

Article

Quantifying the Environmental Impacts of Manufacturing Low Earth Orbit (LEO) Satellite Constellations

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Abstract: The growing amount of space debris in the low Earth orbit poses a danger to manned as well as uncrewed missions. Additionally, the new business model of providing internet from space is emerging among new space players, making low Earth orbit more crowded. These factors have encouraged the space community to focus on sustainability in space. Satellite manufacturers typically have the capability to perform complete life cycle analysis (LCA) on their own products based on the manufacturing data. However, there is a lack of a method for non-manufacturers such as environmentalists and the general public to predict the carbon footprint of satellite manufacturing using a subsystem-level mass budget. Hence, this paper presents a method to quantify environmental pollution caused by the production of satellite constellations. Starlink is taken as a case study in this paper, and mass budget is predicted based on space systems engineering budget estimation techniques, the parametric method, and Federal Communication Commission orbital data. With the budget table used as an input, space-specific life cycle assessment is performed based on European Space Agency's life cycle inventory database. Finally, the single score for Starlink constellation version 1 was found to be 76 kilo points. This signifies the annual environmental load. These results could be helpful in obtaining an overview of the environmental effects of the production phase of satellite constellations. Further, the results could act as a foundation for further research on implementing more circular approach practices on Earth as well as in space.

Keywords: circular economy; lifecycle assessment; low earth orbit; satellite constellation



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1. Introduction

Space debris has long been a concern for crewed spaceflight programs as well as robotic missions in the near space environment [1]. In 2009, the National Aeronautics and Space Administration (NASA) faced an emergency in the evacuation of astronauts due to the possible threat of collision, and the situation forced the crew to take shelter [2]. Furthermore, the emergence of a novel business model for space-based internet services is adding to the congestion within the low Earth orbit environment. Over the years, space sustainability has become a topic of research and given importance, considering the Earth's orbital environment as a finite resource. Although the term "space sustainability" is now commonly used in the space sector, there was no widely agreed-upon definition until recently. In 2018, the United Nations (UN) Committee on the Peaceful Uses of Outer Space (COPUOS) addressed this by establishing guidelines for the Long-term Sustainability of Outer Space Activities. For the first time, these guidelines offered an initial definition of space sustainability as "The long-term sustainability of outer space activities is defined as the ability to maintain the conduct of space activities indefinitely into the future in a manner that realizes the objectives of equitable access to the benefits of the exploration and use of outer space for peaceful purposes, in order to meet the needs of the present generations while preserving the outer space environment for future generations" [3]. Although a definition of the term is presented, the primary emphasis of guidance lies in

the preservation of the space environment". Hence, a need for new definition that includes various aspects of sustainability associated with space arises. According to [4], there are three fundamental pillars that should be included in defining space sustainability. They are "sustainability from space", "sustainability in space", and "sustainability for space". Correspondingly, when the topic of space sustainability is addressed within the sector, focus is typically directed towards two key facets. One is sustainability from space through space data and sustainability in space focusing on space debris. *Promoting* sustainability based on downstream data is the primary goal of obtaining space data. And reducing space debris, considering space in orbit as a finite resource, is another area of research. But there is a third aspect of sustainability associated with this topic, which is the environmental impact on earth due to production that comes under sustainability for space. Within sustainability for the space context, the focus is given more to rocket launches. For instance, research shows a major concern is the atmospheric pollution resulting from rocket launches, which release combustion gases and particles capable of depleting the ozone layer and disrupting Earth's energy balance. Existing international regulations are inadequate, and local policies are limited. It is imperative to conduct extensive research and develop sustainability metrics to guide future regulations and foster more environmentally sustainable practices within the space industry [5]. In this paper, we focus on "sustainability for space", emphasizing the effects of satellite manufacturing, considering its status as the least explored domain from the space sustainability perspective, prompting a critical need for comprehensive investigation and analysis. Life cycle assessment (LCA), sometimes referred to as life cycle analysis, measures the impacts on the environment associated with the life cycle of a product, process, or service [6]. ISO standards 14040 and 14044 deal with LCA [7,8]. NASA's investigations deviate from the standardized LCA, as outlined in ISO 14040/44, as they exclusively focus on economic costs without incorporating assessments of environmental [9]. Based on the generic ISO standards that drive LCA studies in any sector, the European Space Agency (ESA) has developed a space-specific LCA that can be used for space missions. Space System Life Cycle Assessment guidelines aims to establish the methodological rules on how to correctly perform space-specific life cycle assessment [10]. The life cycle inventory database used by ESA is available on the subsystem level and also on the component level. A subsystem/component-level mass budget cannot be obtained for any satellite since it is commercially confidential. As of now, space-specific LCA can be performed only by respective satellite manufacturers who have readily available data on the subsystem/component-level mass budget. There is a need for a method to calculate the environmental footprint during the production process by any user for any low Earth orbit (LEO) satellite, even though a mass budget is not available to provide insights on environmental effects. This paper presents a method to perform a life cycle assessment for low Earth orbit satellites, with the Starlink constellation as a case study, and based on the mass budget, midpoint indicators are calculated using the Simapro Life Cycle Assessment tool. Through this, we aim to address the following research question:

How can the environmental impacts be quantified during the production phase of low Earth orbit constellation satellites by applying the systems engineering and life cycle assessment principles?

This article is structured in following way. Section one provides a context for the sustainability paradox of the space industry and the need for focusing on the environmental impacts of the production phase of space missions. Section two, the Materials and Methods Section, outlines the application of the mass budget techniques used in space systems engineering and LCA to assess the life cycle environmental impact, emphasizing the delineation of the system boundary considered for this analysis. The case study Results Section presents a comprehensive examination of Starlink, including the breakdown of satellite subsystems and their mass budget and LCA results. The Discussion Section interprets these findings, exploring their implications for the environmental sustainability of satellite mega-constellations production, proposing future work in potential framework develop-

ment that can give insights into all aspects of environmental effects that are discussed in the context of the sustainability paradox.

2. Literature Review

2.1. Space Sustainability

In today's broader perspective, sustainability is almost always seen in terms of three dimensions: social, economic, and environmental [11]. However, in the space industry, more focus is given to the environmental aspect of space. For example, as per the UN COPOUS definition on space sustainability stated in the Introduction Section, one can interpret that the focus is placed on "preserving outer space". But there are other aspects that should be considered in the "space sustainability" definition. According to the Organization for Economic Co-operation and Development (OECD) paper on space sustainability, the concept of "space sustainability" encompasses a broader spectrum of considerations beyond the delineation provided by the UN COPOUS. This expanded perspective incorporates environmental, societal, occupational, and economic facets [12,13]. Space agencies mainly focus on specific aspects of space sustainability. For instance, NASA sustainability efforts are mainly oriented towards the economic aspect [9]. ESA is focusing more on a clean space initiative that covers Eco-design, Cleansat, and active debris removal [14]. Eco-design aims to establish a shared eco-design framework for the European space sector. Cleansat concentrates on the advancement of green technologies to mitigate environmental impacts. Active debris removal targets the development of technologies necessary for managing the end-of-life of space assets [15]. For instance, in alignment with the directives outlined in their National Space Strategy, the United Kingdom (U.K.) is intensifying its initiatives in the domain of space sustainability. This commitment is exemplified by the initiation of two active debris removal phase B mission studies, a collaborative undertaking with Astroscale and ClearSpace, both of which were awarded in September 2022, amounting to a total funding of GBP 4 million. These studies are pivotal in assisting the U.K. Space Agency in determining the most viable mission concept to advance into a comprehensive design and launch phase. The culmination of these efforts is anticipated in 2026, marked by a demonstration showcasing the nation's proficiency in rendezvousing, docking with, and deorbiting two decommissioned U.K. satellites [16]. Hence, we can see private companies' and space agencies' initiatives on specific aspects of sustainability and a lack of integrated decision making considering all aspects of sustainability.

