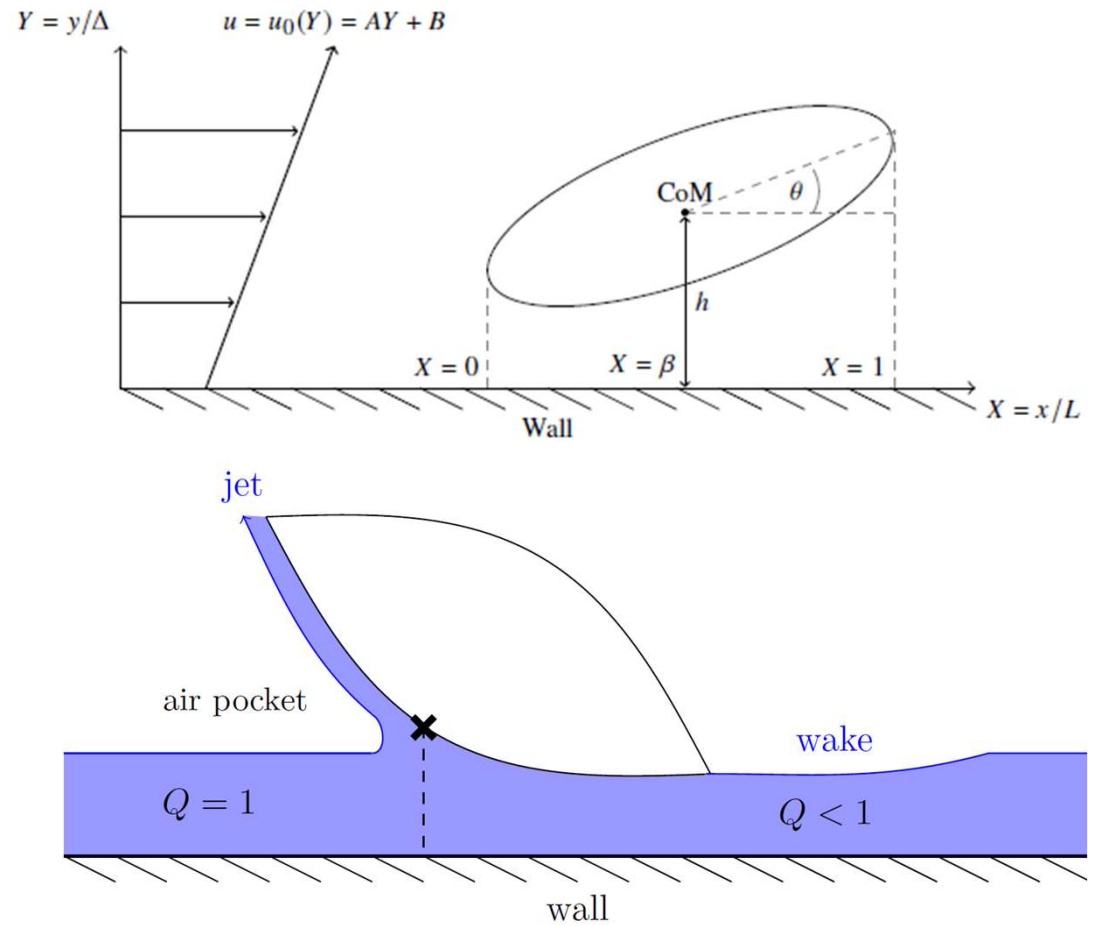




Dynamics of an ice particle submerged in water

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Frank T Smith

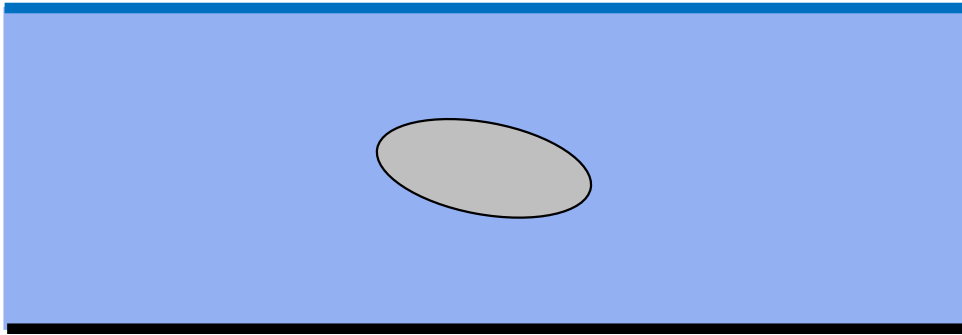
Modelling aircraft icing



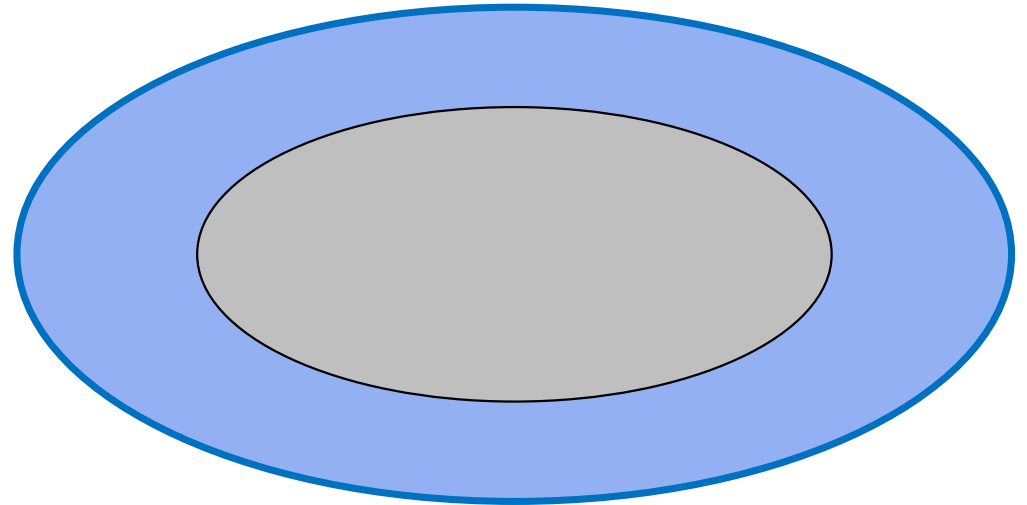
Ice particle in water

air

water layer



Ice particle in a water layer



Melting particle coated in a layer of water

