

The Earth's core as a reservoir of water

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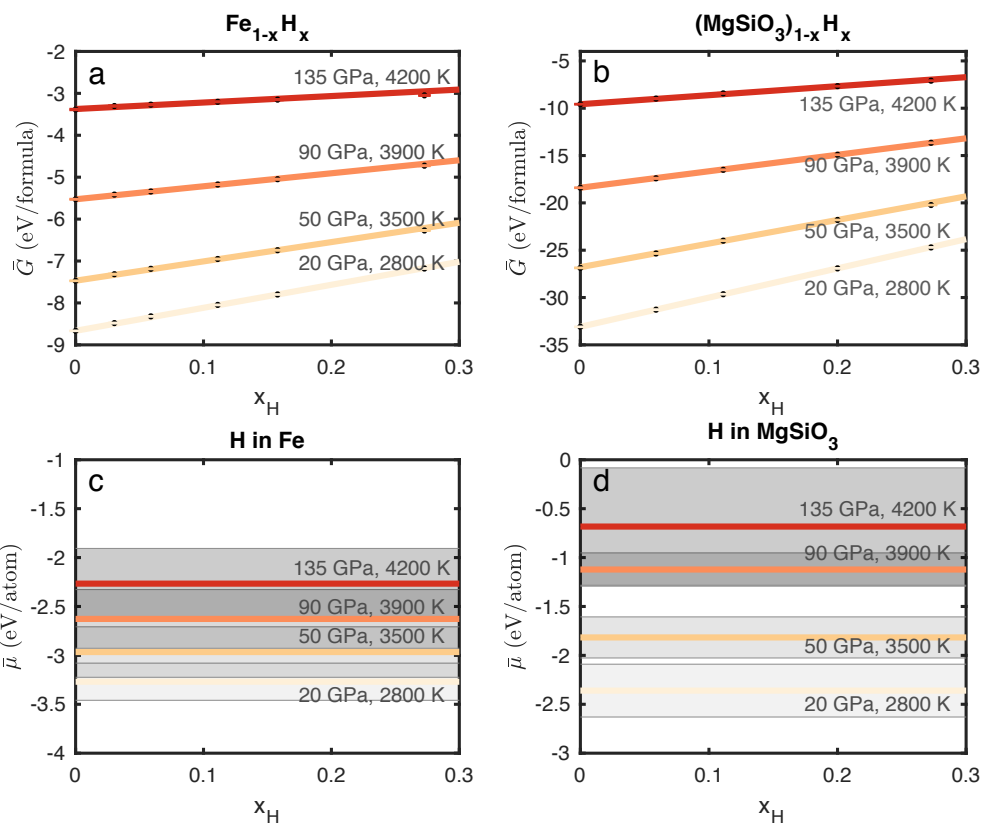
Current estimates of the budget and distribution of water in the Earth have large uncertainties, most of which come from the lack of information about the deep Earth. Recent studies suggest that the Earth could have gained a considerable amount of water during the early stages of Earth's evolution from the hydrogen-rich solar nebula, and that a large amount of the water in the Earth may have partitioned into the core. Here, we calculate the partitioning of water between iron and silicate melts at 20-135 gigapascals and 2800-5000 kelvin, using *ab initio* molecular dynamics and thermodynamic integration techniques. Our results indicate a siderophile nature of water at core-mantle differentiation and core-mantle boundary conditions, which can be weakened with increasing temperature; nevertheless, we find that water always partitions strongly into the iron liquid at both reducing and oxidising conditions. The siderophile nature of water is also verified by an empirical-counting method showing the distribution of hydrogen in an equilibrated iron and silicate melt. We therefore conclude that the Earth's core may act as a large reservoir containing most of the Earth's water. In addition to constraining accretion models and water distribution, the findings may partially account for the mismatch between mineral physics and seismic observations in the Earth's core.

