-dimensional energy of formation of a critical
 138 nucleus. By neglecting the effects of viscosity and inertia in the liquid, J_0 can be defined in the form [36,39]

$$J_0 = N_0 \sqrt{\frac{2\sigma}{\pi m}}, \quad (5)$$

139 having $N_0 = \rho_L/m$ where ρ_L is the liquid density and m is the molecular mass of the liquid.

140 For steady-state nucleation, the number of critical nuclei Σ formed in the volume V_0 during a time interval τ_S
141 can be approximated by

$$\Sigma = V_0 \int_0^{\tau_S} J_S(P_L, T) dt, \quad (6)$$

142 where J_S is the nucleation rate in a liquid at a pressure P_L and temperature T [36,40]. The definition of J_S in Eq.
143 4 is time independent, but the acoustic field causes P_L and T to be transient. Thus, we assume that the integration
144 interval τ_S is sufficiently small so that no appreciable changes in J_S occur due to variations in T and P_L . Σ can
145 then be approximated as

$$\Sigma \cong J_S V_0 \tau_S. \quad (7)$$

146 Considering the formation of the first Σ nuclei, we can define

$$J_S = \frac{\Sigma}{V_0 \tau_S}, \quad (8)$$

147 where J_S is the phenomenological nucleation rate for the appearance of Σ nuclei in a volume V_0 after τ_S seconds.
148 Having that V_0 is a control volume where Σ bubbles nucleate after τ_S seconds, the value of this parameter is
149 assumed to be the volume within the 3 dB drop in intensity at the transducer focus. Therefore, the choice of V_0
150 depends on the transducer geometry.

151 The quantity τ_S defines the time interval over which the first Σ bubbles nucleate. This is also referred to as the
152 “mean-lifetime of the metastable fluid” [41,42], the “average time of formation of the first supercritical nucleus”
153 [43] or the “experiment/observation time” at the steady state [44]. The attainable length of this quantity is known
154 to decrease as metastability increases, making the measurement of thermodynamic properties deep in the
155 metastable region difficult or even practically impossible [28,36].

156 Thermodynamically, the value of τ_S should be larger than the time-lag of nucleation, i.e. a measure of the
157 timescales needed for the nucleation rate to reach its steady-state value given by Eq. 4. Values for the time-lag

158 of nucleation have been shown to be of the order of nanoseconds for vapour bubble nucleation in water [31].
159 Moreover, the choice of τ_S needs to be such that variations in P_L and T are minimal and these quantities can be
160 assumed nearly constant. Thus, parametrisation of τ_S is constrained by the interactions between the ultrasound
161 source, the propagating medium and resulting heat deposition.

162 Approximating the integral in Eq. 6 in the form of Eq. 7 means that, in HIFU, τ_S should be modelled as a
163 fraction of the ultrasound wave where pressure values are the lowest and remain reasonably constant. Therefore,
164 τ_S was approximated as $(1/10f)$, where f is the ultrasound frequency. This ensures that P_L variations within
165 this time interval are negligible, i.e. $P_L(t - \tau_S/2) \approx P_L(t) \approx P_L(t + \tau_S/2)$, where t is time. It also guarantees
166 that τ_S is sufficiently smaller than the timescales for gas diffusion in liquids, so diffusion can be neglected and
167 the nucleating medium is modelled as water.

168 The attenuation of sound waves in non-ideal, inhomogeneous media is given by the combined effects of
169 absorption, diffraction and scattering, following a power law with respect to the frequency [66]. Assuming $\tau_S =$
170 $(1/10f)$ will result in large values of τ_S at low frequencies (100 – 1000 kHz), which would allow sufficient
171 time for heat deposition in the medium and cause an increase in temperature. However, following the power
172 law of attenuation, absorption can be neglected at low frequencies and the focal region is thought not to undergo
173 significant temperature variations during τ_S . Conversely, acoustic absorption is appreciable in the megahertz
174 frequency range (1 – 10 MHz). Nonetheless, heat deposition can be equally neglected because τ_S is of the order
175 of nanoseconds and the focal temperature can be assumed nearly constant over such timescales.

176 **2.3. Nucleation Pressure Thresholds**

177 Having the nucleation rate J_S that forms the first Σ nuclei in a time-volume setup $V_0\tau_S$, a phenomenological
178 approximation to the nucleation pressure threshold of a liquid can be obtained by solving Eqs. 4 and 8 in terms
179 of the pressure in the liquid P_L . This approach for obtaining the temperature-dependent nucleation pressure
180 threshold $P_L^N(T)$ was first employed in [45] and has also been used in more recent publications [44,46].

181 The nucleation pressure threshold has also been referred to as tensile strength, cavitation pressure or intrinsic
182 threshold in the literature [24,29,38,42,45]. In this paper, the terminology “cavitation pressure/threshold” is
183 avoided. This is because such nomenclature has been mostly used to describe the phenomenon of detectable

184 bubble activity in a liquid that is not necessarily depleted of microbubbles [24]. Nucleation, on the other hand,
 185 is viewed as the mechanism by which a first-order phase transition happens [31].

186 Equating the thermodynamic (Eq. 4) and the phenomenological (Eq. 8) expressions for the nucleation rate,
 187 replacing the critical work of nucleation given by Eq. 3 and solving for P_L gives

$$P' - P_L^N = \left(\frac{16\pi\sigma^3}{3k_B T \ln\left(\frac{J_0 V_0 \tau_S}{\Sigma}\right)} \right)^{\frac{1}{2}}. \quad (9)$$

188 In this expression, P_L^N is the pressure P_L in the liquid at which an average of Σ nuclei appear during a time
 189 interval τ_S in a homogeneous volume of liquid V_0 at a temperature T . A Poynting correction allows the vapour
 190 pressure P_V of the liquid to be used instead of the nucleus internal pressure P' [38,39]. At high pressures, these
 191 are different quantities because of the assumption of thermodynamic equilibrium $\Delta\mu = 0$ used to obtain Eq. 3.
 192 The pressure drop ($P' - P_L$) can be accurately approximated by

$$(P' - P_L) = \zeta(P_V - P_L) \quad (10)$$

193 having

$$\zeta = 1 - \left(\frac{\rho_V}{\rho_L}\right) + \frac{1}{2}\left(\frac{\rho_V}{\rho_L}\right)^2, \quad (11)$$

194 where ρ_V and ρ_L denote the saturated densities of vapour and liquid water, respectively [39].