In 2018, the World Economic Forum conducted a competitive solicitation for proposals and subsequently selected a consortium consisting of four entities to develop the Space Sustainability Rating [17]. This consortium is comprised of the European Space Agency, Massachusetts Institute of Technology, University of Texas at Austin, and Bryce, Space and Technology. The collaborative efforts of these organizations and the World Economic Forum were instrumental in delineating the technical and programmatic dimensions of the Space Sustainability Rating during the period spanning 2019 to 2021. The Consortium collectively contributes expertise across various domains, encompassing the modeling and assessment of the impact of space debris in Earth orbit, astrodynamics, characterization of space objects, technology policy, space economics, and an understanding of the roles played by emerging countries and private entities within the space sector [18].

The evaluation of these scores is predicated upon a comprehensive assessment of various factors. These encompass but are not limited to satellite and mission design, orbital parameters, post-mission disposal strategy, and collision avoidance strategy [19]. Furthermore, the selection and attributes of the launch provider exert influence on the overall score. Supplementary credit is accorded for the inclusion of discretionary components such as de-orbiting fixtures designed for the active removal of the object upon the fulfillment of its operational lifespan. It is imperative to underscore that the extent to which a mission aligns with international guidelines will also be factored into the evaluative process [20].

The sustainability rating is not designed to give insights on overall aspects considering all three sources of environmental impacts that should be considered. Apart from leaving

out “sustainability for space”, there is a clear ongoing imbalance between “sustainability in space” and “sustainability from space” [4]. Following [4], as space applications and technologies continue to be developed to address sustainable development challenges for humanity’s benefit, referred to as “sustainability from space,” the “sustainability of the space sector” paradoxically becomes less sustainable.

2.2. Systems Engineering

Systems engineering is often construed as a convergence of artistic and scientific dimensions. This portrayal is fitting, as it demands both the imaginative capacity and technical proficiency of engineers, coupled with the systematic application of management principles [21]. Systems engineering focuses on identifying customer needs and the required functionality early in the development cycle, documenting requirements, and subsequently advancing with design synthesis and system validation, all while considering the complete problem [22]. In systems engineering, budgeting is the process followed during the design process of the product. Budgeting essentially involves the collection and organization of information regarding a significant resource and subsequently allocating this resource optimally across various components of the system under consideration. A technical budget can encompass a variety of topics, such as standby power, memory, processor usage, load, accuracy, and other product-specific aspects [23]. Following this systematic approach, in space systems engineering, after analyzing the requirements, initial performance budgets are estimated [24]. Mass budget is one of the budgets among many other technical budgets estimated in the preliminary stage of space mission design [25]. The determination of the mass budget for satellites primarily relies on two distinct approaches. The first method involves the construction of an average mass budget table derived from historical data, consolidating information from past satellite missions. This approach leverages the collective experience and outcomes of previously launched satellites to establish a baseline for estimating mass parameters. The second method employs a parametric method, wherein mass budget calculations are based on a set of predefined parameters and formulas. This method involves a more detailed and specific analysis, incorporating factors such as satellite function, design specifications, and mission requirements. The subsequent sections will delve into a comprehensive discussion of these two approaches.

2.2.1. Average Mass Budget Method

A straightforward approach to gaining insight into the mass budget of spacecraft within the scope of our research area is to refer to the average mass budget table. Average mass budget is predicted based on historical data from existing satellites. The average mass budget is the first step for making initial estimates as a starting point before the iterative process of detailed subsystem design [25]. Table 1 below represents the average mass budget by spacecraft types. It shows the mass budget distribution among various subsystems.

While performing LCA, the impacts can be measured in terms of midpoint indicators. Midpoint indicators serve as intermediate measures of environmental impact, indicating alterations in the natural environment resulting from emissions or resource utilization [26]. Spacecraft manufacturers can perform the midpoint indicators calculation in a straightforward way since the data on component level are readily available for them. The results are more accurate since a detailed component-level mass budget is available for the manufacturers who are interested in performing their own assessments. However, there is no publicly available method for predicting the footprint of a satellite manufacturer since the exact subsystem/component-level mass budget data are held by the respective satellite manufacturers. Hence, the preliminary mass budget prediction techniques used in space systems engineering are adopted for this research. Table 1 represents the average dry mass distribution among various subsystems, and it is categorized according to the type of spacecraft [25]. Since we are focusing on a low Earth orbit constellation, column 3 (LEO prop %) in Table 1 is our primary focus. The average mass budget table represented in Table 1 is used by during initial phases of mission design by systems engineers and mission design

and analysis engineers to estimate the preliminary budget based on the requirements. A user can use the same table (LEO with propulsion) to calculate the midpoint indicators with the help of ESA's Life Cycle Inventory (LCI) database. However, it is necessary to partition it for our case study because of two reasons. One is that we need to partition it according to ESA LCI database, and the other reason is because the "propellant mass 22%" in LEO in the propulsion category in Table 1 is more generic and is not suitable use for our case study since Starlink uses a Hall-effect thruster [27]. The propellant mass also affects the mass of the tank. Hence, partitioning is necessary for the propulsion subsystem and propellant for our case study. The new SMAD (Space Mission Analysis and Design) list shows that all spacecraft used for the average mass budget estimation for LEO with propulsion [28]. If we look closer, the mass of propellant varies from 2% to 76% [25]. With Hall-effect thrusters, the quantity of propellant required for one year of station keeping in geosynchronous Earth orbit (GEO) is approximately 0.2% to 0.4% of the total mass, contrasting with the higher range of 1.5% to 3% typically consumed by traditional chemical propulsion systems [29]. Knowing only the total mass of Starlink, propellant mass calculation is needed. Therefore, by subtracting the propellant mass from the total mass, the total dry mass can be obtained. From the total dry mass, it is feasible to partition it according to the average mass budget table and space systems' budget allocation techniques.

Table 1. The average mass, represented as a percentage of the dry mass, categorized according to the type of spacecraft for various subsystems [25].

Subsystem (% of Dry Mass)	No Prop	LEO with Prop	High Earth	Planetary
Payload	41%	31%	32%	15%
Structure and mechanisms	20%	27%	24%	25%
Thermal control	2%	2%	4%	6%
Power (including harness)	19%	21%	17%	21%
Tracking, telemetry, and control (TT&C)	2%	2%	4%	7%
On-board processing	5%	5%	3%	4%
Attitude determination and control	8%	6%	6%	6%
Propulsion	0%	3%	7%	13%
Other (balance+launch)	3%	3%	3%	3%
Total	100%	100%	100%	100%
Propellant	0%	27%	72%	110%

