# COTS Components Radiation Test Activity and Results at MSSL part 2

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Abstract—following the paper [1] presenting the full radiation test result of ADC128S102 and DAC121S101 in NSREC2016 conference, this paper continues to report the test results of another three popular commercial off the shelf (COTS) devices AD8065, DG612 and EL7457 under the same EUCLID mission program at MSSL. The tests cover both total ionization dose (TID) and single event effect (SEE). The paper aims to share the test results with the community and provides valuable data for any relevant research.

Index Terms—COTS, SEE, TID, IC, MSSL, AD8065, DG612, EL7457

#### I. INTRODUCTION

MSSL has a long established history in making scientific instrument with major space agency in the world like ESA, NASA. Programs like Hindo instrument on Solar-B, PEACE instrument on Cluster are extremely successful with more than 10 years continuous service in orbit.

EUCLID is one of the latest ESA flagship program for mapping the dark universe. The Visible (VIS) instrument has equipped 36 CCDs driven by 12 chains of readout and power electronics. The design is highly modulated. This results in large quantity of fewer variants of EEE components. This in principle should help the procurement to lower the unit price. However the initial exchange of quotes with the supplier indicates the unit cost of the radhard ICs are still outstanding. Besides, some unique IC with excellent performance lacks the rad-hard version. This drives MSSL design team into the route of up-screening the COTS parts.

Following the report of ADC128S102 and DAC121S101 on NSREC2016 receiving widely popularity, this paper will present the full radiation test results of another three devices: AD8065[2], DG612[3] and EL7457[4].

AD8065 is a dual channel JFET input op-amp from Analogue Device. DG612 is a four channel analogue switch from Vishay. EL7457 is a level shift clock driver from Intersil. They play a key role in a CCD readout circuit design. In the up-screening program, we performed gamma dose test to access the total dose effect and threshold. Due to the funding limit and low risk of SEE to these analogue

The research was carried out at the Mullard Space Science Laboratory, University College London, as part of the EUCLID VIS flight instrument development project.

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devices, only SEL test was performed on DG612 and EL7457.

In the prior project for instrument UVIS as part of the NOMAD suite, flying on the ESA's ExoMars TGO spacecraft, AD8065 and DG612 are also used in the CCD readout circuit design. A similar up-screening program had been run on these two parts. But only TID was examined in that program. The results of both passed the 30krad test threshold, which enhances the confidence in pursuing the same route for EUCLID program.

EL7457 has been investigated for radiation performance at MSSL for Gaia mission. The prior results [5] show the TID tolerance could be as high as 50krad. SEL LET threshold is above 80 MeV.cm<sup>2</sup>.mg<sup>-1</sup>. The result reported in this paper shows a degradation of TID but similar good performance on SEL.

#### II. TEST SETUP

#### A. Test Facilities and Plan

The test facilities and plan for the three devices here are almost identical to the ones for the two devices reported in NSREC2016 [1]. Therefore, the detail is not repeated here. Just for quick reference, Table I shows the step, total dose and timing for the TID test. The exact dose rate varies a little from the plan in real test. Table II lists the source of heavy ions. To test beyond the 60 MeV.cm².mg⁻¹, the EUT can be tilted with respect to the beam axis. The test will stop when beam fluence reaches of  $1E10^7$  ions/cm².

TABLE I IRRADIATION EVALUATION TEST STEPS [6]

| STEPS                         | 1     | 2     | 3     | 4     | 5     | 6     | 7     |
|-------------------------------|-------|-------|-------|-------|-------|-------|-------|
| PROCESS                       | Irrad |
| Dose[krad(Si)]                | 2.5   | 2.5   | 5     | 10    | 10    | -     | ı     |
| Cumulative Dose<br>[krad(Si)] | 2.5   | 5     | 10    | 20    | 30    | -     | -     |
| Dose Rate<br>[rad(Si)/h]      | 360   | 360   | 360   | 360   | 360   | -     | 1     |
| Exposure Time (h)             | 6.9   | 6.9   | 13.9  | 27.8  | 27.8  | 24    | 168   |
| Temperature (°C)              | 25    | 25    | 25    | 25    | 25    | 25    | 85    |

TABLE II

ION BEAM SETTING AT RADEF [7]

| Ion                    | LET <sup>SRIM</sup> at surface<br>[MeV.cm <sup>2</sup> .mg <sup>-1</sup> ] | Range <sup>SRIM</sup><br>[µm] | Beam energy<br>[MeV] |
|------------------------|--|-------------------------------|----------------------|
| $^{20}\text{Ne}^{+6}$  | 3.63   | 146                           | 186                  |
| $^{40}Ar^{+12}$        | 10.2   | 118                           | 372                  |
| $^{56}\text{Fe}^{15+}$ | 18.5   | 97                            | 523                  |
| $^{82}Kr^{22+}$        | 32.1   | 94                            | 768                  |
| $^{131}Xe^{35+}$       | 60.0   | 89                            | 1217                 |

The data is quoted from the RADEF test report.

#### III. TEST RESULTS

#### A. AD8065

The AD8065 from ADI in Figure 1 is a single channel voltage feedback amplifiers with FET input. The device is developed in ADI's proprietary XFCB (eXtra Fast Complementary Bipolar) process. The particular part number under test is AD8065AR in an 8-ld SOIC package.

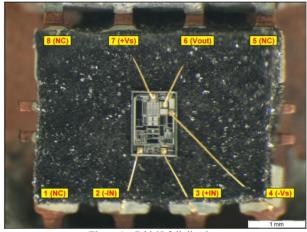


Figure 1 AD8065 full die view

# 1) TID

#### Setup

The electrical parameters and bias condition for the test is listed in Table III.