Governing equations

underbody curve

$$F = F_u(X) + h(T) + (X - \beta)\theta(T),$$

conservation of mass and momentum

$$F_T + (uF)_X = 0,$$

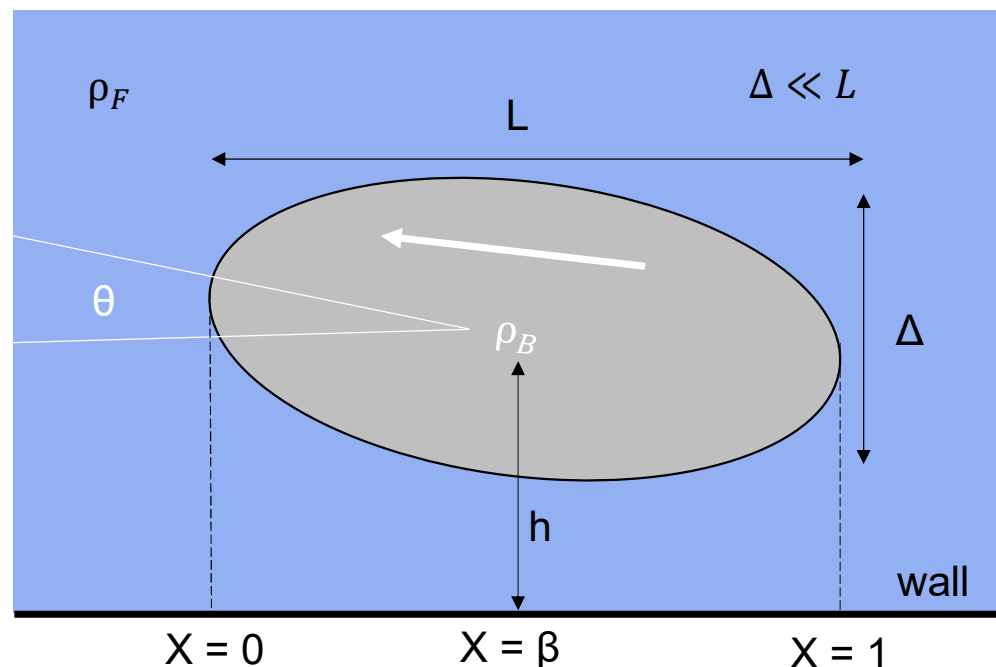
$$u_T + uu_X = -p_X, \quad 0 = -p_Y,$$

body motion equations

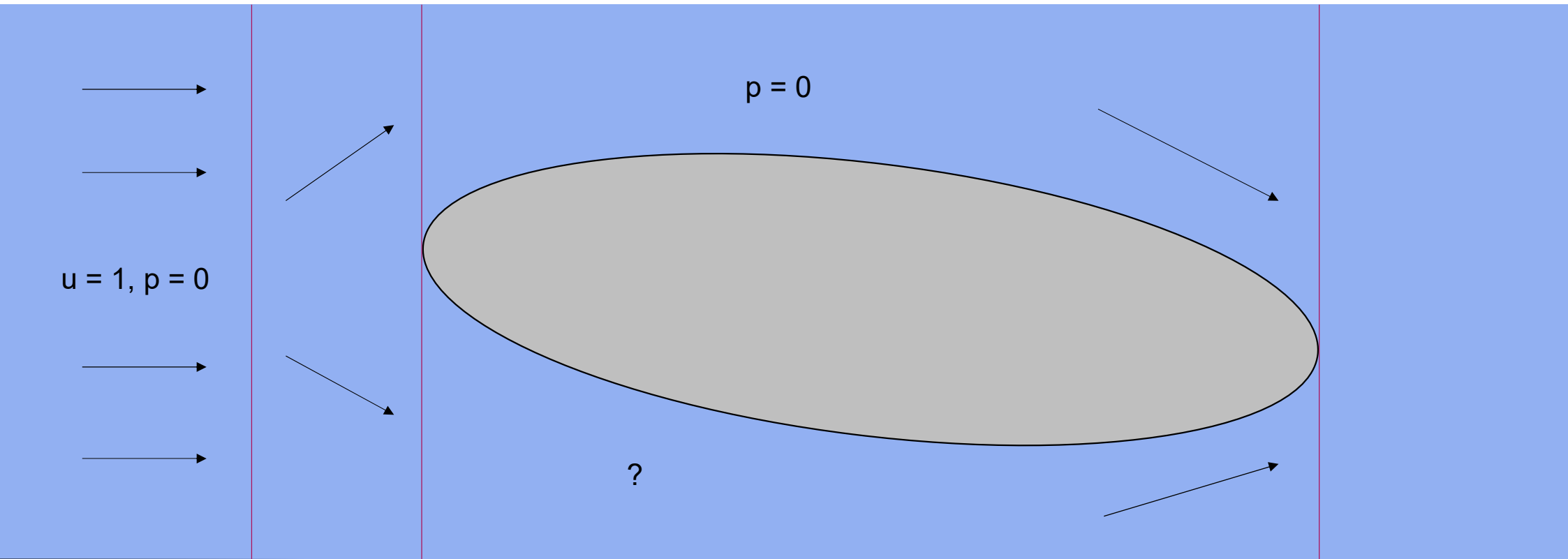
$$Mh_{TT} = \int_0^1 p \, dx, \quad I\theta_{TT} = \int_0^1 (x - \beta)p \, dx.$$