195 The nucleation pressure threshold then assumes the form

$$P_L^N = P_V - \frac{1}{\zeta} \left(\frac{16\pi\sigma^3}{3k_B T \ln\left(\frac{J_0 V_0 \tau_S}{\Sigma}\right)} \right)^{\frac{1}{2}}. \quad (12)$$

196 This quantity can be evaluated by using standard thermodynamic quantities such as the vapour pressure of the
 197 liquid P_V and its density in the liquid and vapour phases. In order to calculate P_V , the International Association
 198 for the Properties of Water and Steam (IAPWS) expression for the vapour pressure of water was used [47]

$$\ln\left(\frac{P_V}{P_C}\right) = (\alpha_1 x + \alpha_2 x^{1.5} + \alpha_3 x^3 + \alpha_4 x^{3.5} + \alpha_5 x^4 + \alpha_6 x^{7.5}) T_r^{-1}. \quad (13)$$

199 In this equation, P_C is the critical pressure of water and $x = 1 - T_r$, where T_r is the reduced temperature T/T_C
 200 having T_C as the critical temperature of water. The values for α are $\alpha_1 = 7.85951783$, $\alpha_2 = 1.84408259$, $\alpha_3 =$
 201 11.7866497 , $\alpha_4 = 22.6807411$, $\alpha_5 = 15.9618719$ and $\alpha_6 = 1.80122502$. For the calculation of P' , the IAPWS
 202 equations for the densities of the saturated liquid ρ_L and vapour phases of water ρ_V were employed such that

$$\rho_L = \rho_c \left(1 + b_1 x^{\frac{1}{3}} + b_2 x^{\frac{2}{3}} + b_3 x^{\frac{5}{3}} + b_4 x^{\frac{16}{3}} + b_5 x^{\frac{43}{3}} + b_6 x^{\frac{110}{3}}\right), \quad (14)$$

203 and

$$\ln\left(\frac{\rho_V}{\rho_c}\right) = c_1 x^{\frac{2}{6}} + c_2 x^{\frac{4}{6}} + c_3 x^{\frac{8}{6}} + c_4 x^{\frac{18}{6}} + c_5 x^{\frac{37}{6}} + c_6 x^{\frac{71}{6}}. \quad (15)$$

204 In Eqs. 14 and 15, ρ_c is the critical density of water. The values for constants b given by $b_1 = 1.99274064$,
 205 $b_2 = 1.09965342$, $b_3 = -0.510839303$, $b_4 = -1.75493479$, $b_5 = -45.5170352$, $b_6 = -6.74694450 \times 10^5$. The
 206 values of c are as follows $c_1 = -2.03150240$, $c_2 = -2.68302940$, $c_3 = -5.38626492$, $c_4 = -17.2991605$, $c_5 =$
 207 -44.7586581 , and $c_6 = -63.9201063$.

208 **2.4. The Effective Surface Tension**

209 Equations 3, 4 and 12 show, respectively, the dependence of the nucleation work, nucleation rate and the
 210 nucleation threshold on the liquid's surface tension σ . Indeed, the surface energy is a substantial component of
 211 the energetics of nucleation. Under special assumptions, it can be shown that W^* equals about one third of the
 212 surface energy of the metastable liquid in question [31]. The surface tension is a macroscopic manifestation of
 213 the cohesion of matter [48]. The high surface tension of water, for instance, is thought to be connected to strong
 214 hydrogen bonds and the high energies involved in breaking and rearranging them into a surface [49].

215 The actual surface tension σ of bubbles at the moment of nucleation is thought to be size, pressure and
 216 temperature dependent [31,50,51]. However, it is common to approximate it with a temperature-dependent

217 planar surface tension $\sigma_\infty(T)$ in CNT. An expression for σ_∞ can be obtained from a revision of the 1994 IAPWS
218 Secretariat release [52]

$$\sigma_\infty(T) = \sigma_1(1 - T_r)^{\sigma_2} [1 + \sigma_3(1 - T_r)], \quad (16)$$

219 In Eq. 16, $\sigma_1 = 235.8 \times 10^{-3} \text{ Nm}^{-1}$, $\sigma_2 = 1.256$ and $\sigma_3 = -0.625$.

220 In CNT, expressions for the surface tension like Eq. 16 are traditionally used for modelling boiling and
221 cavitation [28,38]. The planar surface tension σ_∞ is the limiting value of σ for $r \rightarrow \infty$, i.e. a planar interface.
222 This is referred to as the capillarity approximation [31,53]. It is important to highlight that the capillarity
223 approximation is heuristic and not intrinsic to CNT [36,53,54].

224 Indeed, the discrepancy between theoretical and experimental results in the nucleation of bubbles in water has
225 been consistently associated with the capillarity approximation [31,48-51,55]. If the capillarity approximation
226 is used, CNT predicts tensile pressures of about -150 MPa for bubble nucleation in water at ambient temperature,
227 whereas most experiments do not surpass -40 MPa [34]. Furthermore, CNT models are unable to account for a
228 vanishing energy barrier $-W^*/k_B T$ as the liquid approaches its limit of stability, called the liquid spinodal
229 [56,57]. Alternative approaches have been developed to account for this shortcoming in CNT's implementation.
230 Density-functional theory (DFT) [50,51] models the continuous change in density between the liquid and vapour
231 phases, and does not evoke a capillarity approximation. Alternatively, molecular dynamics (MD) simulations
232 [41,42,49,54] model nucleation from the attractive-repulsive forces between molecules.

233 Researchers have also attempted to find phenomenological scaling factors which could correct the surface
234 tension or the nucleation work so these would match experiments [38,57]. Recently, nucleation rates obtained
235 in sophisticated HIFU experiments have been used in Eq. 4 in order to approximate an "effective value" of σ_∞
236 up to temperatures of 200 °C [28]. These experiments found that using a surface tension approximated by 23.7%
237 of σ_∞ could model HIFU nucleation pressure thresholds in CNT with a good agreement to experimental results.
238 Similar experiments have been performed more recently up to 90°C [29]. The latter reported similar results,
239 however with a scaling value ranging from 25% to 27.5% for the surface tension of water.

240 Drawing from these findings, a temperature-dependent scaling factor c_E for the surface tension was calculated
 241 such that $\sigma_E = c_E(T)\sigma_\infty(T)$. This methodology was found to harmonise CNT and HIFU experimental results
 242 with better accuracy than a single scaling value for all temperatures. This was achieved by optimising in c_E the
 243 absolute error between analytic predictions of Eq. 12 and experimental data for nucleation pressure thresholds
 244 in acoustic fields from aforementioned studies.

245 Using temperature-dependent HIFU nucleation pressure thresholds from experimental works in the literature
 246 [28-30,58], $c_E(T)$ was calculated by minimising the absolute error given by Eq. 17 for each temperature.

$$E(c_E(T_{EXP})) = \sqrt{(P_L^N(T_{EXP}, c_E) - P_{EXP})^2}. \quad (17)$$

247 In Eq. 17, P_{EXP} and T_{EXP} represent, respectively, experimental values of the nucleation pressure threshold and
 248 the temperature at which they were obtained. Moreover, $P_L^N(T_{EXP}, c_E)$ represents the predictions of Eq. 12 for
 249 pressure thresholds at a temperature T_{EXP} and a scaling factor c_E . In this work V_0 was calculated as an ellipsoidal
 250 focal volume within the - 3dB drop region for a 2 MHz HIFU transducer (Sonic Concepts H106) as specified
 251 by the manufacturer.

252 Values of c_E previously published in the literature use either a constant kinetic term [59] or have been obtained
 253 as a single value for a wide temperature range [28]. Herein, data from the aforementioned studies is combined
 254 with a pressure and temperature-dependent kinetic factor in order to obtain a linear dependence for c_E on the
 255 liquid's temperature. For $0^\circ\text{C} < T < 90^\circ\text{C}$, this relationship reads:

$$c_E(T) = 0.4869 - 6.1425 \cdot 10^{-4}(T + 273.15), \quad (18)$$

256 where T is the temperature in Celsius.

