

# Preparation and Rheological Characterization of Dilute Polydisperse Bubble Suspensions



Stamatina Mitrou<sup>1,2</sup>, Luca Mazzei<sup>1</sup>, and Panagiota Angeli<sup>1</sup>

<sup>1</sup>ThAMeS Multiphase Group | Department of Chemical Engineering

<sup>2</sup>EPSRC CASE studentship supported by GSK | Health Partner

## Motivation

- ❖ Air is entrapped during the manufacturing of toothpastes due to the high-shear mixing of the components.
- ❖ Bubbles have been shown to affect the viscosity of the ambient fluid, inducing complex viscoelastic phenomena and leading to density changes and inconsistencies during filling.
- ❖ This project aims to investigate the rheology of polydisperse bubble suspensions and help to understand how aeration affects the viscosity during the manufacturing of formulations.



## Introduction

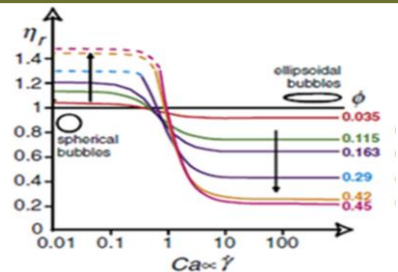


Fig.1: Rheological behaviour of monodispersed bubble suspensions.

- ❖  $Ca \gg 1 \rightarrow$  bubbles deform significantly and the flow around them is facilitated.
- ❖  $Ca \ll 1 \rightarrow$  bubbles deform negligibly (being almost spherical) and the flow around them is hindered.
- ❖  $Ca \sim 1 \rightarrow$  onset of shear-thinning behaviour for monodispersed suspensions.

For steady shear states, the capillary number ( $Ca$ ) is defined as follows:

$$Ca = \frac{\eta_0 \dot{\gamma}}{\sigma} = \lambda / t_d$$

$\lambda$ : relaxation time of the bubbles;  $t_d$ : deformation time of the bubbles.

## Experimental design

- ❖ Aeration systems used: porous membrane set up, coupled with a high shear mixer.
- ❖ Ambient fluids tested: viscous mineral oil (9.4 Pa\*s)
- ❖ The rheology was investigated using an Anton Paar rotational viscometer and simple shear tests.
- ❖ **Challenge:** i) low bubble volume fractions. Normal stress differences could not be measured. ii) no control over achieved volume fraction.
- ❖ Solution: design of a new propeller aerator able to increase aeration efficiency.

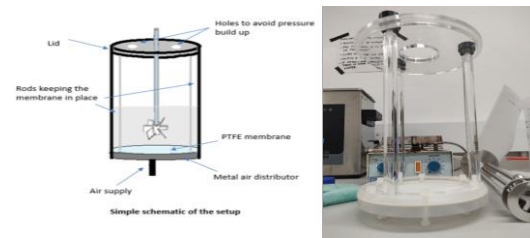


Fig.2: Porous membrane aeration setup

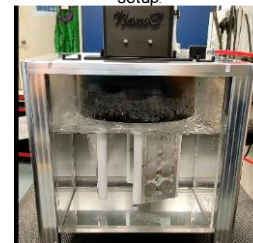


Fig.3: Propeller aerator

## Results

- ❖ Maximum volume fraction  $\phi = 15.08\%$ .

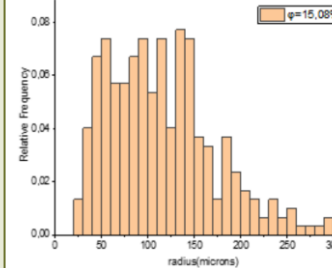


Fig.4: Bubble size distribution

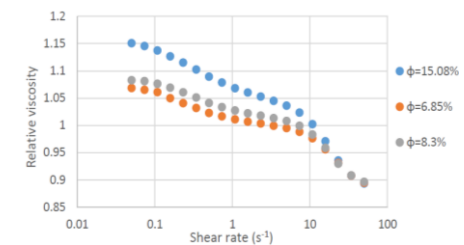


Fig.5: Relative Viscosity VS shear rate

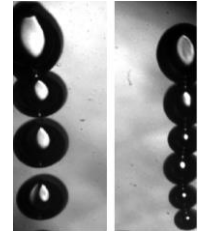


Fig.6: Bubble coalescence and threading for  $10\text{ s}^{-1}$  and  $20\text{ s}^{-1}$ .

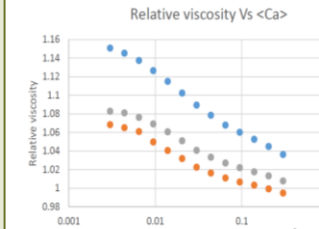


Fig.7: Relative viscosity VS  $\langle Ca \rangle$  in min. oil bubble suspensions.

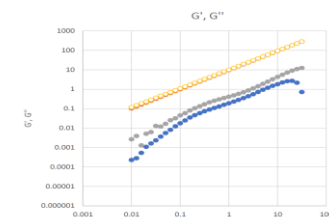


Fig.8:  $G'$ ,  $G''$  for min. oil bubble suspensions.

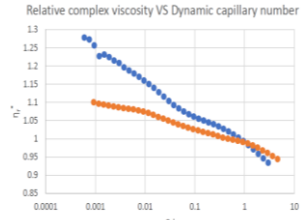


Fig.9:  $\eta_r^*$  VS  $\langle Cd \rangle$

- ❖ The produced bubble suspensions were found highly polydisperse.
- ❖ Double power law decay of viscosity.
- ❖ Time sweep and rheo-PIV tests revealed bubble coalescence for shear rates larger than  $5\text{ s}^{-1}$ .
- ❖ The polydisperse bubble suspensions exhibited a more gradual shear-thinning behaviour, which spanned over a range of  $\langle Ca \rangle$  between 0.001 and 0.01. The bubbles do not deform equally and simultaneously due to their different sizes. When larger bubbles have reached  $\langle Ca \rangle = 1$  and their shear-thinning contribution begins to appear, smaller bubbles are still spherical and resist the flow.
- ❖ The elastic character of the suspension increases with the bubble volume fraction.
- ❖ For dynamic capillary numbers slightly larger than one, we observed a decrease of the relative viscosity with the bubble volume fraction. The decrease does not follow the suggested trend for the relative infinite-shear complex viscosity, i.e.  $\eta_r^* = 1 - (5/3)\phi$ .