2.2.2. Parametric Method

In the parametric method, mathematical equations or algorithms are used based on spacecraft characteristics such as mission type, payload mass, and payload power to estimate the satellite mass [30]. After estimating the initial mass budget through the average mass budget table, as discussed in the previous section, the parametric method is used to obtain a detailed, mass budget for each and every subsystems based on detailed mission requirements. But for this research, the aim is to quantify midpoint indicators for a generic LEO constellation with limited available Federal Communications Commission (FCC) data, which means the parametric method cannot be used for all subsystems. Hence, the average mass budget table is used for most of the subsystems, and the parametric model is used for the propellant. The key reason is that data regarding orbit change, satellite total mass, and satellite lifetime are available. Therefore, a parametric model is employed to obtain a detailed estimate of propellant mass. Consequently, this paper utilizes a combination of the average mass budget method and the parametric method. Propellant mass data are predicted using a parametric method, supported by FCC filings submitted to the government. The FCC serves as a regulatory body overseeing communications in the United States, including telecommunications, broadcasting, and satellite services [28]. It regulates satellite operators within the country. Companies and individuals must submit

orbital data to the FCC for various activities, and these filings are essential for maintaining regulatory compliance and transparency. Hence, every satellite operator must submit several documents, including orbital data and an orbital debris mitigation (ODM) plan as part of the application process, ensuring compliance with the regulations set forth by the FCC. The Debris Assessment Software (DAS) v. 3.2.6, developed by the NASA Orbital Debris Program Office, is utilized to evaluate adherence to NASA's guidelines for minimizing orbital debris during the planning and design phases of space missions. While the DAS helps ensure compliance with NASA's requirements, the FCC's regulations mandate additional disclosure requirements that go beyond the DAS outputs. The ODM plan must incorporate these supplementary disclosures. Including the DAS compliance matrix along with the relevant inputs and outputs from the NASA DAS code can streamline the application review process [31]. The DAS input and output usually contains satellite mass and orbital data [32]. These data can be considered as primary data submitted by satellite operators via filings to the FCC. Mass and orbital data are essential for performing space-specific LCA for the method discussed in this paper. On the international level, satellite operators are governed by the International Telecommunication Union (ITU). The ITU oversees a collaborative framework for coordinating radio frequencies used by satellites on a global scale. This system aims to prevent interference both among satellite systems and between satellites and other radio communication networks [33]. As part of the FCC application process, applicants must provide orbital data for their planned missions. However, in the context of the ITU, any files related to the orbital debris mitigation (ODM) requirements are not included in the ITU's regulatory procedures for non-geostationary satellites, except for those containing orbital data [34]. At the international level, users can access orbital data through ITU filings available on its website, but they cannot access the mass data of satellites, which is typically obtained from NASA's Debris Assessment Software (DAS). In this paper, the mass value for the Starlink version 1 satellite is derived from [35], but this cannot be regarded as primary data from the manufacturer. The FCC-mandated orbital debris mitigation (ODM) filings starting in 2024 [31]. However, SpaceX filed for approval for its modification of 1665 V1 satellites in 2018 without requiring an ODM submission for version 1 at that time [36]. This explains why the primary data are available in terms of orbital information but not mass. Now that the FCC requires all satellite operators to submit an ODM plan, users will be able to refer to the FCC for both mass and orbital primary data. However, this approach has a limitation, as FCC filings only cover U.S.-manufactured or U.S.-launched satellites within their jurisdiction, excluding non-U.S. satellites. On a global scale, ITU handles the filings, but only orbital data can be considered primary, while mass data must be sourced from other references, as we have done in this paper. ITU does not currently have a policy requiring the submission of ODM plans, which would provide mass data as primary information. Therefore, in this paper, we rely on the FCC data, and the discussed method can act as a foundational research with use of primary data after being mandated. If ITU were to adopt policies promoting sustainable practices by mandating the submission of an orbital debris mitigation (ODM) plan in the form of NASA Debris Assessment Software (DAS) reports, this approach could be extended to satellites launched globally.

2.3. LCA and System Boundary

Life cycle assessment (LCA) is a tool used to evaluate the environmental impacts and resource utilization throughout a product's life cycle, encompassing stages from raw material acquisition through production and use phases to waste management. The methodological development in LCA has been robust, and it is widely applied in practice [37]. This life cycle encompasses a series of interconnected stages, beginning with the acquisition or generation of raw materials from natural resources and concluding with the final disposal of the segment [38]. It is widely used across many industries as a tool to compare two products and their environmental footprints, allowing the selection of the product with the lowest environmental impact. To perform LCA, a systemic perspective is needed to

support decisions that have effects on the sustainability of policies, production systems and services, i.e., the environmental, social, and economic spheres in which the concept of sustainability is articulated. This is because measures aimed at achieving one specific goal (like reducing greenhouse gases) might involve negative consequences that were not considered in the first instance, whether they be different impact types (i.e., triggering unexpected environmental, social, or economic mechanisms) upon different geographical areas or stages of the value chain of a product or service (i.e., the life cycle). Including all these aspects in the decision-making process to avoid so-called “burden shifting” is a great advantage that the application of life cycle thinking brings to the development of policies, products, and services in today’s globalized context [39]. ISO standards 14040 and 14044 deal with LCA:

1. ISO 14040:2006 Environmental management—Life cycle assessment—Principles and framework; this provides a clear overview of the practice, applications, and limitations of LCA to a broad range of potential users and stakeholders, including those with a limited knowledge of life cycle assessment;
2. ISO 14044:2006 Environmental management—Life cycle assessment—Requirements and guidelines; this is designed for the preparation of, conduct of, and critical review of, life cycle inventory analysis. It also provides guidance on the impact assessment phase of LCA and on the interpretation of LCA results as well as the nature and quality of the data collected [7]. When it comes to “life cycle assessment” or “analysis”, several of NASA studies do not match with the ISO standards discussed above. They cover only economic costs, omitting the environmental impacts [9]. Therefore, NASA studies were excluded from our research. However, based on the generic ISO standards that drive LCA studies in any sector, ESA has developed a space-specific LCA that can be used for space missions. Space System Life Cycle Assessment guidelines aim to establish the methodological rules on how to correctly perform space-specific LCAs. It can be applied on two levels directly [10]:

Level 1: System level (Space system/launch segment/ground segment/space segment). Figure 1 below represents the entire system boundary of a space mission. The ESA handbook is formatted in a way that impact assessment in terms of midpoint indicators can be calculated for the entire space mission or even for individual segments without taking into account other segments.

Level 2: Equipment/component/material/process.

ESA LCA handbook is used to perform the analysis in this paper. For the analysis, we focus on LEO constellation satellites (space segment from Level 1) and on Level 2 (equipment/component/material/process), considering that the LCI from the ESA database includes subsystem-level and component-level mass budget data. Figure 2 below shows the Level 2 classification on C + D (detailed definition + qualification and production). In this paper, we focus solely on the space segment. The calculations are further limited to the C + D phase, encompassing the production of platform, payload and propellant. The calculation includes equipment production processes necessary for the Starlink satellite assembly. Usually, for single-satellite manufacturing, the engineering model (EM), structural model (STM), and qualification model (EQM) are included because of their significant impact on midpoint indicators. As this research focuses on a constellation of satellites, STM, EM, and EQM are also excluded because of negligible contribution to the final midpoint indicator results.