density ratio

$$\frac{\rho_B}{\rho_F} = O\left(\frac{L}{\Delta}\right)^2 \Rightarrow M, I \ll 1$$



Boundary conditions



$$\frac{1}{2}u^2 + p = \frac{1}{2} \text{ at } X = 0$$

$$p = 0 \text{ at } X = 1$$

Governing equations

To approach an $O(1)$ density ratio, assume:

$$M, I \ll 1$$

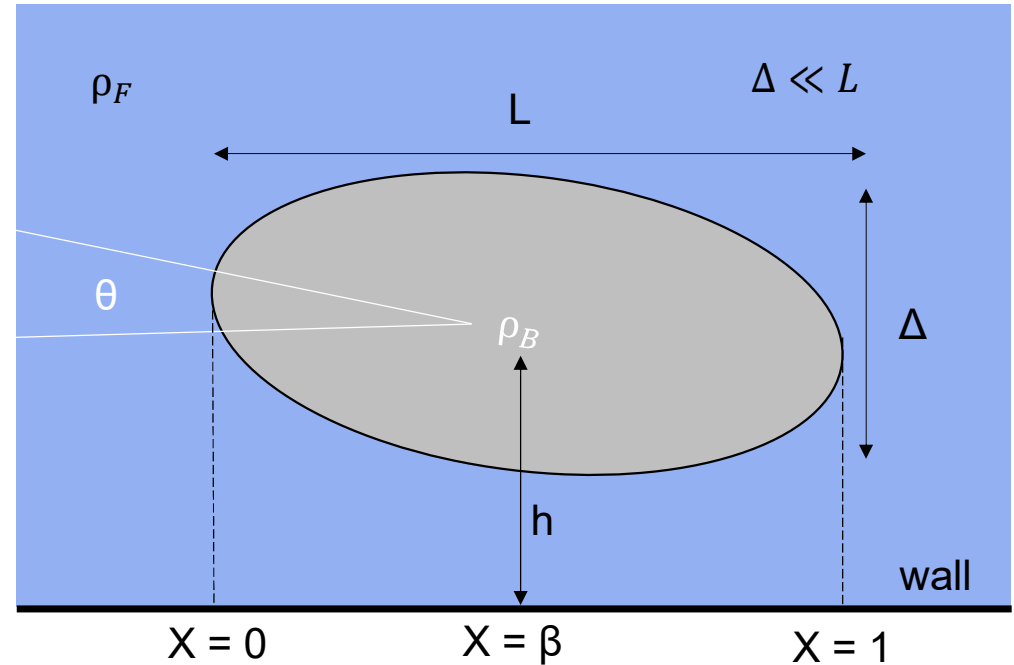
New governing equations:

$$F = F_u(X) + h(T) + (X - \beta)\theta(T),$$

$$F_T + (uF)_X = 0,$$

$$u_T + uu_X = -p_X, 0 = -p_Y$$

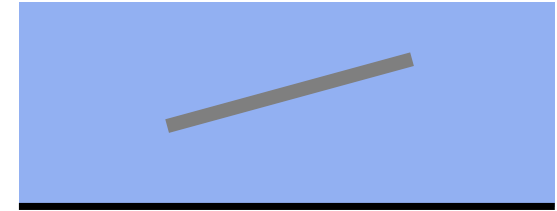
$$\int_0^1 p \, dx = \int_0^1 (x - \beta)p \, dx = 0.$$



Boundary conditions

$$\frac{1}{2}u^2 + p = \frac{1}{2} \text{ at } X = 0. \quad p = 0 \text{ at } X = 1.$$

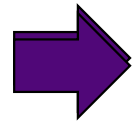
Linear analysis for flat plate



$$(F, h_C, \theta, u, p) = (1 + \delta F_1, 1 + \delta h_1, \delta \theta_1, 1 + \delta u_1, \delta p_1) + \dots, \quad (h_C = h - \beta \theta)$$

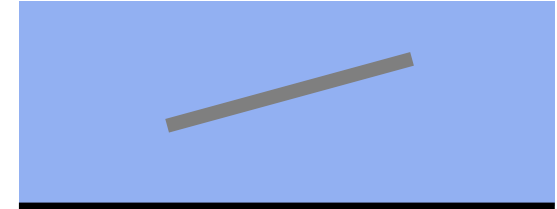
Linearised equations:

$$\begin{aligned} F_1 &= h_1(T) + X\theta_1(T), \\ F_{1T} + F_{1X} + u_{1X} &= 0, \\ u_{1T} + u_{1X} &= -p_{1X}, \\ \int_0^1 p_1 dx &= \int_0^1 xp_1 dx = 0, \\ u_1 &= -p_1 \text{ at } X = 0, \\ p_1 &= 0 \text{ at } X = 1. \end{aligned}$$



$$\begin{aligned} u_1 &= -(h'_1 + \theta_1)X - \theta'_1 X^2/2 - A_1(T), \\ p_1 &= (h''_1 + 2\theta'_1)X^2/2 + \theta''_1 X^3/6 + (A'_1 + h'_1 + \theta_1)X + A_1(T), \end{aligned}$$

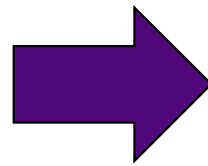
Linear analysis for a flat plate



$$(F, h_C, \theta, u, p) = (1 + \delta F_1, 1 + \delta h_1, \delta \theta_1, 1 + \delta u_1, \delta p_1) + \dots,$$

Linearised equations:

$$\begin{aligned} F_1 &= h_1(T) + X\theta_1(T), \\ F_{1T} + F_{1X} + u_{1X} &= 0, \\ u_{1T} + u_{1X} &= -p_{1X}, \\ \int_0^1 p_1 dx &= \int_0^1 xp_1 dx = 0, \\ u_1 &= -p_1 \text{ at } X = 0, \\ p_1 &= 0 \text{ at } X = 1. \end{aligned}$$



$$\begin{aligned} h_1''/2 + \theta_1''/6 + A_1' &= \mathcal{R}, \\ h_1''/6 + \theta_1''/24 + A_1'/2 &= \mathcal{S}, \\ h_1''/8 + \theta_1''/30 + A_1'/3 &= \mathcal{T}. \end{aligned}$$