Determining the water or hydrogen partition coefficient at high pressure (HP) high temperature (HT) conditions between iron and silicate melts isn't easy due to the low scatter cross section area of hydrogen, and therefore various methods have been used to detect hydrogen indirectly. In 1996, Kuramoto and Matsui¹ estimated the partition coefficient of hydrogen between iron and silicate melts using a thermodynamic model based on gas solubility. They reported that hydrogen is siderophile and the partitioning of hydrogen into iron increases with increasing pressure and temperature. A year later, Okuchi² measured the hydrogen partition coefficient by calculating the amount of hydrogen trapped in the bubbles of quenched FeH_x phases and determined the hydrogen concentration in the silicate melt through mass balance calculations. Their result agreed with the thermodynamic model in that over 95% of water accreted to the Earth should have reacted with iron and gone into the core. Several years later, Shibazaki *et al.*³ employed a different method to determine the hydrogen partition coefficient between solid iron and ringwoodite, for which they estimated the hydrogen concentration in iron from hydrogenation-induced lattice expansion, and by Fourier transform infrared spectroscopy (FTIR) in ringwoodite. Their experiments also indicate a siderophile nature of hydrogen. In contrast, Zhang and Yin⁴ reported an almost neutral behavior of hydrogen between liquid iron and silicate melts at 3200 K and 40 GPa by performing two-phase *ab initio* molecular dynamics (AIMD) simulations. Recently, Clesi *et al.*⁵ used elastic recoil detection analysis (ERDA) to determine hydrogen concentration in both iron and silicate melts at pressures of 5~20 GPa. They obtained a hydrogen metal-silicate partition coefficient of ~0.2, indicating lithophile behaviour of hydrogen. The contradiction to previous results was attributed to fugacity and possibly also the presence of carbon in samples. Malavergne *et al.*⁶ coupled the use of ERDA and Secondary Ion Mass Spectrometry (SIMS) to measure the hydrogen partition

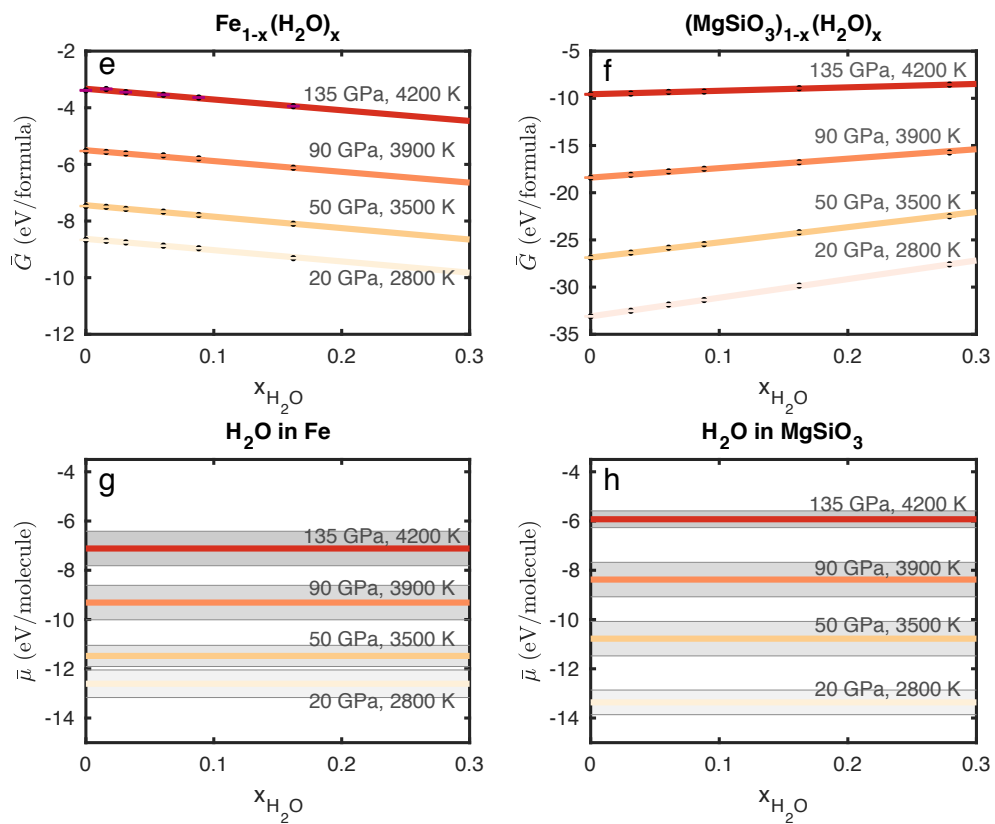
coefficient. Their study confirmed the pressure effect on hydrogen partitioning observed before, and also suggest that hydrogen could change from lithophile to siderophile above ~15 GPa.