TABLE III
ELECTRICAL MEASUREMENTS TEST CONDITION AND LIMITS

| N° | SYMBOL | TEST                            | CONDITIONS                       | LIM   | ITS  | UNIT |
|----|--------|---------------------------------|----------------------------------|-------|------|------|
| N  | SYMBOL | TEST                            | (T <sub>AMB</sub> = 22±3°C)      | MIN.  | MAX. | UNII |
| 1  | VIO1   | Input Offset Voltage            | VCM=0V                           |       | 1.5  | mV   |
| 2  | liB    | Input Bias Current              | -                                | -     | 6    | pА   |
| 3  | lio    | Input Offset Current            |                                  |       | 10   | pА   |
| 4  | AVOL   | Open-Loop Gain                  | VO=±3V, RL=1kΩ                   | 100   |      | dB   |
| 5  | CMRR   | Common-mode<br>Rejection Ratio  | VCM=-1V to +1V                   | -85   |      | dB   |
| 6  | +VOUT  | Output Voltage                  | FI. 41.0                         | -4.88 |      | V    |
| 7  | 2,00.  | Swing                           | RL=1 kΩ                          | +4.90 |      | V    |
| 8  | ICC    | Quiescent Current               |                                  |       | 7.2  | mA   |
| 9  | PSRR   | Power Supply<br>Rejection Ratio |                                  | -85   |      | dB   |
| 10 | tr     | Output Rise Time                | VO=4V (step)<br>RL=No load, G=1. |       |      | s    |
| 11 | tf     | Output Fall Time                | VO=4V (step)<br>RL=No load, G=1. | -     |      | s    |
| 12 | VIO2   | Input Offset Voltage            | VCM=0V, VS=±12V,<br>RL=1kΩ       |       | 1.5  | mV   |

1. VS= $\pm$ 5V, RT=1k $\Omega$ , unless otherwise noted in table III.

The bias circuit is kept very simple and shown in Figure 2.

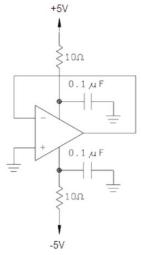


Figure 2 AD8065 TID test bias circuit

#### Result

The summary of results are presented in Table IV.

 $\label{thm:table_iv} TABLE~IV$  Summary of total ionized dose test of AD8065 in 2015

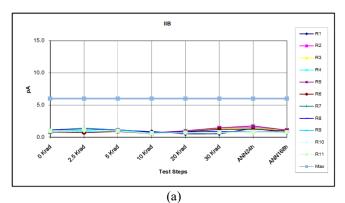
|                           | 0 krad | 2.5 krad | 5 krad | 10 krad | 20 krad | 30 krad | ANN24h | ANN168h |
|---------------------------|--------|----------|--------|---------|---------|---------|--------|---------|
| V <sub>IO</sub> 1         | PASS   | PASS     | PASS   | PASS    | PASS    | PASS    | PASS   | PASS    |
| IB                        | PASS   | PASS     | PASS   | PASS    | PASS    | PASS    | PASS   | PASS    |
| I <sub>IO</sub>           | PASS   | PASS     | PASS   | PASS    | PASS    | PASS    | PASS   | PASS    |
| AVOL                      | PASS   | PASS     | PASS   | PASS    | PASS    | PASS    | PASS   | PASS    |
| CMRR                      | PASS   | PASS     | PASS   | PASS    | PASS    | PASS    | PASS   | PASS    |
| ±V <sub>OUT</sub>         | PASS   | PASS     | PASS   | PASS    | PASS    | PASS    | PASS   | PASS    |
| Icc                       | PASS   | PASS     | PASS   | PASS    | PASS    | PASS    | PASS   | PASS    |
| PSRR                      | PASS   | PASS     | PASS   | PASS    | PASS    | PASS    | PASS   | PASS    |
| t <sub>r</sub>            | PASS   | PASS     | PASS   | PASS    | PASS    | PASS    | PASS   | PASS    |
| te                        | PASS   | PASS     | PASS   | PASS    | PASS    | PASS    | PASS   | PASS    |
| V <sub>IO</sub> 2         | PASS   | PASS     | PASS   | PASS    | PASS    | PASS    | PASS   | PASS    |
| INPUT<br>VOLTAGE<br>NOISE | PASS   | PASS     | PASS   | PASS    | PASS    | PASS    | PASS   | PASS    |

Comparing to the test result from UVIS program [8] presented in Table V, the performance is very consistent.