$$\mathcal{R} = -\theta_1' - h_1' - \theta_1 - A_1,$$

$$\mathcal{S} = -\theta_1'/3 - h_1'/2 - \theta_1/2 - A_1,$$

$$\mathcal{T} = -\theta_1'/4 - h_1'/3 - \theta_1/3 - A_1/2.$$

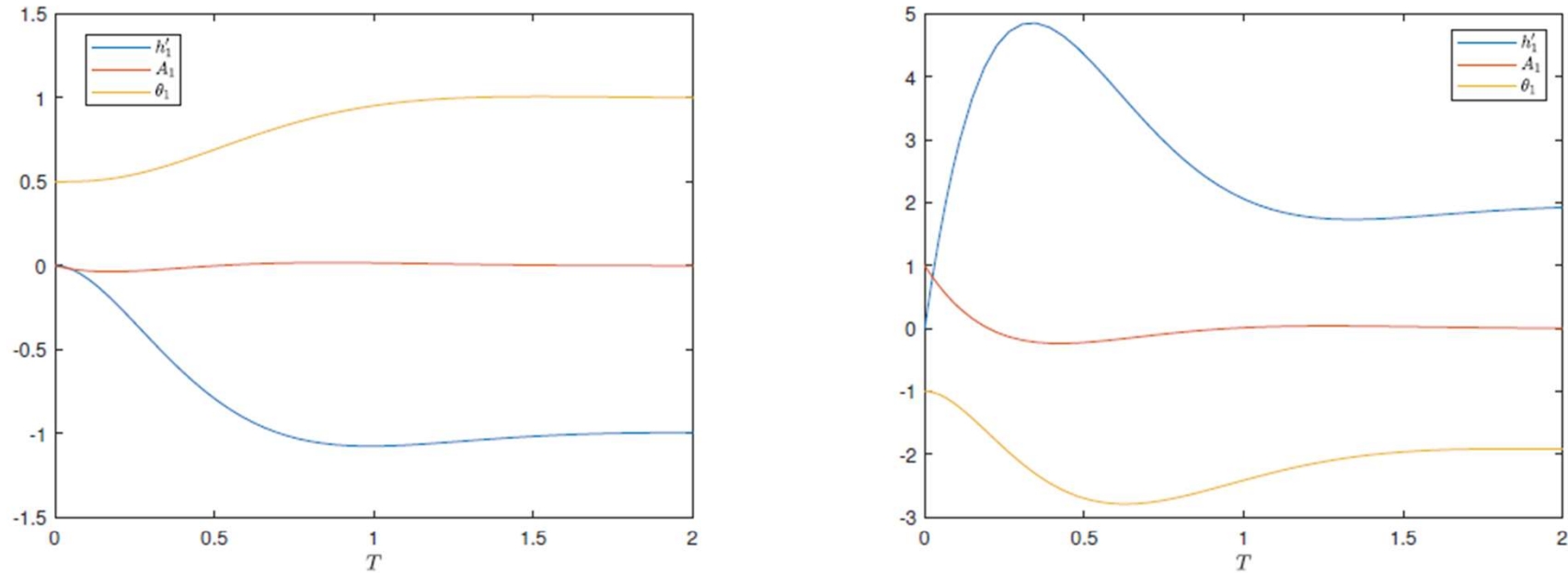


Figure 1: Results from solving the linearized system, showing convergence to two different steady states for the two different initial conditions, each with $h'_1 = -\theta_1 = \text{const}$ and $A_1 = 0$. The body may have either a negative velocity (left) or a positive velocity (right).

Full nonlinear system

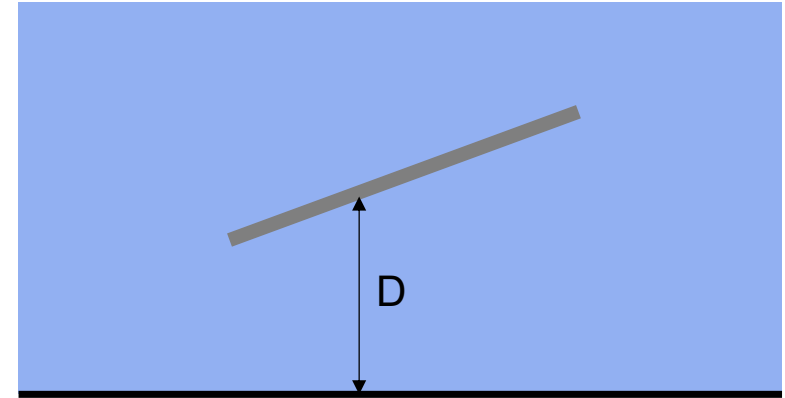
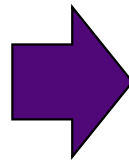
$$F_T + (uF)_X = 0,$$