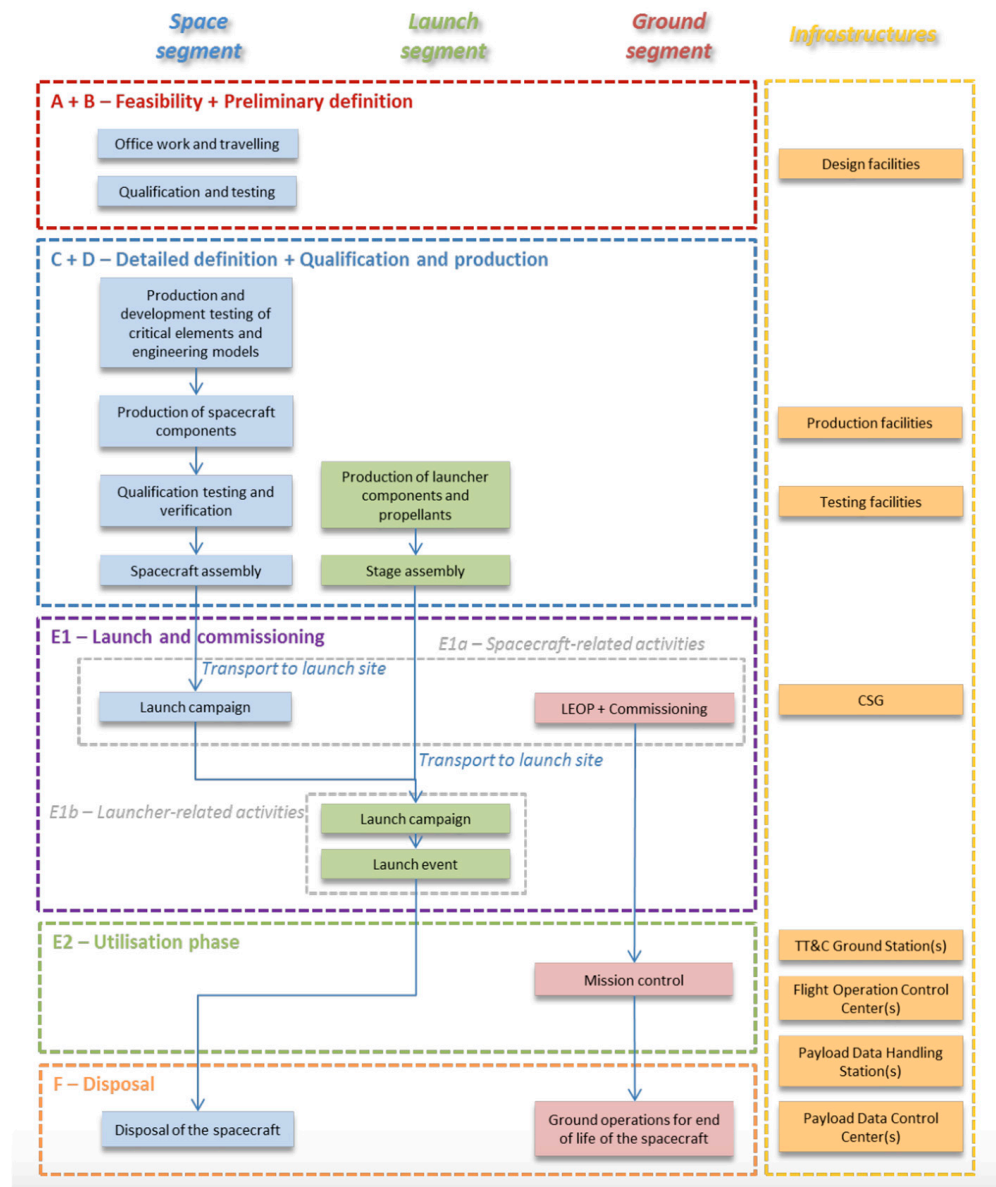


Figure 1. Space mission system boundary [10].

Once all resources have been defined for a specific impact category, the cumulative impact of the product system within that category can be approximated by aggregating the characterized emissions associated with that impact category. This method is iteratively applied to all impact categories within a methodology, often numbering 10 or more, to furnish an assessment of the potential environmental strain induced by a product across various categories. These evaluations of environmental strain are commonly referred to as midpoint indicators [40].

Figure 3 below represents the scope of the ESA's Life Cycle Inventory (LCI) database for equipment production) [10]. It covers upstream activities that include all necessary procedures for the external manufacturing of primary materials and/or sub-components utilized on the production premises, as well as core activities, which includes primary operations, spanning from the initial to the final stages, and encompassing all tasks undertaken by the organization responsible for generating the LCI.

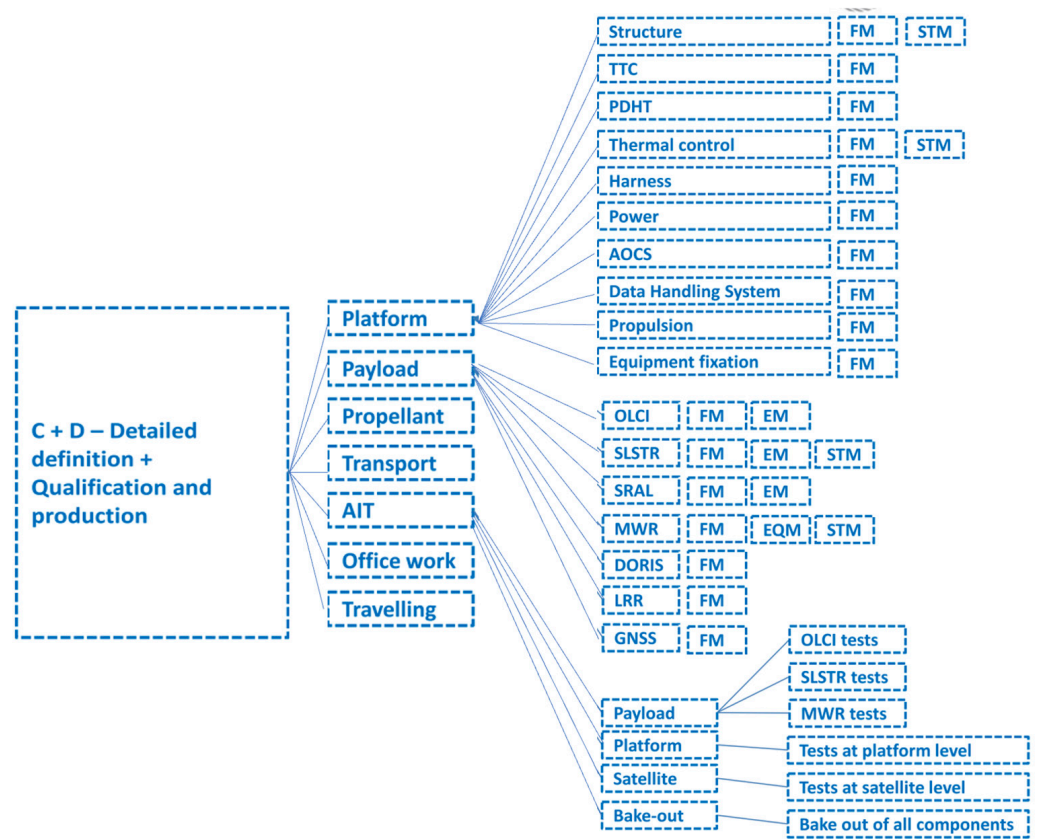


Figure 2. System boundary of a space segment for LCA in the C + D phase [10].