 $TABLE\ V$  Summary of total ionized dose test of AD8065 in 2014

|                   | 0KRAD | 2.5KRAD | 5KRAD | 10KRAD | 20KRAD | 30KRAD | ANN24h | ANN168h |
|-------------------|-------|---------|-------|--------|--------|--------|--------|---------|
| V <sub>IO</sub> 1 | PASS  | PASS    | PASS  | PASS   | PASS   | PASS   | PASS   | PASS    |
| I <sub>IIB</sub>  | PASS  | PASS    | PASS  | PASS   | PASS   | PASS   | PASS   | PASS    |
| I <sub>IO</sub>   | PASS  | PASS    | PASS  | PASS   | PASS   | PASS   | PASS   | PASS    |
| A <sub>VOL</sub>  | PASS  | PASS    | PASS  | PASS   | PASS   | PASS   | PASS   | PASS    |
| CMRR              | PASS  | PASS    | PASS  | PASS   | PASS   | PASS   | PASS   | PASS    |
| $\pm V_{OUT}$     | PASS  | PASS    | PASS  | PASS   | PASS   | PASS   | PASS   | PASS    |
| Icc               | PASS  | PASS    | PASS  | PASS   | PASS   | PASS   | PASS   | PASS    |
| <b>PSRR</b>       | PASS  | PASS    | PASS  | PASS   | PASS   | PASS   | PASS   | PASS    |
| t <sub>r</sub>    | PASS  | PASS    | PASS  | PASS   | PASS   | PASS   | PASS   | PASS    |
| t <sub>f</sub>    | PASS  | PASS    | PASS  | PASS   | PASS   | PASS   | PASS   | PASS    |
| V <sub>IO</sub> 2 | PASS  | PASS    | PASS  | PASS   | PASS   | PASS   | PASS   | PASS    |

The detail measurement data shows the device's parameter is well within the specification with large margin. One of the key parameters for the CCD readout circuit application is IIB. Figure 3 shows this parameter is sensitive to the gamma dose, but for the test up to 30krad, it is well within the specification.



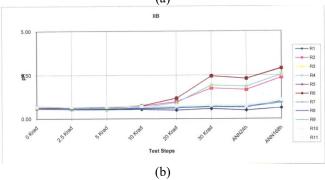


Figure 3 (a) is from test under EULICD program, (b) is from test under UVIS program. Note the y-axis scale is different so that the curve looks very different.

#### **Summary**

The value of all the electric parameters under monitor remains unchanged or very little move only, when the sample is subject to radiation at 198.43rad(Si)/h up to total dose of 30krad. The device shows superb immunity to radiation damage. Based on the current result, it is confident to state the device has a good potential to survive even higher dose.

# B. DG612

DG612 in Figure 4 is a high-speed, low-glitch quad channel analog switch from Vishay Siliconix. The device is built on the Vishay's D/CMOS process, which combines n-channel DMOS switching FETs with low-power CMOS control logic and drivers. An epitaxial layer prevents latchup. The part number under test is DG612DY in SOIC-16 package.

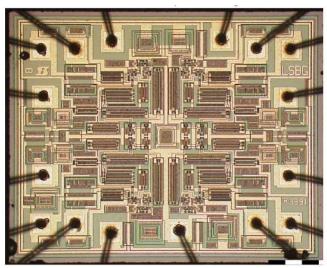


Figure 4 DG612 full die view

## 1) TID

# <u>Setup</u>

The electrical parameters and bias condition for the test is listed in Table VI.

#### TABLE VI

ELECTRICAL MEASUREMENTS TEST CONDITION AND LIMITS

| N° | SYMBOL  | TEST                           | CONDITIONS                          | LIN       | IITS | UNIT |
|----|---------|--------------------------------|-------------------------------------|-----------|------|------|
| N  | STWIBOL | 1531                           | (T <sub>AMB</sub> = 22±3°C)         | MIN.      | MAX. | UNII |
| 1  | RDS(ON) | Drain-to-source ON resistance. | IS=-1mA, VD=0V                      |           | 45   | Ω    |
| 2  | IS(OFF) | Source Off Leakage             | VS=0V, VD=10V                       | -<br>0.25 | 0.25 | nA   |
| 3  | ID(OFF) | Drain Off Leakage<br>Current   | VS=10V, VD=0V                       | -<br>0.25 | 0.25 | nA   |
| 4  | ID(ON)  | Switch On Leakage<br>Current   | VS=VD=0V                            | -0.4      | 0.4  | nA   |
| 5  | lin     | Input Current                  |                                     | -1        | 1    | μA   |
| 6  | +       | Positive supply current        | VIN=0V or 5V                        | -         | 1    | μA   |
| 7  | l-      | Negative supply<br>current     | VIN=0V or 5V                        | -1        |      | μА   |
| 8  | ton     | Turn-On Time                   | RL=300Ω, CL=75pF,<br>VS=±2V. Note 2 |           | 35   | ns   |
| 9  | tOFF    | Turn-Off Time                  | RL=300Ω, CL=75pF,<br>VS=±2V. Note 2 |           | 25   | ns   |
| 10 | Q       | Charge injection               | CL=1nF, VS=0V. Note                 |           |      | рС   |
| 11 | XTALK   | Crosstalk                      | RIN=10Ω, RL=50Ω,<br>f=5MHz. Note 3  |           |      | dB   |

1. V+=15 V; V-=-3 V; VL=5 V; VIN=4 V, 1 V, unless otherwise noted in in Table IV.

The bias circuit shown in Figure 5 is also kept simple and close to the real application.

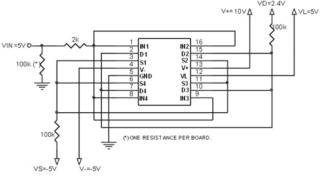


Figure 5 DG612 TID test bias circuit

#### Results

The summary of the result is listed in Table VII.