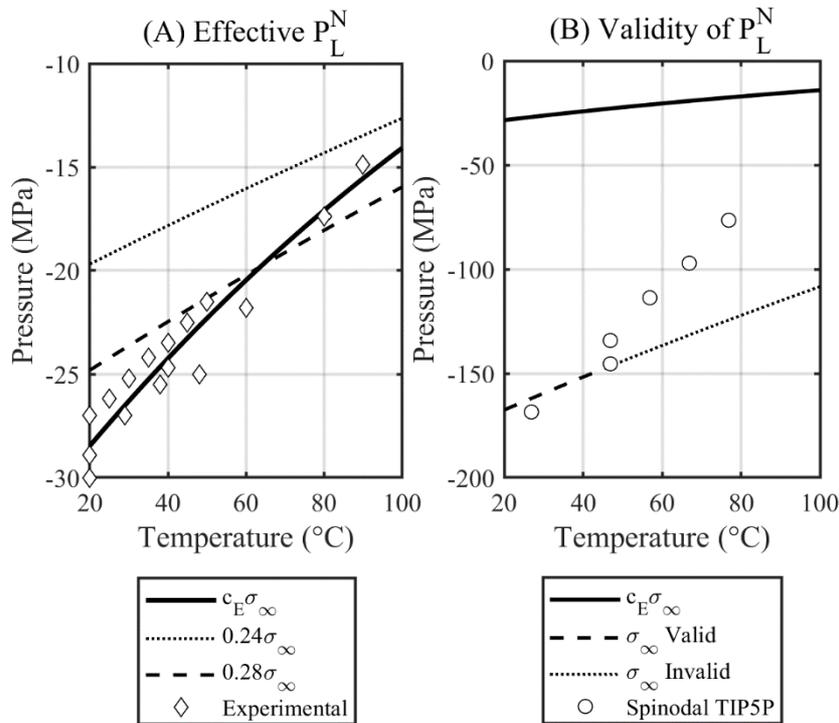
257 It follows that the effective surface tension for HIFU-induced bubble nucleation is approximated as $\sigma_E(T) =$
 258 $c_E(T)\sigma_\infty(T)$. For temperature values between 90 and 110 °C, c_E is extrapolated based on Eq. 18. For
 259 temperature values above 110 °C a conservative approach is taken and a constant c_E is assumed, such that
 260 $c_E(T > 110^\circ\text{C}) = c_E(110^\circ\text{C})$.

261 **3. Results and Discussion**

262 **3.1. The Effects of the Surface Tension on Nucleation Pressure Thresholds**

263 Figure 1-A compares P_L^N values obtained for $c_E\sigma_\infty$ (solid line), values obtained for a scaled planar surface
 264 tension as 24% and 28% of σ_∞ [28,29] and experimental results in HIFU nucleation [28-30,58]. Fig. 1-A shows
 265 the better agreement of P_L^N to experimental results for the temperature-dependent c_E given by Eq. 18. Values of
 266 P_L^N obtained for scaling at 24% and 28% of σ_∞ are good approximations for the order of magnitude of P_L^N
 267 however fail to be consistent throughout the temperature range of interest in HIFU applications.

268 Moreover, Fig. 1-B compares the values of P_L^N obtained from a planar surface tension (dashed and dotted line)
 269 with a temperature-dependent “effective” surface tension $c_E\sigma_\infty$ (solid line). White circles represent the liquid
 270 spinodal pressure of water obtained from DFT simulations for the five-site transferable interaction potential
 271 (TIP5P) equation of state [55]. This is an equation of state derived from the TIP5P model of water, describing
 272 its properties within the realm of molecular dynamics at low temperatures. It can be seen in Fig. 1-B that
 273 nucleation pressure thresholds calculated using σ_∞ yield quantities far below the spinodal pressure of liquid
 274 water [34,60,61].



275

276 Figure 1. (A) Comparison between a temperature-dependent scaling $c_E(T)$ given by Eq. 18 for the surface tension to
277 constant values of 24% and 28%. (B) Temperature-dependent nucleation pressure threshold in water for a planar surface
278 tension σ_∞ given by Eq. 16 and an effective surface tension $c_E\sigma_\infty$ obtained with Eqs. 16 and 18. Dotted values show
279 CNT predictions which are below the liquid spinodal pressure of water obtained by the TIP5P, which is represented in
280 white circles.

281 This a known limitation of CNT if the surface tension is approximated with size-independent expressions, such
282 as the planar surface tension approximation. In these cases, CNT is not able to account for a vanishing work of
283 nucleation W^* as pressures approach the spinodal pressures of water [31]. The spinodal of a liquid is the limit
284 between its metastable and unstable regions. As the liquid's pressure approaches the spinodal, density
285 fluctuations grow without limit due to a divergent liquid compressibility [44]. It follows that at the spinodal, the
286 free energy barrier that delays nucleation disappears, and a new phase forms spontaneously in an alternative
287 process to nucleation, termed spinodal decomposition [36]. Therefore, predictions of P_L^N that are below the
288 values for the spinodal pressure of water should be deemed invalid.

289 **3.2. Physical Rationale for Nucleation Pressure Thresholds and the Regimes of Boiling** 290 **and Cavitation**

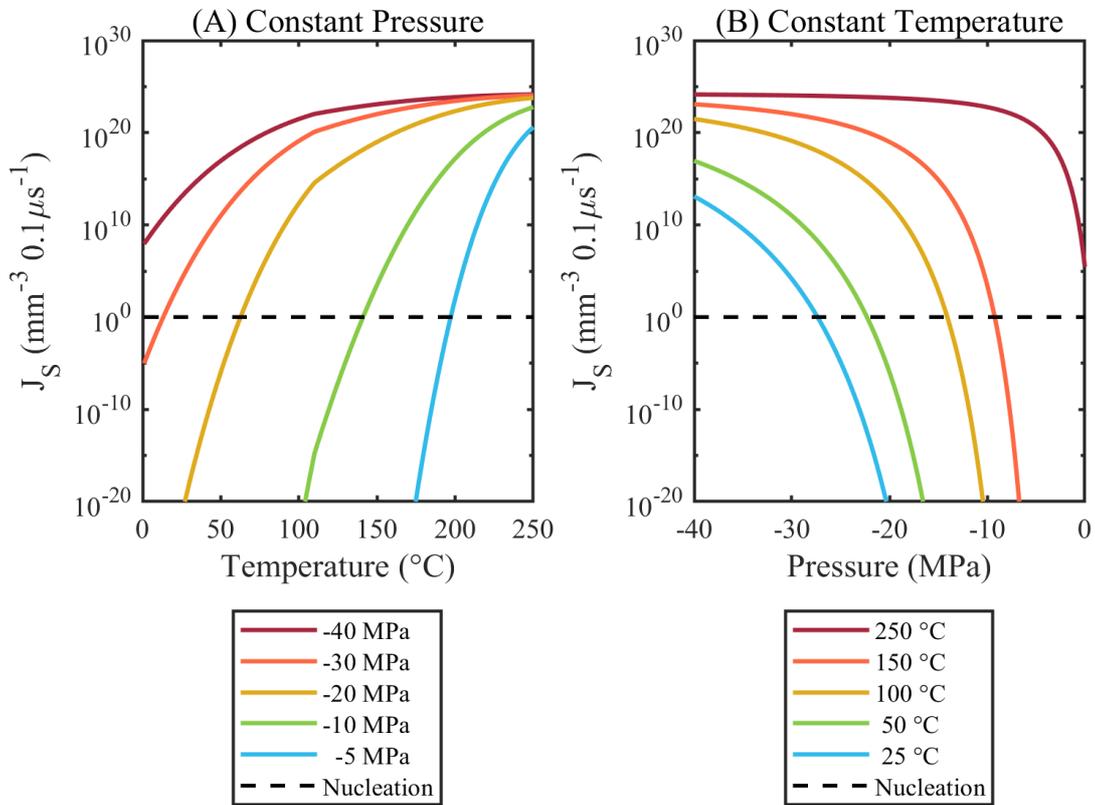
291 In Fig. 2, the steady-state nucleation rate given by Eq. 4 is shown as a function of temperature for several
292 pressure contours (-40, -30, -20, -10 and -5 MPa) in 2-A, and as a function of pressure for several temperature
293 contours (25, 50, 100, 150 and 250 °C) in 2-B. These values are in units of the number of bubble nuclei per
294 millimetre cubic per 0.1 microseconds, which are length and timescales compatible with HIFU.