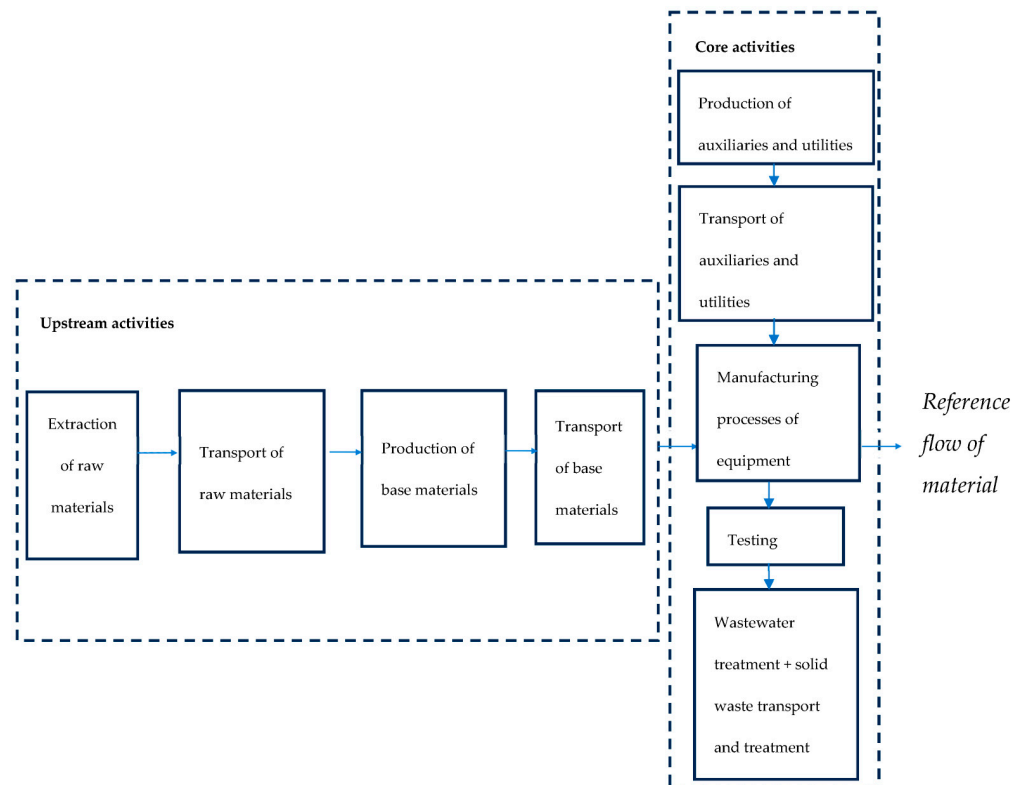


Figure 3. Scope of equipment production [10].

2.4. LCA in Space Missions and Research Gap

Table 2 shows the key literature exploring LCA across the various components of a complete space mission, including the launch segment, space segment, and ground segment. However, as the focus of this case study is on the space segment, we focused on 14 relevant papers from [41]. Of these, ten papers address the complete space mission, which include [42–51], while four specifically focus on only space segment [52–55]. Papers on complete space mission LCAs were also examined, as they encompass the space segment as part of the broader mission analysis.

Table 2. Key literature of LCA in space missions.

LCA Category	Description	Sources
Complete space mission	Deloitte and Thales conducted an LCA on the Sentinel-3 satellite, utilizing primary data provided by Thales, the manufacturer of the Sentinel-3 satellite	[42]
Complete space mission	Research focused on orbital debris; no calculation done	[43]
Complete space mission	LCA for two alternative propellants	[44]
Complete space mission	Research focused on orbital debris; no calculation done	[45]
Complete space mission	EPFL Cubesat primary data	[46]
Complete space mission	Primary data from Stathyclyde mission design team for MIOS mission	[47]
Complete space mission	Thales presenting Sentinel 3 result, as they are the manufacturer	[48]
Complete space mission	Qinetiq is the manufacturer; LCA in this paper is also performed by Qinetiq with their primary data	[49]
Complete space mission	Research focused on developing open-source LCA platform; no calculation done	[50]
Complete space mission	LCA for space-based solar power with data from NASA mission	[51]
Space segment	LCA performed by Thales Aliena Space with primary data from their missions	[52]
Space segment	LCA performed for three space elevator designs with mass data from another paper	[53]
Space segment	LCA performed by OHB for CO2M mission with primary data from OHB, as they are the prime contractor	[54]
Space segment	LCA performed by TUDelft for their own Cubesat Delfi-n3Xt	[55]

Based on Table 2, research from [42,46–49,52,54,55] presents the LCA results based on their own manufacturing capabilities. Hence, they have the access to the primary data, which is essential for conducting space-specific LCAs. As they are also the manufacturers, performing the LCA is straightforward due to the availability of primary mass budget data. Refs. [43,45] explored the relationship between orbital debris and LCA, although they did not provide any detailed calculations. Ref. [53] explored the LCA for three alternative space elevator design from another paper. Ref. [44] explored LCA for two alternative propellants for Sentinel 3 satellite. Ref. [51] performed an LCA using data from a NASA mission design, while [50] investigated the use of an open-source platform for conducting space mission LCA. Hence, it can be inferred that there is a clear gap in the availability of a generic method for predicting the mass budget of commercial satellites. This limitation hinders the ability

of users, other than those with direct access to primary mass budget data, to perform life cycle assessments (LCA) on satellite missions. Consequently, the current approach to LCA remains largely restricted to manufacturers or entities with privileged data access.

As discussed in Section 2.1, a research gap exists in the field of “sustainability for space”. The ESA LCA handbook addresses this gap by providing guidelines for space-specific LCAs focused on sustainability. However, using the ESA LCA handbook requires access to subsystem-level mass budget data for a specific satellite, which are often unavailable due to commercial confidentiality. Therefore, while the ESA handbook is beneficial for satellite manufacturers with access to this data, a gap remains for generic users who lack such information.

3. A Method for Quantifying the Environmental Impacts of Manufacturing Low Earth Orbit (LEO) Satellite Constellations

Figure 4 below illustrates a five-stage method for performing a life cycle assessment (LCA). The process begins with the acquisition of orbital data for the satellite from Federal Communications Commission (FCC) filings. The rationale for selecting FCC filings as the data source is discussed in detail in Section 2.2.2. Following this, the mass budget is partitioned using the European Space Agency (ESA) Life Cycle Inventory (LCI) database, as elaborated in Section 2.2.1. Parametric estimation is then employed to predict the propellant mass, with the justification for this method provided in Section 2.2.2. Afterward, the final mass budget is estimated, and midpoint indicators are calculated according to the system boundaries outlined in Section 2.3. In this approach, SimaPro 9.5 software is used to compute the midpoint indicators after the final mass budget has been established.

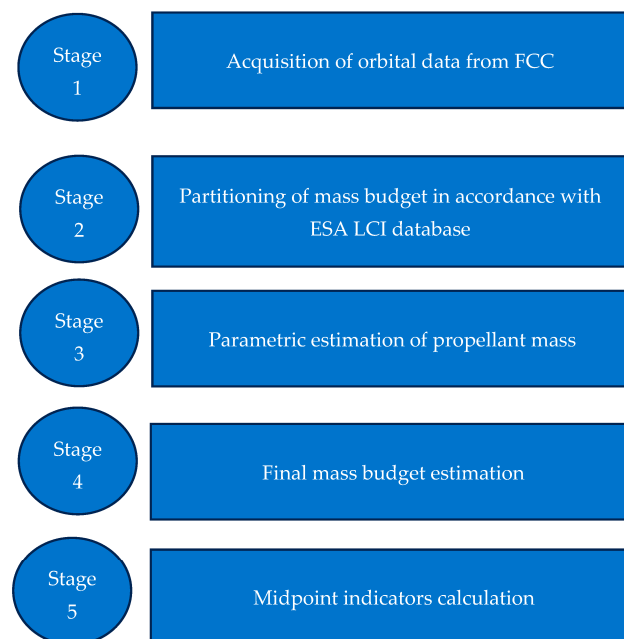


Figure 4. Illustration of method for calculating midpoint indicators.

4. Starlink as Case Study

The rationale for focusing on low Earth orbit (LEO) in this study is due to the significantly higher number of orbiting objects of all types in LEO compared to other orbital regimes. It is evident that a greater number of satellites are launched into LEO than other orbital regimes. Figure 5 below illustrates the current number of orbiting objects by type and orbital regime, as reported in the latest space debris environment report by ESA [56].