TABLE VII

SUMMARY OF TOTAL IONIZED DOSE TEST OF DG612 IN 2015

|                     | 0 krad | 10 krad | 15 krad | 20 krad | 22.5 krad | 25 krad | 35 krad | ANN24h | ANN168h |
|---------------------|--------|---------|---------|---------|-----------|---------|---------|--------|---------|
| R <sub>DS(ON)</sub> | PASS   | PASS    | PASS    | PASS    | PASS      | PASS    | PASS    | PASS   | PASS    |
| I <sub>S(OFF)</sub> | PASS   | PASS    | NOTE 1  | NOTE 1  | NOTE 1    | NOTE 1  | NOTE 1  | NOTE 1 | PASS    |
| I <sub>D(OFF)</sub> | PASS   | PASS    | NOTE 1  | NOTE 1  | NOTE 1    | NOTE 1  | NOTE 1  | NOTE 1 | PASS    |
| I <sub>D(ON)</sub>  | PASS   | PASS    | PASS    | PASS    | PASS      | PASS    | PASS    | PASS   | PASS    |
| I <sub>IN</sub>     | PASS   | PASS    | PASS    | PASS    | PASS      | PASS    | PASS    | PASS   | PASS    |
| I+                  | PASS   | NOTE 1  | NOTE 1  | NOTE 1  | NOTE 1    | NOTE 1  | NOTE 1  | NOTE 1 | PASS    |
| L.                  | PASS   | NOTE 1  | NOTE 1  | NOTE 1  | NOTE 1    | NOTE 1  | NOTE 1  | NOTE 1 | PASS    |
| ton                 | PASS   | PASS    | PASS    | PASS    | PASS      | PASS    | PASS    | PASS   | PASS    |
| t <sub>OFF</sub>    | PASS   | PASS    | PASS    | PASS    | PASS      | PASS    | PASS    | PASS   | PASS    |
| Q                   | PASS   | PASS    | PASS    | PASS    | PASS      | PASS    | PASS    | PASS   | PASS    |
| XTALK               | PASS   | PASS    | PASS    | PASS    | PASS      | PASS    | PASS    | PASS   | PASS    |

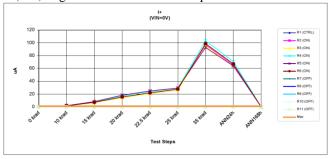
Comparing to the result from UVIS program [9] in Table VIII, the performance is stable.

# TABLE VIII SUMMARY OF TOTAL IONIZED DOSE TEST OF DG612 IN 2014

|                     | 0 KRAD | 2.5 KRAD | 5 KRAD | 10 KRAD | 20 KRAD | 35 KRAD | ANN24h | ANN168h |
|---------------------|--------|----------|--------|---------|---------|---------|--------|---------|
| R <sub>DS(ON)</sub> | PASS   | PASS     | PASS   | PASS    | PASS    | PASS    | PASS   | PASS    |
| I <sub>S(OFF)</sub> | PASS   | PASS     | PASS   | PASS    | NOTE 1  | NOTE 1  | NOTE 1 | PASS    |
| I <sub>D(OFF)</sub> | PASS   | PASS     | PASS   | PASS    | NOTE 1  | NOTE 1  | NOTE 1 | PASS    |
| I <sub>D(ON)</sub>  | PASS   | PASS     | PASS   | PASS    | PASS    | PASS    | PASS   | PASS    |
| I <sub>IN</sub>     | PASS   | PASS     | PASS   | PASS    | PASS    | PASS    | PASS   | PASS    |
| I+                  | PASS   | PASS     | PASS   | NOTE 1  | NOTE 1  | NOTE 1  | NOTE 1 | PASS    |
| I.                  | PASS   | PASS     | PASS   | NOTE 1  | NOTE 1  | NOTE 1  | NOTE 1 | PASS    |
| ton                 | PASS   | PASS     | PASS   | PASS    | PASS    | PASS    | PASS   | PASS    |
| t <sub>OFF</sub>    | PASS   | PASS     | PASS   | PASS    | PASS    | PASS    | PASS   | PASS    |
| Q                   | PASS   | PASS     | PASS   | PASS    | PASS    | PASS    | PASS   | PASS    |
| XTALK               | PASS   | PASS     | PASS   | PASS    | PASS    | PASS    | PASS   | PASS    |

Note 1: parameter out of limits.

The parameter sensitive to the radiation is  $I_+$ ,  $I_-$ ,  $I_S(OFF)$  and ID(OFF). Figure 6 shows the result of parameter  $I_+$ .



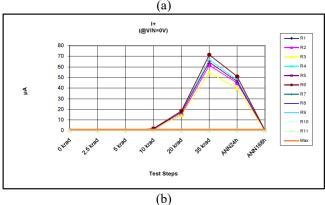


Figure 6 (a) is from test under EULICD program, (b) is from test test under UVIS program. The dose test stepping is arranged differently in the two tests, so the table and graph looks slightly different. But from both tests, the parameter was found to be out of limit at 10krad check point.

Note the parameter I<sub>+</sub> and I<sub>-</sub> are within the limit when they are tested at condition VIN=5V but out of limit at condition VIN=0V.

#### Summary:

In the test from this report, the sample is exposed to a real dose rate at 213.77rad(Si)/h. Test stops at 35krad. It is found four electric parameters under monitoring are sensitive to the radiation. They are: I+, I-, IS(OFF) and ID(OFF). The two supply currents (I+, I-) start to be out of limit ( $\pm 1\mu A$  at room temperature) between 0 and 10krad. The maximum current recorded is ~100μA at 35krad. It looks like the current will increase exponentially with the accumulated dose. The device remains functioning despite the increasing supply current. So it is considered acceptable. The leakage currents (IS(OFF), ID(OFF)) start to increase out of spec between 10 and 15krad. The max is recorded at 29.5mA at 35krad. This is higher than the possible switch on Is and ID, as limited by the resistor in series in the test circuit. This suggests that there is parasitic short-path created by the accumulated dose. All the four parameters recover to initial value after 168h annealing. For unbiased samples, none of the four parameters have changed.