$$u_T + uu_X = -p_X, 0 = -p_Y$$

$$\int_0^1 p \, dx = \int_0^1 (x - \beta)p \, dx = 0.$$

$$\frac{1}{2}u^2 + p = \frac{1}{2} \text{ at } X = 0.$$

$$p = 0 \text{ at } X = 1.$$



$$u = -\frac{[h'_C X + \frac{1}{2}\theta' X^2 + A(T)]}{D}, \text{ with } D = h_C + X\theta.$$

$$p = -\int_0^X u_T \, dx - \frac{1}{2}u^2 + \frac{1}{2}.$$

Full nonlinear system

$$\begin{aligned}\alpha_0 A' + \alpha_1 h_C'' + \frac{1}{2} \alpha_2 \theta'' &= e_4 - \frac{1}{2} + \beta_0, \\ \alpha_1 A' + \alpha_2 h_C'' + \frac{1}{2} \alpha_3 \theta'' &= e_4 - \frac{1}{2} b_4 + \beta_1, \\ \alpha_2 A' + \alpha_3 h_C'' + \frac{1}{2} \alpha_4 \theta'' &= e_4 - d_4 + \beta_2,\end{aligned}$$

$$\alpha_i = \sum_{j=0}^{i-1} \frac{h_C^j (-1)^j}{(i-j)\theta^{j+1}} + \frac{h_C^i (-1)^i}{\theta^i} \alpha_0, \quad i \geq 1,$$

$$\alpha_0 = \frac{1}{\theta} \log \left(1 + \frac{\theta}{h_C} \right).$$

$$\alpha_i = \int_0^1 \frac{x^i}{D} dx, \quad i = 0, 1, 2, 3, \dots$$

$$\beta_i = \int_0^1 \frac{x^i (h_C' x + \theta' x^2 / 2 + A) D'}{D^2} dx.$$

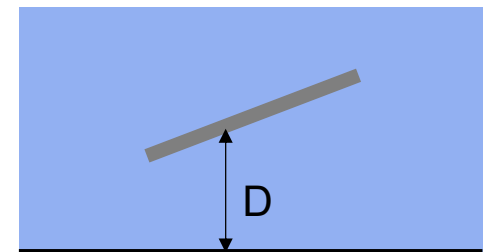
$$b_4 = \int_0^1 \frac{(h_C' x + \theta' x^2 / 2 + A)^2}{D^2} dx,$$

$$d_4 = \int_0^1 \frac{x (h_C' x + \theta' x^2 / 2 + A)^2}{D^2} dx,$$

$$e_4 = \frac{1}{2} \frac{(h_C' + \theta' / 2 + A)^2}{D_1^2},$$

$$D = h_C + X\theta$$

$$D_1 = h_C + \theta$$

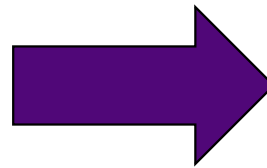


Leading edge collisions

In the limit of collision at the leading edge, i.e. $h_C \rightarrow 0$, the following asymptotic expansions apply:

$$\begin{aligned} h_C &= (t_0 - t)h_1 + (t_0 - t)\Lambda h_\lambda + \dots, \\ \theta &= \theta_0 + (t_0 - t)\theta_1 + (t_0 - t)\Lambda\theta_\lambda + \dots, \\ A &= \Lambda A_\lambda + (t_0 - t)A_1 + \dots, \end{aligned}$$