	PL	PF	PD	PM	RB	RF	RD	RM	UI	Total
LEO	10136	5747	115	227	953	3274	40	579	83	21154
GEO	800	3	3	9	64	0	0	0	33	912
EGO	521	1	1	49	203	82	3	4	1889	2753
GTO	51	28	1	10	235	202	12	51	626	1216
NSO	282	0	0	1	96	0	0	2	38	419
MEO	77	0	4	49	25	42	1	4	415	617
LMO	83	138	5	46	246	590	22	215	955	2300
MGO	68	65	1	3	177	1968	4	0	1178	3464
HEO	29	13	0	1	54	113	0	0	1101	1311
Other	45	0	0	5	5	0	0	0	97	152
Total	12092	5995	130	400	2058	6271	82	855	6415	34298

Figure 5. Current number of orbiting objects per type and orbital regime [56].

PL stands for payloads, which refer to space objects designed to perform specific functions in space, excluding launch functionality [56]. This category includes operational satellites as well as calibration objects. Since all operational satellites come under the payloads category, from Figure 5, we can infer that most of the debris in LEO is caused by operational satellites. Hence, in the LEO satellite category, particular focus is given to the Starlink constellation of satellites, and it was taken as our case study. The key reason is because Starlink represents the world's largest low Earth orbit (LEO) internet constellation, slated to encompass a total of 42,000 satellites [57]. The next-largest commercial constellation planned in LEO is by OneWeb, with 7000 satellites [58].

4.1. Stage 1: Acquisition of Orbital Data from FCC

In 2018, SpaceX proposed orbit modification for their 1600 operating satellites from 1150 km to 550 km, and as part of their proposal request, an atmospheric demise report using NASA's Debris Assessment software was also attached for Starlink satellites [36]. The 1600 satellites closely match the 1665, V1 model. Hence, we assume that V1 was used in the analysis of debris assessment. To begin with, V1 version that has a total mass of 260 kg was taken. As of today, four versions of Starlink satellites have been launched. The mass value of each version is shown in Table 3. And the data regarding the number of satellites that have been launched into space are taken from [59].

Table 3. Starlink versions.

Version	No. of Satellites	Mass (kg)	Reference
V0.9 (Launched)	60	217	[35]
V1 (Launched)	1665	260	[60]
V1.5 (Launched)	2139	306	[61]
V2 (Planned launch)	29,988	2000	[62]
Total	33,852		

In this paper, Starlink version 1 mass budget is estimated based on the average dry mass budget table in Table 1. Table 1 cannot be explicitly implemented because the equipment list in the ESA LCI database differs for two subsystems, power, and propulsion.

4.2. Stage 2: Partitioning of Mass Budget in Accordance with ESA LCI Database

Table 3 indicates that the mass of a Starlink V1 satellite is 260 kg. However, it is necessary to predict the propellant mass and dry mass in terms of a detailed subsystem/component-level mass budget for the V1 satellite, consistent with the ESA LCI database. The average mass budget for low Earth orbit (LEO) satellites is derived from [25] and is discussed in detail in Section 2.2.1. The European Space Agency (ESA) Life Cycle Inventory (LCI) database is examined extensively in Section 2.3. For an accurate life cycle assessment

(LCA), it is crucial to partition the mass budget in alignment with the categories and structure outlined in the ESA LCI database. Table 4 represents the average dry mass distribution of subsystems and its relationship with the ESA's LCI data. The ESA's LCI database is more detailed for propulsion and power systems. LCI is further divided into detailed components regarding power, harness, thruster, and tank. The detailed partitioning is only necessary for the power, harness, thruster, and tank propulsion, as the rest of the LCI database matches with the average mass budget, as we can see in Table 4 below. Detailed partitioning is performed with space systems engineering budget allocation techniques for power, harness, thruster, tank, and propulsion subsystem mass.

Table 4. Estimating mass budget based on European Space Agency Life Cycle Inventory database.

Subsystem	Average Dry Mass Distribution (%)	ESA LCI Database Subsystem/Components	Final Mass Budget Distribution	Comment	Reference
Payload	31%Mdry	Payload type	31%Mdry		[24]
Structure and mechanisms	27%Mdry	Structure	27%Mdry		[24]
Thermal control	2%Mdry	Thermal control	2%Mdry		[24]
Power (including harness)	21%Mdry	Power	21%Mdry (-) 0.02 × Mdry	0.02 is taken as average from (0.01–0.04 × Mdry)	[24]
		Harness	0.02 × Mdry		
TT&C	2%Mdry	TT&C	2%Mdry		[24]
On-board processing	5%Mdry	Data handling	5%Mdry		
AOCS	6%Mdry	AOCS	6%Mdry		[24]
Propulsion	3%Mdry	Thruster	3%Mdry mass (-) 10% of propellant calculation	Propellant valve/pipeline mass are considered negligible 10% of propellant	[24]
		Tank	10% of propellant calculation		[24]
Other (Balance+Launch)	3%Mdry	Other (structure)	3%Mdry		[24]
		Propellant	Propellant calculation		4.3

4.3. Stage 3: Parametric Estimation of Propellant Mass

Based on Table 4, it is evident that estimating the dry mass of the satellite requires the prediction of the propellant mass. The total mass of the Starlink V1 satellite is 260 kg, and the dry mass (Mdry) can only be determined by subtracting the propellant mass from the total mass. Therefore, in this section, parametric estimation techniques are employed to predict the propellant mass for the V1 satellite, as discussed before in the Section 2.2.2. SpaceX uses a Hall-effect electric propulsion subsystem for their satellites [63]. The specific impulse is around 1500 s for the engine and is used to move the Starlink to the operational orbit and then for station keeping as well as eventually to deorbit them after their operational lifetime [64]. Based on the specific impulse value, the BHT600 Hall-effect thruster is taken as a reference. To find the propellant mass and dry mass, the rocket equation is used [25]:

$$m_f = m_o e^{-\left(\frac{\Delta v}{v_0}\right)}, \quad (1)$$

where m_f (final mass) can be expressed with initial mass m_o , with the propellant and the mass of propellant m_p .

$$m_f = m_o - m_p \quad (2)$$

From Table 1, m_f value (final mass) of the Starlink version 1 is taken as 260 kg.

In order to find the propellant mass, the orbital data of Starlink are necessary. These data are acquired from SpaceX filings to the FCC. The insertion altitude of Starlink is from 300 km to 350 km based on the solar activity [63]. For the worst case scenario, 300 km is taken for calculating the DeltaV, with the operational altitude of 550 km. The operational orbit seems to be circular, and different inclinations are planned for the constellation according to the report submitted by SpaceX to FCC [63]. The calculation assumes a fuel-efficient coplanar Hohmann transfer between two circular orbits [24].

$$a_{tx} = (r_A + r_B) / 2 \quad (3)$$

Equating the values of $r_A = 300$ km and $r_B = 550$ km, we can obtain a_{tx} value as $a_{tx} = 6796$ km.

$$V_{iA} = (\mu / r_A)^{(1/2)} \quad (4)$$

where inserting values of $\mu = 631.348$ (gravitational constant \times Earth's mass) and $r_A = 300$ km yields the following:

$$V_{iA} = 7.72 \text{ km/s} \quad (5)$$

$$V_{fB} = (\mu / r_B)^{(1/2)} \quad (6)$$

where inserting values of $\mu = 631.348$ (gravitational constant \times Earth's mass) and $r_B = 300$ km, $V_{fB} = 7.58$ km/s.

$$V_{txA} = \mu [(2/r_A - 1/a_{tx})]^{(1/2)} \quad (7)$$

where inserting values of μ , r_A as 300 km, and a_{tx} as 6796 km returns $V_{txA} = 7.8$ km/s.