#### 2) SEE

#### <u>Setup</u>

Bias circuit in Figure 7 is a copy of real application.

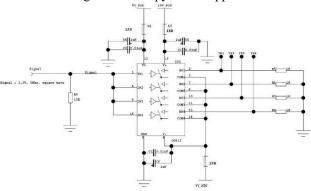


Figure 7 DG612 SEL test bias circuit. Test configuration is DUT\_VL = +5V, DUT\_V+ = +10V, DUT\_V- = -5V, INPUTS = Square wave  $\pm 3.3$ V at 5MHz.

#### Results

The summary of the result is listed in Table IX.

SUMMARY OF SEL TEST OF DG612 IN 2015

| Facility | medium | run_number | Facility_run_number | board_id | temperature | dut_partnumber | test_mode | uol | ТЕТ | roll | tilt | Eff. LET | run_duration | entered_fluence | TES. |
|----------|--------|------------|---------------------|----------|-------------|----------------|-----------|-----|-----|------|------|----------|--------------|-----------------|------|
| RADEF    | vacuum | 1          | 70                  | 1        | room        | 1,2            | SEL       | Хe  | 60  | 0    | 0    | 60.0     | 685          | 1.00E+07        | 0    |
| RADEF    | vacuum | 2          | 71                  | 1        | room        | 3,4            | SEL       | Хe  | 60  | 0    | 0    | 60.0     | 264          | 1.00E+07        | 0    |
| RADEF    | vacuum | 3          | 72                  | 1        | room        | 1,2            | SEL       | Хe  | 60  | 0    | 53   | 99.7     | 436          | 1.00E+07        | 0    |
| RADEF    | vacuum | 4          | 73                  | 1        | room        | 3,4            | SEL       | Хe  | 60  | 0    | 53   | 99.7     | 544          | 1.00E+07        | 0    |
| RADEF    | vacuum | 5          | 74                  | 1        | room        | 1,2            | SEL       | Xe  | 60  | 0    | 60   | 120.0    | 543          | 5.91E+06        | 0    |
| RADEF    | vacuum | 6          | 75                  | 1        | room        | 1,2            | SEL       | Xe  | 60  | 0    | 60   | 120.0    | 586          | 5.72E+06        | 0    |
| RADEF    | vacuum | 7          | 76                  | 1        | room        | 3,4            | SEL       | Xe  | 60  | 0    | 60   | 120.0    | 1450         | 1.00E+07        | 0    |

#### **Summary**

Four samples are tested with two samples at a time. The SEL detection threshold is set at 100mA for VL, 100mA for V+ and -100mA for V-. The test starts with Xenon without tilt (LET =  $60 \text{ MeV.cm}^2\text{.mg}^{-1}$ ), no SEL event was detected upto beam fluences of  $1E10^7$  ions/cm². Then test continues with higher LET by tilting the Xenon source. At effective LET of  $100 \text{ and } 120 \text{ MeV.cm}^2\text{.mg}^{-1}$ , still no SEL event was captured.

We can conclude the device is latchup free up 120MeV. This may be directly resulted from the design of an epitaxial layer.

#### C. EL7457

EL7457 in Figure 7 is a high-speed, non-inverting, quad CMOS driver, manufactured by Intersil. It is likely to be built on SOI technology as most INTERSIL devices are using this process. This device has been tested for TID and SEL in a radiation study for GAIA project in 2007[10].

Its rad-hard version is ISL7457SRH. ESA has carried out independent SEE test on it in 2014[11].

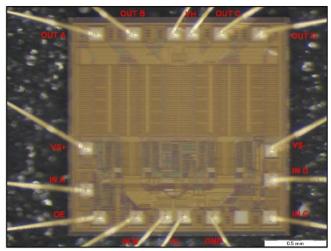


Figure 7 EL7457 full die view

## 1) TID

#### Setup

The electrical parameters and bias condition for the test is listed in Table X.