$$\Lambda = \frac{1}{\log(t_0 - t)},$$

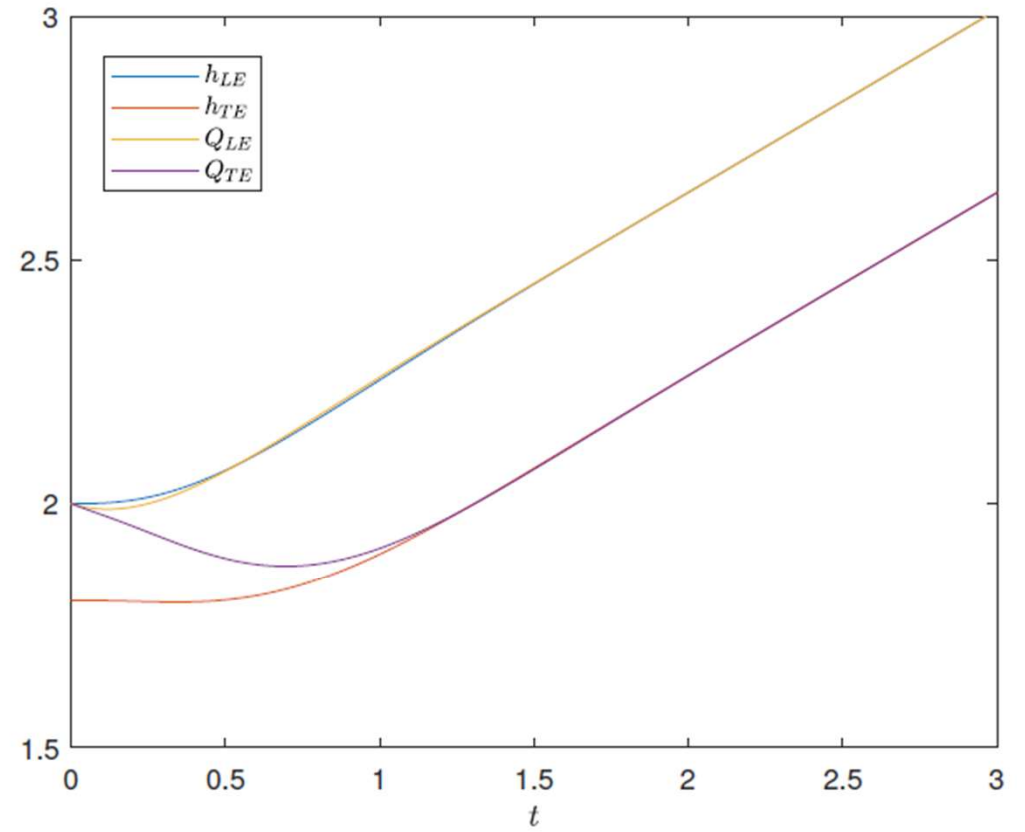
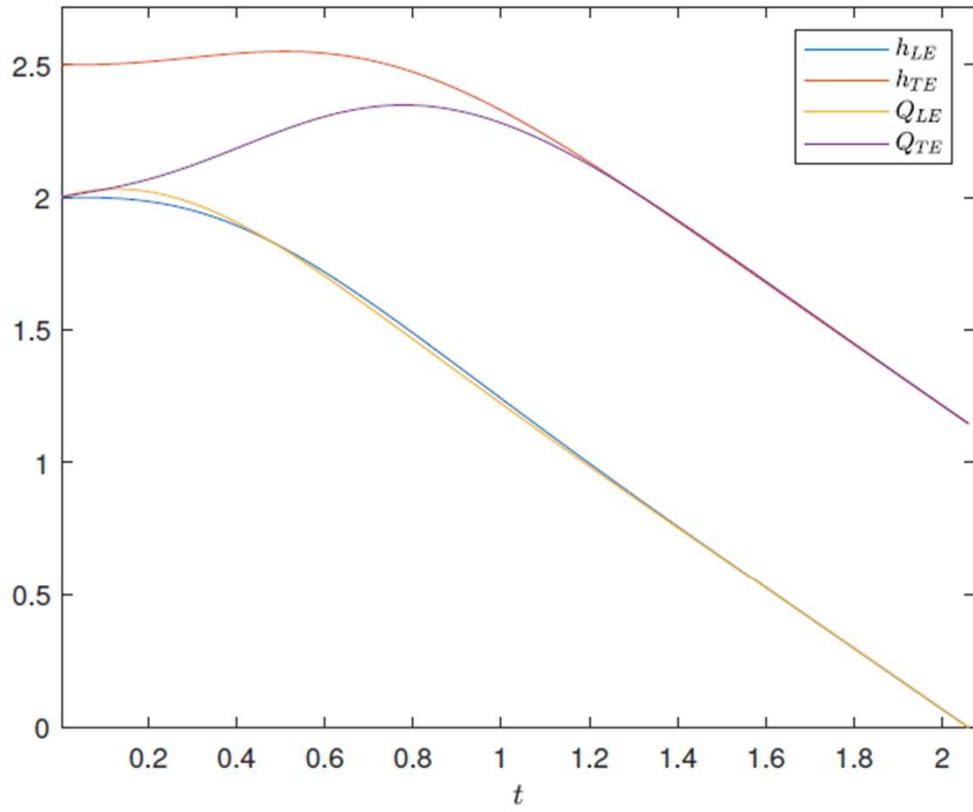


$$A_\lambda \left[A_\lambda + \theta_0 h_1 \left(1 + \frac{1}{6} \log \left(\frac{\theta_0}{h_1} \right) \right) \right] = 0,$$