295 The dashed line indicates the formation of at least one bubble nucleus ($\Sigma = 1$) in an ellipsoidal volume $V_0 = 1.73$
296 mm^3 after a time interval of $\tau_S = (1/10f) = 50$ ns for a given pressure-temperature pair. This approximation
297 for V_0 is valid under the assumption that the focus of a 2 MHz transducer (Sonic Concepts, H106) is an
298 axisymmetric ellipsoid with axial and lateral half width dimensions of 2.86 and 0.365 mm, as specified by the
299 manufacturer.

300 Figure 2 exemplifies the phenomenological approach to nucleation used in this work. Eq. 4 states that any given
301 pair of pressure and temperature (P_L, T) will be associated to a certain nucleation rate $J_S(P_L, T)$. Moreover, Eq.

302 8 postulates that there is a critical value of J_S which is approximately $\Sigma/V_0\tau_S$ at which the system cannot be
 303 considered single-phased anymore.

304 For $\Sigma = 1$, this value is marked by a dashed line in Fig. 2. Thus, at a given temperature T , a nucleation pressure
 305 threshold P_L^N is the value of the pressure in the liquid for which the curve of J_S given by Eq. 4 intersects the line
 306 given by $1/V_0\tau_S$. Values of J_S above $1/V_0\tau_S$ indicate nucleation rates which can be interpreted as bubble
 307 formation, whilst values below it indicate rates that are too low for the onset of bubble activity. It is important
 308 to highlight that within the current phenomenological implementation where J_S is obtained for a pure liquid,
 309 values of $J_S \gg 1/V_0\tau_S$ are more theoretical than of practical value.



310

311

Figure 2. Effects of pressure and temperature on the nucleation rate.

312

313

314

Results in Fig. 2 show how pressure and temperature affect the nucleation rate in different ways depending on the thermodynamic state of the liquid. Fig. 2-A shows that at temperatures above 100 $^{\circ}\text{C}$, a 10 MPa change in pressure will not have as significant of an effect in J_S than it would at temperatures lower than 50 $^{\circ}\text{C}$, as shown

315 by the contours of -40, -30 and -20 MPa. In such a case, nucleation at high temperatures is controlled by the
316 superheating of the system.

317 This can be further verified by noticing that the curves for -40 and -30 MPa plateau at temperatures much lower
318 than those for -20, -10 and 0 MPa in Fig. 2-A. Indeed, the curves of the nucleation rate as a function of
319 temperature are steeper at less negative pressures (-20, -10 and -5 MPa). This indicates behaviour similar to
320 explosive boiling: appreciable increases in the nucleation rate for small temperature variations. These are
321 important trends that should be kept in mind, considering that in the presence of non-linear heating some HIFU
322 protocols are notable for inducing temperature rises of over 60 °C in a few milliseconds [11].

323 Moreover, it can be seen in Fig. 2-B that for nucleation at very negative pressures, a change in temperature will
324 not affect J_S significantly at high temperatures (100-250 °C). In contrast, nucleation rates are at least 5 orders
325 of magnitude higher between temperature contours of 50 and 25 °C. This indicates that the pressure of the liquid
326 becomes more relevant in nucleation at lower temperatures. A similar trend was also observed in a
327 sonocrystallisation process where solid crystals are created out of a supersaturated solution exposed to
328 ultrasound [72,73]. The authors reported that the effect of pressure on nucleation is more pronounced at lower
329 supersaturation ratios.

330 These results explain how HIFU-induced bubble nucleation can be driven by two factors: very low pressures
331 [15] or high temperatures [11]. Indeed, histotripsy protocols have been broadly named cavitation-cloud
332 histotripsy (CCH) and boiling histotripsy (BH), deriving from the sense that bubble nucleation at high
333 temperatures is termed boiling and bubble nucleation at lower temperatures and very low pressures is termed
334 cavitation. Results shown in Fig. 2 corroborate with this terminology, showing that stretching and heating the
335 system affect the nucleation rate in different ways depending on the initial temperature of the system.

336 **3.3. Effects of Ultrasound Frequency on Pressure Thresholds**

337 The interpolation for c_E in Eq. 18 was obtained for HIFU nucleation data performed at frequencies lower than
338 2 MHz. It is therefore important to assess the effects of the ultrasound frequency in nucleation when using CNT.
339 In this study, the mean lifetime of the metastable fluid τ_S is, effectively, the time the fluid is placed at nearly
340 constant pressure and temperature before nucleation. The dependence of the nucleation pressure threshold P_L^N

341 on the mean-lifetime of a metastable fluid described by Eq. 12 is shown in Fig. 3 as a function of frequency,
 342 where $\tau_s = (10f)^{-1}$. From Eq. 12, the magnitude of P_L^N is expected to decrease at slow rates for an increasing
 343 mean lifetime τ_s [45]. This dependence describes the time interval needed for underlying energetic phenomena
 344 to take place in nucleation, and is not related to bubble oscillations in an acoustic field. Such a trend somehow
 345 agrees with the predictions of the Mechanical Index (MI) [16]. The MI states, following from experimental
 346 observations, that ultrasound-induced cavitation is more likely at lower frequencies.

347 Figure 3 shows P_L^N at 38 °C as a function of the ultrasound frequency from 0.1 Hz to 10 MHz and the focal
 348 volume from 1 mm³ to 1 cm³. The vector gradient in Fig. 3-A shows a greater decrease in the magnitude of P_L^N
 349 in the direction of bigger volumes and lower frequencies. This means that the nucleation pressure threshold
 350 decreases at lower frequencies. As an example, the difference in P_L^N at 20 °C between 1 MHz and 2 MHz is
 351 approximately 0.16 MPa for a focal volume of 1 mm³ and approximately 0.14 MPa for a focal volume of 1 cm³.
 352 The effects of frequency and focal volume are reduced at higher temperatures. At 100 °C, these difference, drop,
 353 respectively, to 0.082 and 0.069 MPa.