# TABLE X ELECTRICAL MEASUREMENTS TEST CONDITION AND LIMITS

| N° | SYMBOL               | TEST                                      | CONDITIONS                         | LIM  | IITS | UNIT |
|----|----------------------|---|------------------------------------|------|------|------|
| N. | STWIBUL              | TEST                                      | (T <sub>AMB</sub> =22±3°C)         | MIN. | MAX. | UNII |
| 1  |                      | Logic "1" Input Current<br>(Vs = ±5V)     | VIH = 5V                           |      | 10   | pA   |
| 2  | I <sub>IH</sub>      | Logic "1" Input Current<br>(Vs = +1510V)  | VIH = 5V                           | 1    | 10   | pA   |
| 3  | . I <sub>L</sub>     | Logic "0" Input Current<br>(Vs = ±5V)     | VIL = OV                           | 1    | 10   | pA   |
| 4  | IL.                  | Logic "0" Input Current<br>(Vs = +1510V)  | VIL= OV                            | -    | 10   | pA   |
| 5  | R <sub>OH</sub>      | ON Resistance VH to OUTx (Vs = ±5V)       | lour = -100mA                      | -    | 6    | Ω    |
| 6  | NOH                  | ON Resistance VH to OUTx (Vs = +15/0V)    | lour = -100mA                      | -    | 5    | Ω    |
| 7  | R <sub>OL</sub>      | ON Resistance VL to OUTx (Vs = ±5V)       | lour = +100mA                      | -    | 6    | Ω    |
| 8  | NOL                  | ON Resistance VL to<br>OUTx (Vs = +15/0V) | lour = +100mA                      | -    | 5    | Ω    |
| 9  |                      | Output Leakage Current<br>(Vs = ±5V)      | VH = VS+, VL = VS-                 | ı    | 10   | pA   |
| 10 | I <sub>LEAK</sub>    | Output Leakage Current<br>(Vs = +15/0V)   | VH = Vs+, VL = Vs_                 | ,    | 10   | pA   |
| 11 |                      | Power Supply Current<br>(Vs = ±5V)        | Inputs = Vs+                       | -    | 1.5  | mA   |
| 12 | · I <sub>s</sub>     | Power Supply Current<br>(Vs = +15/0V)     | Inputs = Vs+                       | -    | 2    | mA   |
| 13 | -                    | Rise time<br>(Vs = ±5V)                   | INx = OV to 4.5V step,<br>CL = 1nF | -    | 40   | ns   |
| 14 | T <sub>r</sub>       | Rise time<br>(Vs = +15/0V)                | INx = OV to 5V step,<br>CL = 1nF   | -    | 20   | ns   |
| 15 | т                    | Fall time<br>(Vs = ±5V)                   | INx = 4.5V to OV step,<br>CL = 1nF | 1    | 30   | ns   |
| 16 | T <sub>f</sub>       | Fall time<br>(Vs = +15/0V)                | INx = 5V to OV step,<br>CL = 1nF   | -    | 20   | ns   |
| 17 | т                    | Turn-on delay time<br>(Vs = ±5V)          | INx = OV to 4.5V step,<br>CL = 1nF | -    | 30   | ns   |
| 18 | T <sub>D+</sub>      | Turn-on delay time<br>(Vs = +15/0V)       | INx = OV to 5V step,<br>CL = 1nF   | 1    | 20   | ns   |
| 19 |                      | Turn-off delay time<br>(Vs = ±5V)         | INx = 4.5V to OV step,<br>CL = 1nF | -    | 40   | ns   |
| 20 | T <sub>D-</sub>      | Turn-off delay time<br>(Vs = +15/0V)      | INx = 5V to OV step,<br>CL = 1nF   | -    | 20   | ns   |
| 21 | _                    | Enable delay time<br>(Vs = ±5V)           | INx = OV to 4.5V step,<br>RL = 1k0 | -    | 35   | ns   |
| 22 | T <sub>ENABLE</sub>  | Enable delay time<br>(Vs = +15/0V)        | INx = OV to 5V step,<br>RL = 1k0   | -    | 25   | Ns   |
| 21 | <b>-</b>             | Disable delay time<br>(Vs = ±5V)          | INx = OV to 4.5V step,<br>RL = 1k0 | -    | 35   | ns   |
| 22 | T <sub>DISABLE</sub> | Disable delay time<br>(Vs = +15/0V)       | INx = OV to 5V step,<br>RL = 1k0   | -    | 25   | Ns   |