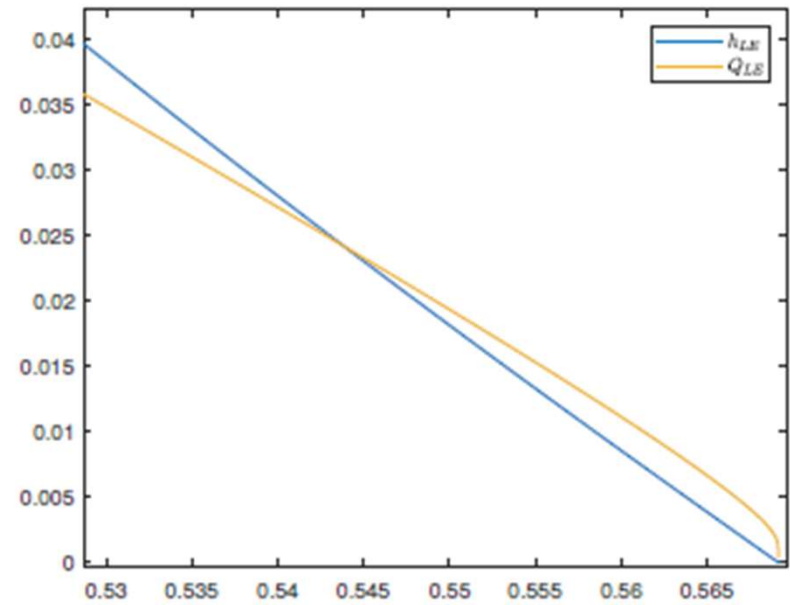
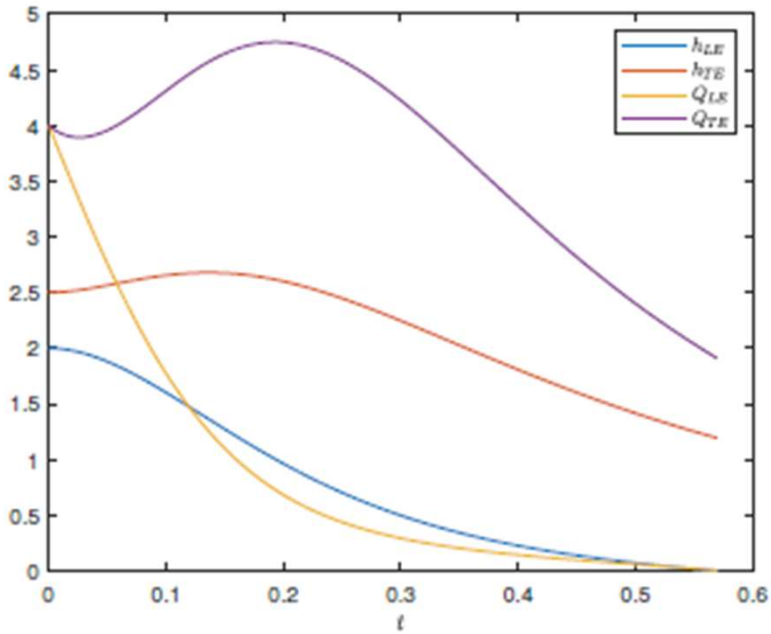
$$A_1 = -\frac{h_1^2}{\theta_0}.$$

$$\begin{aligned} \alpha_0 A' + \alpha_1 h_C'' + \frac{1}{2} \alpha_2 \theta'' &= e_4 - \frac{1}{2} + \beta_0, \\ \alpha_1 A' + \alpha_2 h_C'' + \frac{1}{2} \alpha_3 \theta'' &= e_4 - \frac{1}{2} b_4 + \beta_1, \\ \alpha_2 A' + \alpha_3 h_C'' + \frac{1}{2} \alpha_4 \theta'' &= e_4 - d_4 + \beta_2, \end{aligned}$$

$$\begin{aligned} \alpha_i &= \sum_{j=0}^{i-1} \frac{h_C^j (-1)^j}{(i-j)\theta^{j+1}} + \frac{h_C^i (-1)^i}{\theta^i} \alpha_0, \quad i \geq 1, \\ \alpha_0 &= \frac{1}{\theta} \log \left(1 + \frac{\theta}{h_C} \right). \end{aligned}$$



$$A_\lambda = 0$$



$$A_\lambda \neq 0$$

Summary

- Adapted model of ice particles in air to address ice particles in water
- Found solutions to linearized problem for flat plate
- Found solutions to full non-linear problem for flat plate
- Asymptotically described leading edge collisions

Thank you!