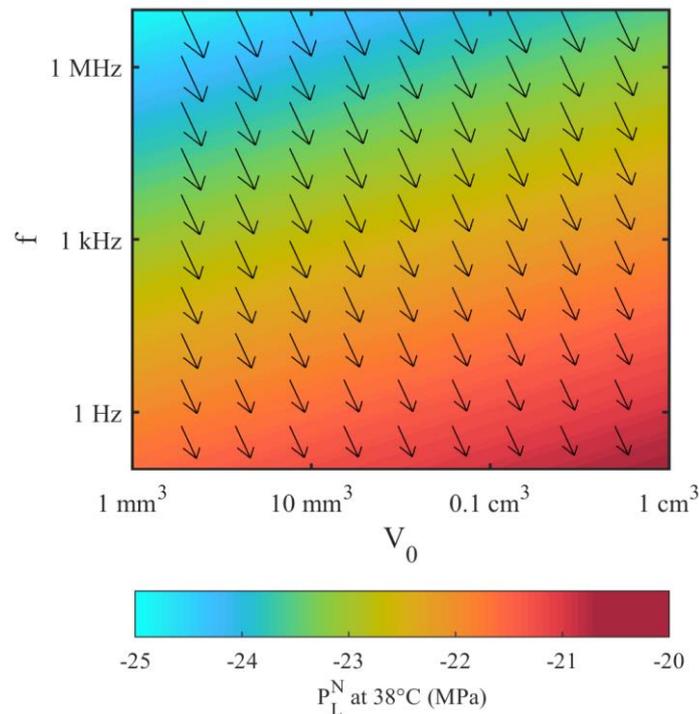


Figure 3. Effects of frequency and focal volume on nucleation thresholds at 38 °C.

356 In summary, the results presented above show that although the ultrasound frequency does play a role in
357 determining the energetics of nucleation, this is of secondary importance to the temperature of the medium. It
358 was also shown that nucleation pressure thresholds are decreased at lower frequencies for a fixed focal volume
359 and constant temperature. This is in agreement with previous experimental work on the effects of frequency on
360 bubble nucleation [62]. Finally, the results shown in Fig. 3 confirm that although $c_E(T)$ was calculated for
361 experimental results performed at lower frequencies, c_E is still valid for modelling HIFU nucleation at 2 MHz.

362 **3.4. Acoustic Propagation and Heat Deposition in Tissue-mimicking Phantoms**

363 The HIFU Simulator 1.2 [63] was employed to solve a Khokhlov–Zabolotskaya–Kuznetsov (KZK) nonlinear
364 acoustic wave equation and obtain pressure waveforms and the absorbed ultrasound energy for a HIFU pressure
365 field. The KZK equation is often used to model high-intensity acoustic beams and has been successfully applied
366 for modelling acoustic fields for HIFU and lithotripsy sources [64-66]. This equation approximates nonlinearity
367 and thermoviscous absorption within a plane wave approximation and also diffraction in a parabolic
368 approximation [66]. From the absorbed acoustic energy obtained with the KZK equation, the temperature rise
369 at the focus can be calculated with the Pennes Bio-Heat Transfer Equation (BHTE). This equation models heat
370 deposition at the HIFU focus accounting for heat diffusion and convective cooling due to blood perfusion [66].
371 In the present work, the convective term in the BHTE is ignored due to the absence of perfusion, and this
372 equation is reduced to a simple heat diffusion equation in the presence of a heat source.

373 Non-linear acoustic propagation and heat deposition in a tissue-mimicking gel were simulated for a single
374 element focused transducer operating at 2 MHz (Sonic Concepts H106). Tissue-mimicking phantoms have been
375 extensively used for experimental work on histotripsy, having found good agreement with ex-vivo results
376 [10,65,67]. The transducer and medium parameters for the HIFU Simulator were taken from previous works on
377 boiling histotripsy [10,33,65] and ultrasound-induced nucleation [28,30,44]. Propagation was simulated for a
378 two-layer medium, first in water and then in phantom for an input electrical power of 150 W and 85% transducer
379 efficiency. Following manufacturer specifications for a 2 MHz transducer (Sonic Concepts, H106), the radius
380 of curvature was 63.2 mm, where the final 5 mm accounts for propagation through the phantom. The linear
381 pressure gain for the focused transducer was 72.9 [65].

382 The spatial grid consisted of 20 points per wavelength in the axial direction and 25 points per wavelength in the
383 radial direction for a total domain length of 9.48 cm. The upper half of the axisymmetric domain consisted of
384 438 elements in the radial direction and 2062 elements in the axial direction, resulting in 903,156 elements.
385 Element sizes were of 0.0731 and 0.0460 mm in the radial and axial directions, respectively. Simulations were
386 carried for 128, 256, 512, 1024 and 2048 harmonics. Results were considered to converge when doubling the
387 number of harmonics yielded less than 0.5% difference in peak positive pressure (PPP) amplitudes. Pressure
388 fields obtained for 2048 harmonics were chosen to be incorporated into the CNT models discussed in this work.

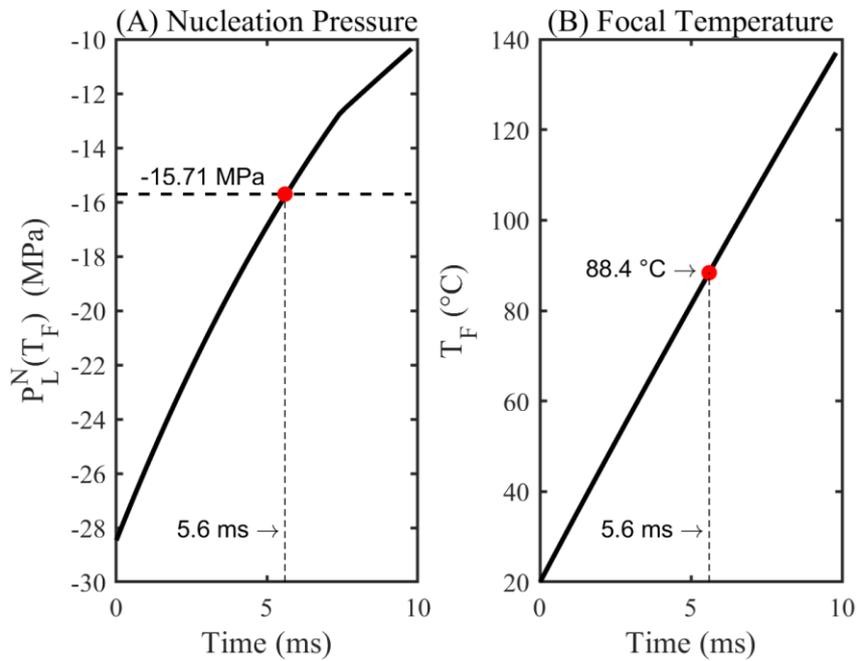
389 HIFU heat deposition was calculated with BHTE equations, which in absence of a convective sink are reduced
390 to standard heat diffusion equations with a heat source given by the absorption of pressure waves. Temperature
391 fields were computed up to 20 ms of HIFU sonication for each element in the grid for an initial temperature of
392 20 °C. These temperature maps were then used to calculate the thermodynamic quantities given by Eqs. 2 – 5,
393 Eqs. 10 – 16 and Eq. 18 at each element of the mesh.

394 **3.5. The Timescales of Nucleation in HIFU**

395 The timescales of boiling bubble nucleation in HIFU have been traditionally approximated by the pulse duration
396 the focal region needs to reach 100 °C [2,3,33,65,68]. This approximation carries the underlying assumption
397 that bubbles always nucleate at 100 °C independently of the pressure of the medium. Such an assumption does
398 not have much physical reasoning other than the empirical observation that tap water boils at about 100 °C
399 under atmospheric pressure. It is important to notice that liquids or tissue phantoms are traditionally degassed
400 before HIFU experimentation, depleting the medium from microbubbles which trigger boiling at 100 °C under
401 atmospheric pressure [24]. Appropriate parametrisation and planning of boiling histotripsy, therefore, need to
402 account for the timescales necessary to cause explosive boiling within milliseconds in terms of focal pressures
403 and temperatures [69].