#### Results

# The summary of the result is listed in Table XI TABLE XI

SUMMARY OF TOTAL IONIZED DOSE TEST OF EL7457

|  |     |     | 0 krad | 2.5 krad | 5 krad    | 10 krad  | 20 krad | 30 krad | Ann24h | Ann168 |
|--|-----|-----|--------|----------|-----------|----------|---------|---------|--------|--------|
|  |     |     |        |          | - INPUT : | SECTION  | _       |         |        |        |
|  |     | ON  | PASS   | PASS     | PASS      | PASS     | PASS    | PASS    | PASS   | PASS   |
|  | ±5V | OFF | PASS   | PASS     | PASS      | PASS     | PASS    | PASS    | PASS   | PASS   |
| I <sub>IH</sub>  |     | ON  | PASS   | PASS     | PASS      | PASS     | PASS    | NOTE 2  | NOTE 2 | NOTE 2 |
|  | 15V | OFF | PASS   | PASS     | PASS      | PASS     | PASS    | PASS    | PASS   | PASS   |
| I <sub>II</sub> ,  I <sub>I,EAX</sub> ROH  ROL  I <sub>S*</sub> I <sub>S</sub> t <sub>R</sub> t <sub>O</sub> |     | ON  | PASS   | PASS     | PASS      | PASS     | PASS    | PASS    | PASS   | PASS   |
|  | ±5V | OFF | PASS   | PASS     | PASS      | PASS     | PASS    | PASS    | PASS   | PASS   |
| I <sub>IL</sub>  | -   | ON  | PASS   | PASS     | PASS      | PASS     | PASS    | PASS    | PASS   | PASS   |
|  | 15V | OFF | PASS   | PASS     | PASS      | PASS     | PASS    | PASS    | PASS   | PASS   |
|  |     |     |        |          |           | SECTION  |         |         |        |        |
|  |     | ON  | PASS   | PASS     | PASS      | NOTE 2   | NOTE 2  | NOTE 2  | NOTE 2 | NOTE : |
|  | ±5V | OFF | PASS   | PASS     | PASS      | PASS     | PASS    | PASS    | PASS   | PASS   |
| LEAK   |     | ON  | PASS   | PASS     | PASS      | PASS     | PASS    | NOTE 2  | NOTE 2 | NOTE : |
|  | 15V | OFF | PASS   | PASS     | PASS      | PASS     | PASS    | PASS    | PASS   | PASS   |
|  | _   | ON  | PASS   | PASS     | PASS      | PASS     | PASS    | NOTE 1  | NOTE 1 | PASS   |
| _  | ±5V | OFF | PASS   | PASS     | PASS      | PASS     | PASS    | PASS    | PASS   | PASS   |
| RoH  | L   | ON  | PASS   | PASS     | PASS      | PASS     | PASS    | NOTE 1  | PASS   | PASS   |
|  | 15V | OFF | PASS   | PASS     | PASS      | PASS     | PASS    | PASS    | PASS   | PASS   |
|  |     | ON  | PASS   | PASS     | PASS      | NOTE 2   | NOTE 2  | NOTE 2  | NOTE 2 | NOTE   |
| _  | ±5V | OFF | PASS   | PASS     | PASS      | PASS     | PASS    | PASS    | PASS   | PASS   |
| ROL  | 15V | ON  | PASS   | PASS     | PASS      | PASS     | NOTE 2  | NOTE 2  | NOTE 2 | NOTE   |
|  | 150 | OFF | PASS   | PASS     | PASS      | PASS     | NOTE 2  | NOTE 2  | NOTE 2 | NOTE   |
|  |     |     |        | - POI    | WER SUP   | PLY SEC  | TION -  |         |        |        |
|  |     | ON  | PASS   | PASS     | PASS      | PASS     | PASS    | NOTE 1  | NOTE 1 | NOTE   |
| ls+  | ±5V | OFF | PASS   | PASS     | PASS      | PASS     | PASS    | PASS    | PASS   | PASS   |
|  |     | ON  | PASS   | PASS     | PASS      | PASS     | PASS    | NOTE 1  | NOTE 1 | NOTE   |
| s.   | ±5V | OFF | PASS   | PASS     | PASS      | PASS     | PASS    | PASS    | PASS   | PASS   |
|  |     | ON  | PASS   | PASS     | PASS      | PASS     | PASS    | NOTE 1  | NOTE 1 | NOTE   |
| s  | 15V | OFF | PASS   | PASS     | PASS      | PASS     | PASS    | PASS    | PASS   | PASS   |
|  |     |     | - SI   | VITCHING | CHARAG    | CTERISTI | CS SECT | ION -   |        |        |
|  |     | ON  | PASS   | PASS     | PASS      | PASS     | PASS    | PASS    | PASS   | PASS   |
|  | ±5V | OFF | PASS   | PASS     | PASS      | PASS     | PASS    | PASS    | PASS   | PASS   |
| t <sub>R</sub>   |     | ON  | PASS   | PASS     | PASS      | PASS     | PASS    | PASS    | PASS   | PASS   |
|  | 15V | OFF | PASS   | PASS     | PASS      | PASS     | PASS    | PASS    | PASS   | PASS   |
|  |     | ON  | PASS   | PASS     | PASS      | PASS     | PASS    | PASS    | PASS   | PASS   |
|  | ±5V | OFF | PASS   | PASS     | PASS      | PASS     | PASS    | PASS    | PASS   | PASS   |
| t <sub>F</sub>   |     | ON  | PASS   | PASS     | PASS      | PASS     | PASS    | PASS    | PASS   | PASS   |
|  | 15V | OFF | PASS   | PASS     | PASS      | PASS     | PASS    | PASS    | PASS   | PASS   |
|  |     | ON  | PASS   | PASS     | PASS      | NOTE 2   | NOTE 2  | NOTE 2  | NOTE 2 | NOTE   |
|  | ±5V | OFF | PASS   | PASS     | PASS      | PASS     | PASS    | PASS    | PASS   | PASS   |
| t <sub>D+</sub>  |     | ON  | PASS   | PASS     | PASS      | PASS     | PASS    | NOTE 2  | NOTE 2 | NOTE   |
|  | 15V | OFF | PASS   | PASS     | PASS      | PASS     | PASS    | PASS    | PASS   | PASS   |
|  | ±5V | ON  | PASS   | PASS     | PASS      | PASS     | PASS    | NOTE 2  | PASS   | PASS   |
|  | ±5V | OFF | PASS   | PASS     | PASS      | PASS     | PASS    | PASS    | PASS   | PASS   |
| τ <sub>D</sub> .   | 15V | ON  | NOTE 3 | NOTE 3   | NOTE 3    | NOTE 3   | NOTE 3  | NOTE 2  | NOTE 2 | NOTE   |
|  | 15V | OFF | NOTE 3 | NOTE 3   | NOTE 3    | NOTE 3   | NOTE 3  | NOTE 3  | NOTE 3 | NOTE 3 |
|  | ±5V | ON  | PASS   | PASS     | PASS      | NOTE 2   | NOTE 2  | NOTE 2  | NOTE 2 | NOTE   |
|  | 25V | OFF | PASS   | PASS     | PASS      | PASS     | PASS    | PASS    | PASS   | PASS   |
| ENABLE   | 15V | ON  | PASS   | PASS     | PASS      | PASS     | NOTE 2  | NOTE 2  | NOTE 2 | NOTE   |
|  | 15V | OFF | PASS   | PASS     | PASS      | PASS     | PASS    | PASS    | PASS   | PASS   |
|  |     | ON  | PASS   | PASS     | PASS      | NOTE 2   | NOTE 2  | NOTE 2  | NOTE 2 | NOTE   |
|  | ±5V | OFF | PASS   | PASS     | PASS      | PASS     | PASS    | NOTE 1  | NOTE 1 | NOTE   |
| t <sub>disable</sub>   | 451 | ON  | PASS   | PASS     | PASS      | NOTE 1   | NOTE 2  | NOTE 2  | NOTE 2 | NOTE:  |
|  | 15V | OFF | PASS   | PASS     | PASS      | PASS     | NOTE 1  | NOTE 1  | NOTE 1 | NOTE   |

NOTE 1: Parameter out of limits

NOTE 2: Loss of functionality of the device.