$$V_{txB} = \mu [(2/r_B - 1/a_{tx})]^{(1/2)} \quad (8)$$

where inserting values of μ , r_B as 550 km, and a_{tx} as 6796 km returns $V_{txB} = 7.51$ km/s.

$$\Delta V_A = |V_{txA} - V_{iA}| = 0.08 \text{ km/s} \quad (9)$$

$$\Delta V_B = |V_{txB} - V_{fB}| = 0.07 \text{ km/s} \quad (10)$$

$$\Delta V_{total} = \Delta V_A + \Delta V_B = 0.15 \text{ km/s or } 150 \text{ m/s} \quad (11)$$

Hence, 150 m/s ΔV is required for orbit rising and for 5 years of station keeping in LEO. For this purpose, the 6–26 equation from [24] is used. The coefficient of drag (CD) is assumed to be 1.01 (for a cube). The best possible match for the Starlink design (rectangular cross-section) when compared to available CD data for different shapes is a cube. The cross-sectional area A value for Starlink is taken from [65]. The dimensions are given as length 3.2 m, width 1.6 m, and height 0.2 m. The cross-sectional area exposed to the flight path can be either 3.2 m \times 0.2 m or 1.6 m \times 0.2 m. For the worst case scenario, 3.2 m \times 0.2 m is taken as A . The maximum density value of 9.25×10^{-13} kg/m³ at 550 km altitude at solar maximum is taken for this calculation, a value that corresponds to the semi-major axis, which is 6921 km. The change in velocity experienced by Starlink for one revolution by inserting all these values is represented by the following:

$$\Delta V_{rev} = \pi(CDA/m)\rho a^2 = 0.0003940266401 \text{ m/s}, \quad (12)$$

ΔV_{rev} is the change in velocity experienced by Starlink for just one revolution. For calculating the ΔV for the entire mission duration, the total revolution Starlink takes in its operational lifetime at 550 km altitude should be determined. In order to determine total

revolution K , we need to find the orbital period value. Equation (13) is used to find the mean motion, and Equation (14) is used to find the orbital period P .

$$\text{Mean motion} = \sqrt{\frac{\mu}{a^3}} = \sqrt{\frac{\mu}{r^3}} = 0.00109 \frac{1}{s} \quad (13)$$

$$P = \frac{2\pi}{\text{mean motion}} \quad (14)$$

P from Equation (14) is 96.07 min, with one sidereal day equal to 1436.068 min. Hence, the total minutes for 5 years of mission duration will be $1825 \times 1436.068 = 27,298.95$ min. Dividing this value with 96.07 min for one revolution, we obtain the total revolutions K Starlink will undergo in 5 years.

$$K = 27,280 \text{ revolution}$$

When we multiply ΔV_{rev} with total revolution K , we obtain the total change in velocity ΔV experienced by Starlink for 5 years.

$$\Delta V = \Delta V_{\text{rev}} \times 27,280 = 10.74 \text{ m/s}, \quad (15)$$

The ΔV value excludes solar panel drag, and the next step is to calculate the ΔV during de-orbit from 550 km operational orbit to 80 km. Starlink satellites start to demise around 80 km altitude. So, 80 km is assumed here from the demise report of Starlink by SpaceX to FCC [66]. The deorbit ΔV equation is taken from [24], where H_i is the operational altitude (550 km), and H_e is the end orbit altitude, which is 80 km. By equating these values, we obtain the following:

$$\Delta v_{\text{deorbit}} = V \left[\frac{H_i - H_e}{4(R_E + H_e)} \right] = 138 \text{ m/s}, \quad (16)$$

Therefore, the total Δv can be represented as given below:

$$\Delta v_{\text{total}} = \Delta v_{\text{Orbit raising}} + \Delta v_{\text{Orbit maintenance}} + \Delta v_{\text{Deorbit}} = 298.74 \text{ m/s}, \quad (17)$$

Equation (1) can be rewritten, and mass of propellant can be represented as follows:

$$m_p = m_o \left[1 - e^{-\left(\frac{\Delta v}{v_0}\right)} \right] \quad (18)$$

Now, the total Δv value from Equation (16) and v_o value are equated in Equation (17) and can be expressed as $I_{sp} \times g$, where I_{sp} is the specific impulse, which is 1500 s, as discussed before, and g is acceleration due to gravity. The high specific impulse for Hall-effect thrusters is the key reason why the propellant mass varies drastically from traditional chemical propellant, and it proves the importance of this detailed propellant mass calculation for the estimation of the final mass budget. By equating specific impulse and g value into Equation (18), we can obtain the mass of propellant m_p :

$$m_p = 4.2 \text{ kg} \quad (19)$$

Hence, the mass of the propellant is 4.2 kg. Therefore, the dry mass can be represented as Total mass (m_f) – Mass of propellant (m_p) = 260 – 4.2 = 255.8 kg.

4.4. Stage 4: Final Mass Budget Estimation

As outlined in Section 4.3, both the total dry mass and the propellant mass are known. Table 5 below represents the dry mass partitioning and propellant mass, which shows the final Starlink version 1 mass budget distribution. The mass budget is partitioned according to ESA's LCI database and the type of case study. For instance, Starlink uses an electric

propulsion system. Hence, appropriate thruster, propellant, and tank are taken into account instead of taking the LCI of a generic propulsion subsystem for accuracy. This table could be applied to any LEO constellation mission for finding the mass distribution for LCA. However, an LCI of a generic propulsion system could be used if the type of propulsion is unknown.

Table 5. Mass budget table for Starlink version 1.

ESA LCI Database Subsystem/Components	Dry Mass Partitioning and Propellant Mass	Final Starlink Mass Budget Distribution (kg)
Payload	31%Mdry	79.2
Structure	27%Mdry	69
Thermal control	2%Mdry	5.11
Power	21%Mdry (-) $0.02 \times \text{Mdry}$	48.6
Harness	$0.02 \times \text{Mdry}$	5.11
Tracking, telemetry, and control (TT&C)	2%Mdry	5.11
Data handling	5%Mdry	12.79
Attitude determination and control	6%Mdry	15.34
Thruster	3%Dry mass (-) 10% of Propellant calculation	7.2
Tank	10% of Propellant calculation	0.4
Other	3%Mdry	7.67
Propellant	Propellant calculation	4.2
Total		260 kg

4.5. Stage 5: Midpoint Indicators Calculation

In order to calculate the midpoint indicators, it is necessary to have the final mass budget table as input. The midpoint indicators can be calculated either on the subsystem level or component level for the space segment [10]. Table 6 below represents the final midpoint indicator results for 1665 Starlink version 1 satellite. We can see that resource use of minerals and metals contributes the most among other indicators considering the system boundary of the analysis. Since we focus on the production phase of the satellite, usage of minerals and metals contributes to 58 kilopoints out of the total 76 kilopoints. An adapted EF method (version 1) is used for this analysis, and the description of the impact category in Table 6 is taken from the Simapro manual [67]. To demonstrate how the method works, we apply the environmental footprint (EF) method (version 1) as an example. Users of this method should always use the latest adapted version of the EF method [68]. The unit of measurement “point” (Pt) is used here for the analysis. It signifies the annual environmental load. This load encompasses the entirety of production and consumption activities within the U.S. economy. The division of this load is allocated proportionally to represent the share attributable to a single American individual [18].

Table 6. Midpoint indicators results for Starlink version 1.