404 Figure 4-A shows the nucleation pressure threshold calculated at the HIFU focus as a function of the peak focal
405 temperature, which increases with time due to heat deposition and is shown in Fig. 4-B. It can be seen in Fig.
406 4-A that heat deposition causes the nucleation pressure threshold P_L^N at the HIFU focus to decrease with pulse
407 duration. The onset of nucleation will happen whenever the value of P_L^N is lower in magnitude than the peak

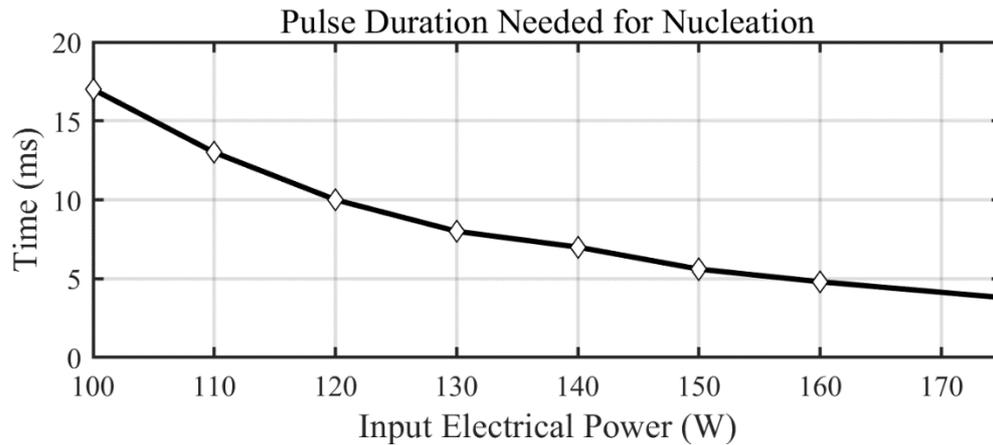
408 negative pressure at the HIFU focus, which is -15.71 MPa for the protocol under consideration and is
409 represented by the black dashed line in Fig. 4-A.



410

411 Figure 4. (A) Evolution in time of the nucleation pressure threshold at the HIFU focus at 66.72 kW cm^{-3}
412 heating rates. (B) Evolution in time of HIFU peak temperatures.

413 Nucleation at 2 MHz driving frequency with $P^+ = 83.54 \text{ MPa}$ and $P^- = -15.71 \text{ MPa}$ is predicted after 5.6 ms
414 of sonication in Figure 4. When these results are compared to those in Fig. 4-B, it can be seen that the simulated
415 temperature of the medium at 5.6 ms of sonication is around 88.4 °C. This shows the possibility of nucleation
416 in boiling histotripsy before the medium reaches 100 °C. These results indicate that boiling histotripsy, when
417 performed within a few milliseconds, has similar origins to that of cavitation below the intrinsic threshold.
418 However, BH would occur due to a lowering of the intrinsic threshold which is a consequence of heat deposition.



419

420

Figure 5. Pulse duration needed for the onset of nucleation as a function of input electrical power.

421

Additional simulations at 100, 110, 120, 130, 140, 160 and 175 W input electrical power were also performed for comparison with the results shown in Figure 4. A change in these parameters results in distinct HIFU pressure and temperature fields which shape the conditions under which nucleation happens. Figure 5 shows the pulse duration needed to trigger nucleation for a range of input electrical powers to the transducer.

425

Figure 5 shows that the pulse duration needed for nucleation decreases monotonically with increasing input electrical power to the transducer. In practice, such trends can inform the choice of appropriate PRFs and duty cycles in terms of the input electrical power when planning histotripsy protocols.

428

These results agree with the experimentally observed tendency of nucleation to take place at shorter timescales for high input electrical powers (large focal peak pressures) [10, 65]. Moreover, the trend in Fig. 5 is slightly non-linear because the focal waveforms become increasingly distorted for higher electrical power inputs to the transducer. This means that the magnitude of focal peak negative pressures does not increase as much as that of peak positive pressures for increasing input electrical power.

433

These results indicate that boiling histotripsy, when performed within a few milliseconds, has similar origins to that of cavitation below the intrinsic threshold. However, BH would occur due to a lowering of the intrinsic threshold which is a consequence of heat deposition. This means that within millisecond timescales it is difficult to draw a boundary between thermal and mechanical effects of HIFU in the nucleation of bubbles.

437

Consequently, the onset of nucleation at the HIFU focus depends both on the peak negative pressure of the ultrasound wave and on the temperature of the medium. This suggests that there is a high likelihood of not

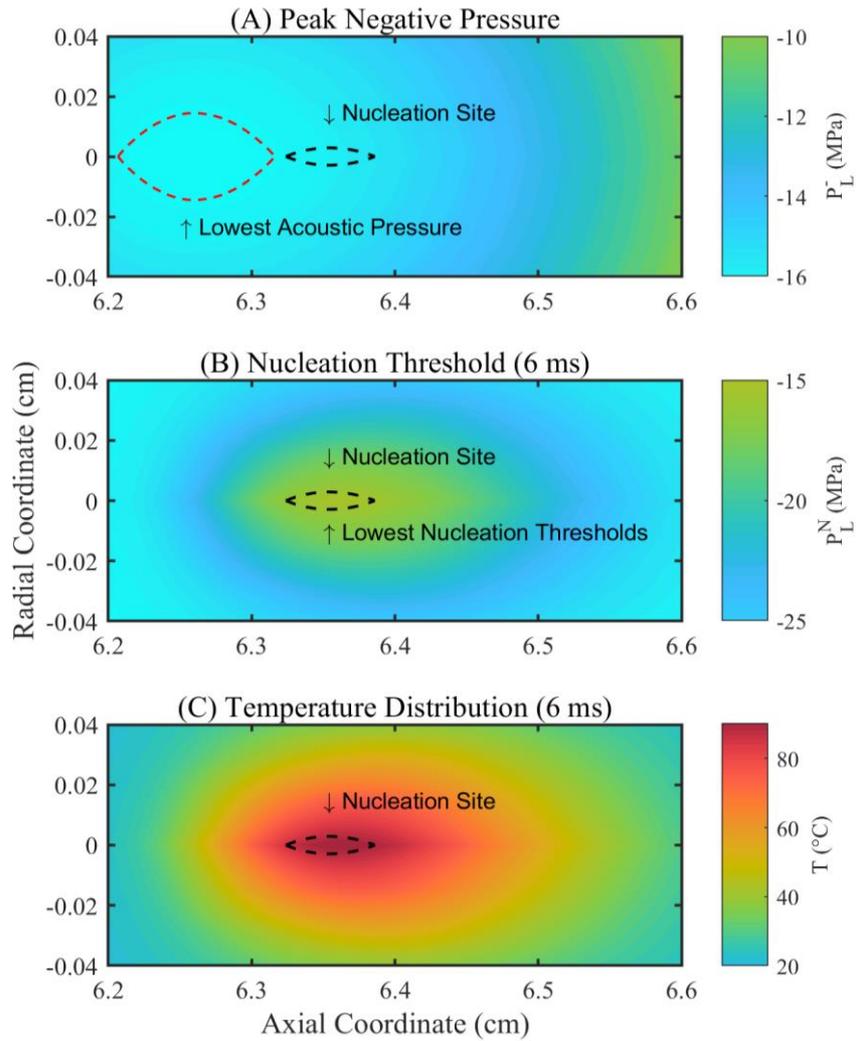
438

439 obtaining millisecond bubble formation if peak negative pressures are below the nucleation pressure threshold.
440 Finally, it is also worth noting that the limiting nucleation rates used to define pressure thresholds were of one
441 bubble per millimetre cubic per 0.1 microseconds. As discussed above, these results will change if the
442 observation timescales for nucleation τ_S are changed. However higher values of τ_S would require a transient
443 expression for the nucleation rate and consideration of the effects of gas diffusion.

