## Aluminum based large telescopes: the ARIEL **Mission case**

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## INTRODUCTION

## **MIRRORS MANUFACTURING**

## **NiP Treatment**

Telescope Assembly (TA) of the ARIEL The space mission passed the Preliminary Design Review (PDR) in 2023. Due to the high degree of innovation and risk of the implementation (see [1] and [2]), the Design Authority remained with the team headed by INAF both for the structural model (SM) and for the engineering one (EM) which are under construction in the recent months. At the same time, it continues the Research & Development activity on some critical parts of the telescope, mainly the Primary Mirror M1 with its mechanical support and the M2-M4 mirrors. Here below is shown the TA structure, highlighting the main components (see [3]).





To improve the quality of aluminum mirrors, a NiP treatment is



Fig. 2 ARIEL M1-M4 EM mirrors.

EM M1 - Polishing

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	LSF SFE Target	Run	SFE RMS [nm]	Low spatial frequency RMS [nm]	Residual 36 terms RMS (nm)	Residual 120 terms RMS [nm]	Date	Not
900		0	815	814	158	45	22.01	+1g
800		3	751	750	130	45	31.01	+1g
700		7	583	581	107	46	07.02	+1g
100		9	520	518	97	45	12.02	+1g
600 [ш] 500 SW2 400		13	406	403	78	47	16.02	+1g
		15	290	286	70	46	21.02	+1g
		17	166	159	63	46	26.02	+1g
11		19	144	137	56	45	06.03	+1g
300		20	129	121	52	45	08.03	+1g

applied. Being harder than Aluminium, can lead to better quality surface during polishing activities: it permits more control and precision in removing higher aberration orders, leading to improved encircled energy and less scattered light. In the ARIEL mission, this treatment was planned for each mirror; however, since the polishing on NiP is applied at ambient temperature and the telescope will work at cryogenic temperatures (50 K), it could, in principle, cause deformations on the surface of M1, introducing aberrations that could be a limitation for the optical performances of the telescope. The reason of this is that NiP and Aluminum have different Coefficients of Thermal Expansion (CTE) and Young Moduli (YM), see [4] for data on NiP.

FEA simulations have been performed on M1: the overall deformation has been derived and characterized in function of different parameters of the deposition, such as: NiP thickness, NiP Young modulus and NiP CTE, since no unique values are present.

It can be seen that with a 2 µm thickness NiP a total deformation of 408 nm is found, reduced to just 36 nm RMS once the first four Zernike terms (i.e., Piston, Tip, Tilt and Power) are removed. The NiP coating is still under investigation, as there are numerous uncertainties regarding its mechanical characteristics, which vary significantly depending on Phosphorus content and temperature. In addition, it is necessary to establish the feasibility of depositing a very thin layer with uniform thickness. The situation is under study and a probable substitute of NiP will be an additional polishing run using a new, proprietary technique that is focused on the removal of the medium and high frequencies, without affecting the surface form of the surface (low aberrations).

Fig. 1 ARIEL TA components.

Currently, the telescope mirrors, which are the most critical components of the telescope, are under the manufacturing phase of the EM models. Each mirror will be subjected to the following processes, in chronological order:

- Row machining
- Diamond turning
- Polishing
- Coating deposition

The primary mirror EM completed all the manufacturing phases with success, complying with the SFE requirements (see Fig. 2-4). M2 to M4 completed the diamond turning process and will go through the polishing and coating phases in the next months. However, with respect to M1, the manufacturing of these mirrors is considered less critical.



Fig. 3 ARIEL M1 EM polishing campaign.



Tab. 1: ARIEL Mirrors specifications

Mirror Mirror type Clear aperture Clear aperture SFE at



Fig. 5 Total deformation due to NiP treatment (left image), deformation due to NiP treatment without the first 4 Zernike terms (Piston, Tip, Tilt and Power, right image).



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		shape	dimensions at 50 K (mm)	293 K (nm)
M1	Concave	Elliptical	1100 x 746.8	65 <sup>1</sup>
	mirror			
M2	2 Convex	Elliptical	110 x 80	40 <sup>2</sup>
	hyperbolic mirror			
Ma	B Concave	Elliptical	28 x 20	182
	parabolic			
	mirror			
M	IPlane mirror	Circular	24	122

1: The indicated SFE is measured.

2: The indicated SFE is as per specification and not still measured, since the mirror manufacturing shall still to be completed.

1. Tozzi, A. et al., "Toward ARIEL's 3. Garcia P.A. et al., "ARIEL TA Optical primary mirror", Proc. SPIE 12180; Subsystems Vibration Test doi: 10.1117/12.2628906" Specification" (ARIEL-UPM-PL-TS-002). 2. Caldwell, A. et al., "ARIEL Payload Design Description" (ARIEL-RAL-PL-4. Kinast J. et al., "Minimizing the bimetallic bending for cryogenic metal optics based on electroless nickel," Proc. SPIE 9151, doi.org/10.1117/12.2056271

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