NOTE 3: The results obtained for the Turn-off delay time (VS =  $\pm 15/0$ V) parameter, exceeded lightly the maximum limit shown in the test plan from 0krad step. As it is explained in the test plan, these limits have been taken from the 5962-08230 specification only as reference due to the fact that no limits were specified in the MFR data sheet (only are specified the typical values). For this reason, the maximum limit of the 20ns is not considered as pass/fails criteria in the initial electrical measurement and control sample.

Figure 8 presents a typical parameter value change vs accumulated dose. Most of the parameters affected by the dose only show very minor excess of limit. The worst failure is observed that some samples have lost functionality at 10krad checking point. The loss of functionality means when the input signal switches between high and low level, the output signal stays constant. No obvious excessive supply current is observed. But we notice the output pin diode threshold had dropped to 0.35V.

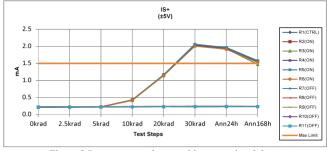


Figure 8 I<sub>S+</sub> parameter change with accumulated dose.

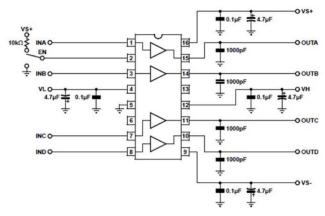
### **Summary**

The real dose rate at test is 203.39rad (Si)/h and up to cumulative dose of 30krad. The result shows EL7457 is very sensitive to the radiation damage. Most parameters are strongly affected by gamma dose. Between 5krad and 10krad, some biased samples lost the functionality or

completely failed. It is said the EL7457 was very poor and very non homogenous in radiation and the ISL7457 (their rad-hard equivalent version) had much better performance by partly re-design (e.g. improve the step coverage) and WLAT (Wafer Lot Acceptance Test) screening. However we note even the official datasheet for ISL7457 only claims 10krad minimum TID at dose rate of 50-300rad/s. This indicates the device design/manufacturing process is intrinsically sensitive to radiation damage. The lot under test only survived up to 5krad compared to the previous report of 50krad [5].

# 2) SEE <u>Setup</u>

The bias circuit in Figure 9 is used for the SEL test.



 $\begin{array}{c} Figure~9~EL7457~SEL~test~bias~circuit.\\ Test~configuration~is~DUT\_V+=+10V,~DUT\_V-=0V,~INPUTS=Square\\ wave~\pm 3.3V~at~2MHz. \end{array}$ 

#### Result

The summary of the result is listed in Table XII.

TABLE XII SUMMARY OF SEL TEST OF EL7457

| run_folder | Facility | medium | run_number | Facility_run_number | test_mode | board_id | dut_part_id | temperature | lon | LET | roll | tilt | Effective LET | run_duration | entered_fluence | SEL |
|------------|----------|--------|------------|---------------------|-----------|----------|-------------|-------------|-----|-----|------|------|---------------|--------------|-----------------|-----|
| RUN003     | RADEF    | vacuum | 3          | 48                  | SEL       | kit 2    | 1, 2        | room        | Xe  | 60  | 0    | 55   | 104.61        | 728          | 1.00E+07        | 0   |
| RUN004     | RADEF    | vacuum | 4          | 49                  | SEL       | kit 2    | 3,4         | room        | Хe  | 60  | 0    | 55   | 104.61        | 767          | 1.00E+07        | 0   |
| RUN005     | RADEF    | vacuum | 5          | 50                  | SEL       | kit 2    | 1, 2        | room        | Xe  | 60  | 0    | 58   | 113.22        | 785          | 1.00E+07        | 0   |
| RUN006     | RADEF    | vacuum | 6          | 51                  | SEL       | kit 2    | 3,4         | room        | Xe  | 60  | 0    | 58   | 113.22        | 782          | 1.00E+07        | 0   |
| RUN007     | RADEF    | vacuum | 7          | 52                  | SEL       | kit 2    | 1, 2        | room        | Хe  | 60  | 0    | 60   | 120.00        | 841          | 1.00E+07        | 0   |
| RUN008     | RADEF    | vacuum | 8          | 53                  | SEL       | kit 2    | 3,4         | room        | Xe  | 60  | 0    | 60   | 120.00        | 844          | 1.00E+07        | 0   |

# Summary

Same procedure and setup are followed as DG612. Only the thresholds are adjusted to 100mA for Vs+ and -100mA for Vs-. EL7457 proves to be latchup free up to 120 MeV.cm<sup>2</sup>.mg<sup>-1</sup>. Another study in [5] with test up to 80MeV also finds no incidence of latchup. SET is not tested. But ESA study on ISL7457ASRH [11]

SET is not tested. But ESA study on ISL7457ASRH [11] records cases at LET as low as 45.4MeV.cm<sup>2</sup>.mg<sup>-1</sup>.

#### IV. SUMMARY

AD8065 shows great immunity to Gamma ray up to the total dose of 30krad TID.

DG612 shows some sensitivity on some parameters but all tends to recover after annealing.

EL7457 is very sensitive to the radiation. Some samples failed between 5krad and 10krad permanently.

Both DG612 and EL7457 prove to be SEL free up to 120 MeV.cm<sup>2</sup>.mg<sup>-1</sup> for beam fluences up to 1E10<sup>7</sup> ions/cm<sup>2</sup>.

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