444 **3.6. Spatial Profile of Nucleation**

445 Following from models predicting nucleation after 5.6 ms, Fig. 6 shows the spatial profile of nucleation in terms
446 of the acoustic pressure, the focal temperature and the temperature-dependent nucleation pressure threshold
447 obtained around the geometrical focus. The KZK model showed this region to be that of highest heat deposition
448 and lowest acoustic pressures. Figure 6-A shows the relationship between the preferential nucleation site (black
449 dashed contours) to the peak negative acoustic pressures. The temperature-dependent nucleation pressure
450 threshold is shown in Fig. 6-B, and the temperature distribution around the geometrical HIFU focus after 6 ms
451 of sonication is shown in Fig. 6-C.

452 Figure 6-A shows that although the lowest acoustic pressures happened pre-focally (red dashed contour), the
453 preferential nucleation site was placed around the HIFU focus at 6.36 cm in the propagation direction. This is
454 somehow counter-intuitive to the idea that HIFU bubble nucleation is associated with the lowest acoustic
455 pressures in the field.



456

457 Figure 6. (A) Peak negative acoustic pressures obtained from KZK simulations. Black dashed contour
 458 demarks preferential nucleation sites. Red dashed contour demarks lowest acoustic peak negative pressures.

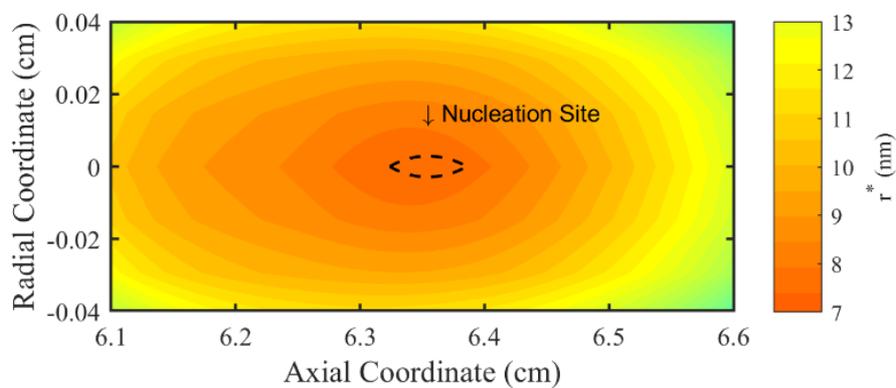
459 (B) Nucleation pressure thresholds obtained from coupled KZK-BHTE-CNT simulations. Black dashed
 460 contour demarks preferential nucleation sites. (C) Temperature distribution after 6 ms of sonication obtained

461 from KZK-BHTE simulations. Black dashed contour demarks preferential nucleation sites.

462 Figures 6-B and 6-C shed some light into this question. Figure 6-B shows that pre-focal nucleation thresholds
 463 after 6 ms of sonication vary from -25 to -20 MPa. The magnitude of these thresholds is much greater than the
 464 magnitude of the peak negative acoustic pressures that are shown in Fig. 6-A, which varies from -16 to -14 MPa
 465 in the same region. Therefore, nucleation as a consequence of acoustic propagation itself should not happen in
 466 these regions. Figure 6-B also shows that nucleation pressure thresholds have their lowest magnitude around
 467 the HIFU focus, where peak negative acoustic pressures surpass the threshold and trigger nucleation.

468 Finally, Fig. 6-C clarifies the disparity between nucleation preferential sites and lowest peak negative acoustic
469 pressures shown in Fig. 6-A. Figure 6-C shows the temperature distribution after 6 ms of sonication. These
470 results show higher temperatures at the geometrical HIFU focus, having the preferential nucleation site as an
471 envelope to the regions of higher temperature. Since the nucleation pressure threshold is temperature-dependent,
472 these results indicate that the regions of highest temperature are the regions where nucleation is more likely to
473 occur within milliseconds given that acoustic pressures surpass the nucleation pressure threshold.

474 In summary, Fig. 6 shows that nucleation is spatially restricted to regions where the peak negative acoustic
475 pressure overcomes the nucleation pressure threshold, however, these regions are not necessarily the regions of
476 lowest acoustic pressure. Such results further indicate that bubble nucleation in boiling histotripsy is a
477 phenomenon limited by temperature at the HIFU focus. This agrees with previous simulations of bubble
478 dynamics in boiling histotripsy, which concluded that the temperature field can also limit the growth of BH
479 bubbles [71]. Finally, it can be seen that although the acoustic pressure is the ultimate trigger for nucleation,
480 HIFU heat deposition facilitates bubble nucleation. Thus, nucleation happens preferentially at the regions of
481 highest heat deposition.



483 Figure 7. Size of critical nuclei around the HIFU focus.

484 Figure 7 shows the critical size of nuclei around the HIFU focus. This is the minimum size that nuclei must
485 achieve such that their chances of spontaneous growth are greater than their chances of collapse. Within the
486 preferential nucleation site, the radius of critical nuclei is of approximately 7.5 nm. These dimensions are in
487 agreement with size stability bounds for bubble dynamics simulations of nano-bubbles in the literature [70].
488 Moreover, Fig. 7 also shows that bubbles nucleated at the HIFU focus following heat deposition tend to be