Midpoint Indicators	Description of Impact Category	kPt
Climate change	Global warming potential over a 100-year period.	1.71
Ozone depletion	Ozone depletion potential (ODP) calculated to assess the destructive effects on the stratospheric ozone layer over a time horizon of 100 years.	0.091
Ionizing radiation, HH	Ionizing radiation potentials: Quantifying the impact of ionizing radiation on the population relative to uranium-235.	0.128

Table 6. Cont.

Midpoint Indicators	Description of Impact Category	kPt
Photochemical ozone formation HH	Photochemical ozone creation potential (POCP): Measurement of the potential contribution to photochemical ozone formation [67].	0.368
Respiratory inorganics	Disease incidence	0.598
Non-cancer human health effects	Comparative toxic unit for humans (CTUh): A metric representing the estimated increase in morbidity in the total human population per unit mass of a chemical emitted, typically measured in cases per kilogram.	1.88
Cancer human health effects	Comparative toxic unit for humans (CTUh): An index expressing the estimated increase in morbidity in the total human population per unit mass of a chemical emitted, measured in cases per kilogram.	1.26
Acidification terrestrial and freshwater	Accumulated exceedance (AE): A measure describing the alteration in critical load exceedance of the sensitive area in terrestrial and primary freshwater ecosystems, influenced by the deposition of acidifying substances.	0.594
Eutrophication freshwater	Phosphorus equivalents: Indication of the extent to which the emitted nutrients reach the freshwater end compartment, with phosphorus considered as the limiting factor in freshwater ecosystems.	4.74
Eutrophication marine	Nitrogen equivalents: Representation of the extent to which the emitted nutrients reach the marine end compartment, with nitrogen considered as the limiting factor in marine water ecosystems.	0.135
Eutrophication terrestrial	Accumulated exceedance (AE): A measure representing the alteration in critical load exceedance of the sensitive area, influenced by the deposition of eutrophying substances.	0.285
Ecotoxicity freshwater	Comparative toxic unit for ecosystems (CTUe): A measure expressing an estimate of the potentially affected fraction of species (PAF) integrated over time and volume per unit mass of a chemical emitted (PAF m ³ year/kg).	0.659
Land use	Soil quality index.	0.044
Water scarcity	m ³ Water eq. deprived.	4.34
Resource use, energy carriers	Abiotic resource depletion fossil fuels (ADP-fossil): It is based on the lower heating value, indicating the depletion of fossil fuel resources.	1.11
Resource use, minerals and metals	Abiotic resource depletion (ADP ultimate reserve)	58
Total		76

5. Discussion and Conclusions

The method presented in this paper answers the primary research question of quantifying the environmental impacts during the production phase of low Earth orbit constellation satellites. The key features of this method include its purpose, which is to predict the mass budget necessary for performing life cycle assessment (LCA). The procedure involves parametric estimation of propellant mass from FCC orbital data and using the average mass budget method, space systems budget allocation technique, and propellant mass value to partition dry mass in accordance with ESA LCI database for estimating the final mass budget. It utilizes Simapro as an LCA tool to perform the analysis. This method

requires data such as FCC orbital data, the satellite's total mass value, and the type of propulsion subsystem. The expected results are presented in terms of midpoint indicators. A major advantage of this method is its ability to predict the environmental footprint of any constellation without needing the detailed mass budget required for performing LCA. This method is applicable in predicting the planned footprint of upcoming constellations and will pave the way for developing a more integrated sustainability framework that considers all three aspects of sustainability. The mass budget table for a LEO constellation, including propellant calculation, answers the research question, and it is presented in Section 2.3, with Starlink as a case study. The section is tailored according to the ESA LCI database. The reason for the need of Table 1 partitioning is discussed in detail in the average mass budget section. Using the method and taking Starlink version 1 constellation as a case study, the total environmental impact is estimated to be 76 kilo points. The results are represented in Table 6.

5.1. Theoretical Contributions

This subsection outlines the novel theoretical insights generated by the present study, shedding light on the broader scholarly discourse within the field. Firstly, by synthesizing the existing literature, this research advances the understanding of performing LCA for LEO constellation satellites with the usage of the average mass budget. It introduces a novel perspective by combining the average mass budget method and parametric method, which results in a more accurate estimation of mass budget for an LEO constellation, which is essential for performing a life cycle assessment. Moreover, through rigorous analysis, this study extends theoretical boundaries by developing a new theory with the help of FCC orbital data as input and combining the existing average mass budget table for LEO satellites and the parametric method, which depends on using mathematical equations. Additionally, by addressing gaps and inconsistencies in previous research, this study contributes to refining and clarifying theoretical propositions, offering a more nuanced understanding of performing life cycle assessment for satellites without readily available mass budget data. Overall, the theoretical contributions of this research serve to enrich the theoretical landscape of "sustainability for space" and provide valuable insights for future research endeavors.

5.2. Methodological Contributions

The generic method discussed in this paper could be used to predict any subsystem/equipment-level mass budget of a satellite, which is essential for calculating midpoint indicators with the help of FCC data and ESA's LCI database. ESA has released an updated LCI space-specific database to the public [69]. This will be primarily beneficial for users with readily available component-level mass budget data. The results will be accurate if users use primary data (component level) to calculate the environmental effects during any of the phases for their respective satellite. However, for users without primary data and who want to predict the footprint of any satellite or constellation of satellites, the method presented in this paper would be beneficial.

5.3. Practical Contributions

LEO satellite operators/manufacturers could use this method during early phases of mission design to predict their own footprint during production phase of satellites based on the mission design. This could pave way for focusing on specific midpoint indicators they are interested in and change the mission design if they want to focus on implementing more sustainable practices during production phase. Apart from LEO manufacturers, any user of this method can predict the footprint of any LEO satellite provided orbital data filed by the commercial company/space agency, even without knowing the mass budget data required to perform LCA.

5.4. Limitations and Future Work

The FCC authorization is limited to U.S.-manufactured and U.S.-launched satellites. Therefore, the method presented in this paper is currently applicable only to satellites launched from the United States. However, as discussed in Section 2.2.2, if the ITU were to adopt the requirement for submitting a NASA Debris Assessment Software (DAS) report, it would be possible to extend this method to satellites launched globally. The method outlined in this paper is for the C + D phase represented in Figure 2, and it is limited to the system boundary discussed in the LCA and system boundary section. It does not account for any other sections other than platform, payload and propellant, as represented in Figure 2. Future work could involve developing a framework for quantifying the environmental and economic impact by incorporating the circular approach for low Earth orbit satellites. For instance, in this paper, we discussed the environmental impacts on Earth due to the production of satellites. This is just one aspect that could be considered while designing a space mission. The other aspect is re-entry pollution caused by discarded satellites and the economic aspect. Hence, a framework that can give insights into economic and environmental aspects (production as well as re-entry pollution caused by discarded satellites in the atmosphere) on Earth could be developed. The outcomes could serve as a basis for subsequent investigations aimed at formulating a sustainability framework conducive to the integration of more circular practices for the space industry on Earth and in space.

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Glossary

AIT	Assembly integration and test
COPUOS	Committee on the Peaceful Uses of Outer Space
EF	Environmental footprint
EM	Engineering model
EQM	Qualification model
ESA	European Space Agency
FCC	Federal Communication Commission
ISO	International Organization for Standardization
LCA	Life cycle assessment
LEO	Low Earth orbit
LCI	Life cycle inventory

m_f	Final mass
m_o	Initial mass
m_p	Mass of propellant
NASA	National Aeronautics and Space Administration
OECD	Organization for Economic Cooperation and Development
Pt	Point
SMAD	Space mission analysis and design
STM	Structural model
TT&C	Tracking telemetry and control
UN	United Nations

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