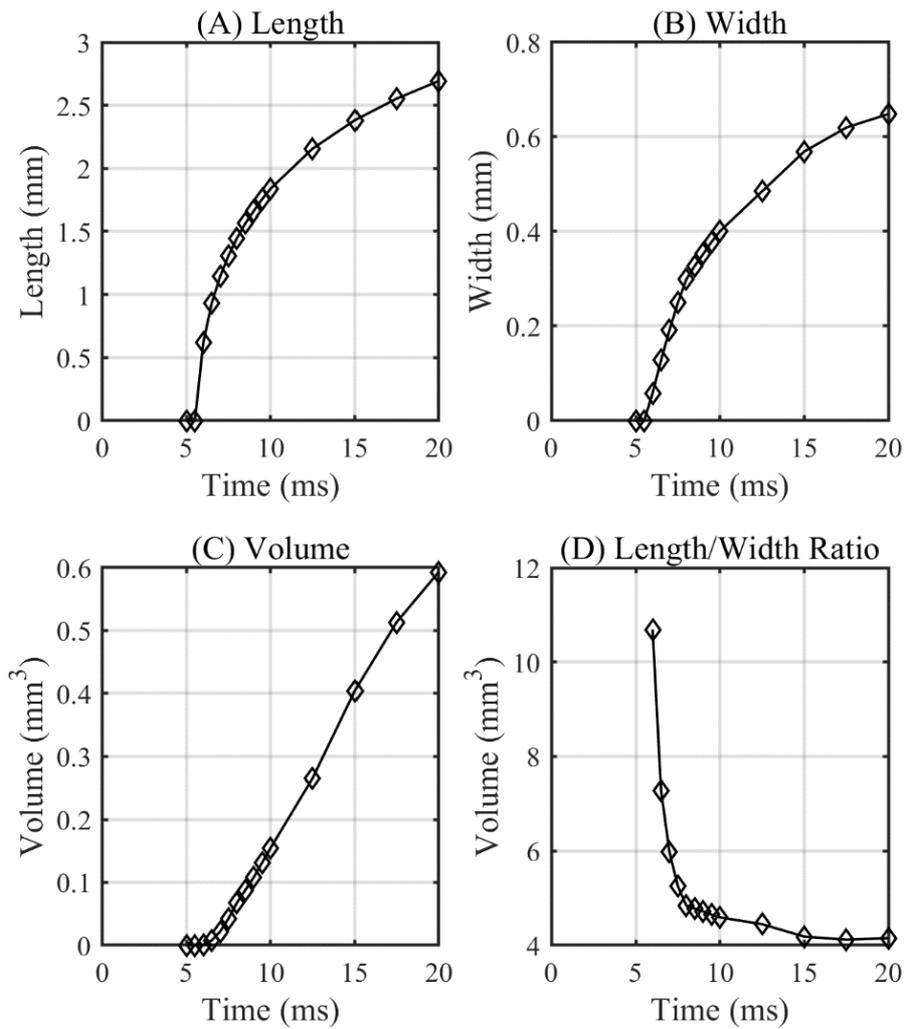
489 larger. This implies that the HIFU focus is the site where bubble nuclei have higher chances of merging with
490 other nuclei of similar size and form larger bubbles which are mechanically stable within the thermodynamic
491 conditions imposed by HIFU pressure and temperature fields.

492 It is important to note that the ability of Eq. 2 to predict the size of critical nuclei shown in Fig. 7 has limitations.
493 This is an equation that predicts the minimum size of bubble nuclei so that nucleation happens. Equation 2 does
494 not take into account either inertial or viscous terms present in standard equations for bubble dynamics [26,71].
495 This highlights the need to integrate these terms into CNT for realistic physical modelling of nucleating bubble
496 dynamics.

497 **3.7. The Effects of Pulse Duration on the Dimensions of the Nucleation Site**

498 In Fig. 8, the effects of pulse duration on the length and width of the preferential nucleation site are displayed.
499 Figure 8-A shows the length of the nucleation site which is zero at any time before the time of nucleation (5.6
500 ms) and then ranges from 0.62 mm after 6 ms of sonication to 2.69 mm after 20 ms of sonication. Similarly,
501 Fig. 8-B shows the width of the preferential nucleation site. These range from 60 μm after 6 ms of sonication
502 to 0.64 mm at 20 ms of sonication. These are not measures of the resulting cavity after a boiling histotripsy
503 protocol, but rather an estimation of the region where boiling bubbles first originate and are thermodynamically
504 stable within the HIFU-induced pressure and temperature fields.

505 In Fig. 8-C, the ellipsoidal volume of the nucleation site is computed based on its length and width. It can be
506 seen that the total volume where bubbles first nucleate and are stable within the HIFU pressure and temperature
507 field increases with pulse duration. This is equivalent to saying that the volume of the nucleation site increases
508 with the size of the region where acoustic pressures surpass the nucleation threshold. As a consequence of the
509 spatial profile of heat deposition in HIFU, the length of the nucleation site is consistently larger than its width.
510 This can be observed in Fig. 8-D, showing that for very short protocols the length of the nucleation region is
511 much larger than its width. For longer pulse durations, this ratio diminishes and the curve reaches what seems
512 to be asymptotic behaviour at a ratio of approximately 4. These results flag a greater need for control and
513 planning of boiling histotripsy lesions along the propagation direction rather than in the perpendicular plane
514 (radial coordinate of the HIFU beam).



515

516 Figure 8. Dimensions of the nucleation site. (A) Length of the nucleation site. (B) The width of the nucleation
 517 site. (C) The volume of the nucleation site assuming ellipsoidal shape. (D) The ratio between the length and
 518 width of the nucleation site. Diamond markers in Fig. 8 represent values obtained for thermal simulations
 519 interpolated as the black solid line.

520 Results shown in Fig. 8 might also provide an explanation for the characteristic “tadpole” shape of boiling
 521 histotripsy lesions. Previous experiments on boiling histotripsy in tissue phantoms captured by high-speed
 522 cameras have shown that the tail of BH lesions is caused by the action of vapour bubbles [33]. Similarly, results
 523 in Fig. 8-D show that the length of the region where vapour bubbles nucleate is at least four times larger than
 524 the width where they can nucleate and grow spontaneously. The dimensions of this region would, therefore,
 525 influence the final shape of a BH lesion.

526 **4. Conclusions**

527 In this work, classical nucleation theory was applied to study bubble nucleation in HIFU pressure and
528 temperature fields, using boiling histotripsy as a case study. A temperature-dependent expression for the
529 nucleation pressure threshold in HIFU was derived from first principles assuming stationary nucleation. The
530 importance of obtaining a suitable approximation for the surface tension of the liquid in obtaining nucleation
531 pressure thresholds was discussed.

532 A temperature-dependent scaling factor for the surface tension in HIFU-induced nucleation was obtained by
533 fitting available experimental data to the theoretical predictions of CNT. The effects of HIFU frequency and
534 focal volume were analysed. It was found that the magnitude of nucleation pressure thresholds decreases with
535 decreasing frequencies, however this effect is reduced at high temperatures.

536 It was shown that the regimes of boiling (nucleation triggered by high temperatures) and cavitation (nucleation
537 triggered by negative pressures) can be distinguished in terms of the nucleation rate. At high temperatures ($T >$
538 $150\text{ }^{\circ}\text{C}$), the superheating of the system is the dominant factor in nucleation. Conversely, at medium and low
539 temperatures ($T < 100\text{ }^{\circ}\text{C}$) the peak negative acoustic pressure plays an increasingly important role in the
540 nucleation of bubbles.

541 This means that when nucleation takes place at millisecond timescales and within the thermodynamic range of
542 boiling histotripsy, the effects of HIFU-induced pressure and temperature fields are coupled and there is no
543 clear dominance of either. Our models show that the acoustic pressure is the ultimate trigger for nucleation,
544 however, HIFU heat deposition facilitates bubble nucleation by lowering thresholds. This is the reason why
545 nucleation happens at the regions of highest heat deposition in BH. Moreover, it was also shown that bubble
546 formation in boiling histotripsy can be achieved at temperatures lower than $100\text{ }^{\circ}\text{C}$ provided that peak negative
547 pressures surpass the nucleation threshold. These results indicate that the boundaries between boiling and
548 cavitation-cloud histotripsy are much more diffuse than currently assumed.

549 The characteristic length and width of the preferential nucleation site were analyzed in terms of the pulse
550 duration. These showed that the region where bubbles nucleate increases with pulse duration, depending
551 ultimately on the temperature profile around the HIFU focus. The lengths of the preferential nucleation site in

552 terms of pulse duration were consistently greater than the width. This can provide an explanation for the
553 formation of the tail of characteristic tadpole-shaped BH lesions.

554 **5. Acknowledgements**

555 MOdA would like to thank CNPq, the Brazilian National Council for Scientific and Technological
556 Development for funding their PhD at UCL.

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