Free energy calculations

The discrepancies in the literature and the complexity of hydrogen partitioning hinder our further understanding of water in the Earth and necessitate a comprehensive study that can accurately describe the partitioning behaviour under various pressure, temperature and fugacity conditions. *Ab initio* thermodynamics is a reliable and widely used method for partition calculations under HP-HT conditions⁷. In this study, we have calculated the Gibbs free energy of a series of iron and silicate melts with different concentrations of H₂/H₂O (see **Extended Data Table 1**) by performing AIMD with thermodynamic integration. We considered two end-member systems: $P_{\text{H}_2\text{O}}/P_{\text{H}_2+\text{H}_2\text{O}} = 1$ and $P_{\text{H}_2}/P_{\text{H}_2+\text{H}_2\text{O}} = 1$ (namely, in the context of experiments, iron and silicate are equilibrated in the environment of pure H₂O or H₂ in these two cases), representing oxidised and reduced conditions, respectively. The calculations were done at conditions above the solidus of our silicate melt at 20, 50, 90 and 135 GPa⁸, corresponding to temperatures of 2800, 3500, 3900 and 4200 K, respectively. We express the Gibbs free energy by $G(p, T, x) = \bar{G}(p, T, x) - TS_{\text{mix}}$, where x is the concentration of H or H₂O in iron or silicate melts, \bar{G} is the pure component of Gibbs free energy, and the second term TS_{mix} is the entropy contribution from mixing. From calculated Gibbs free energies, we derived the chemical potential of H/H₂O as $\mu_{\text{H}/\text{H}_2\text{O}}(p, T, x) = \bar{\mu}_{\text{H}/\text{H}_2\text{O}}(p, T, x) - TS_{\text{mix}}^{\text{H}/\text{H}_2\text{O}}$ (see **Methods**). With the calculated chemical potentials $\mu_{\text{H}/\text{H}_2\text{O}}(p, T, x)$, the partition coefficients can be derived. Here, we use “hydrogen” to refer to the general definition of “water”, and use H₂ and H₂O to denote the hydrogen and water molecules, respectively.



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Figure 1: **Calculated free energies.** **a, b, e and f)** Calculated Gibbs free energies $\bar{G}(p, T, x)$ (points) and their fits (curves) for $\text{Fe}_{1-x}\text{H}_x$, $(\text{MgSiO}_3)_{1-x}\text{H}_x$, $\text{Fe}_{1-x}(\text{H}_2\text{O})_x$ and $(\text{MgSiO}_3)_{1-x}(\text{H}_2\text{O})_x$ melts, respectively. **c, d, g and h)** Derived $\bar{\mu}_{\text{H}/\text{H}_2\text{O}}(p, T, x)$ quantities in iron and silicate melts. Shaded regions indicate uncertainties. See **Extended Data Table 1** for the raw data and **Supplementary Information** for a better view with uncertainties.

Fig. 1a and b show our calculated Gibbs free energies $\bar{G}(p, T, x)$ of iron and silicate melts as a function of hydrogen concentration, and **Fig. 1c and d** plot the derived $\bar{\mu}_{\text{H}}$. **Fig. 1e-h** show the Gibbs free energies $\bar{G}(p, T, x)$ of iron and silicate melts with H_2O and the derived pure component of chemical potential $\bar{\mu}_{\text{H}_2\text{O}}$. Under the same pressure, $\bar{\mu}_{\text{H}}$ is always lower in iron than in silicate. This is indicative that H is siderophile. Similarly, $\bar{\mu}_{\text{H}_2\text{O}}$ in liquid iron is also lower than in silicate melt from 50 to 135 GPa in **Fig. 1g and h**, suggesting a siderophile behavior of H_2O . While at 20 GPa, $\bar{\mu}_{\text{H}_2\text{O}}$ is slightly higher in liquid iron. This shows a pressure effect on H_2O partitioning.

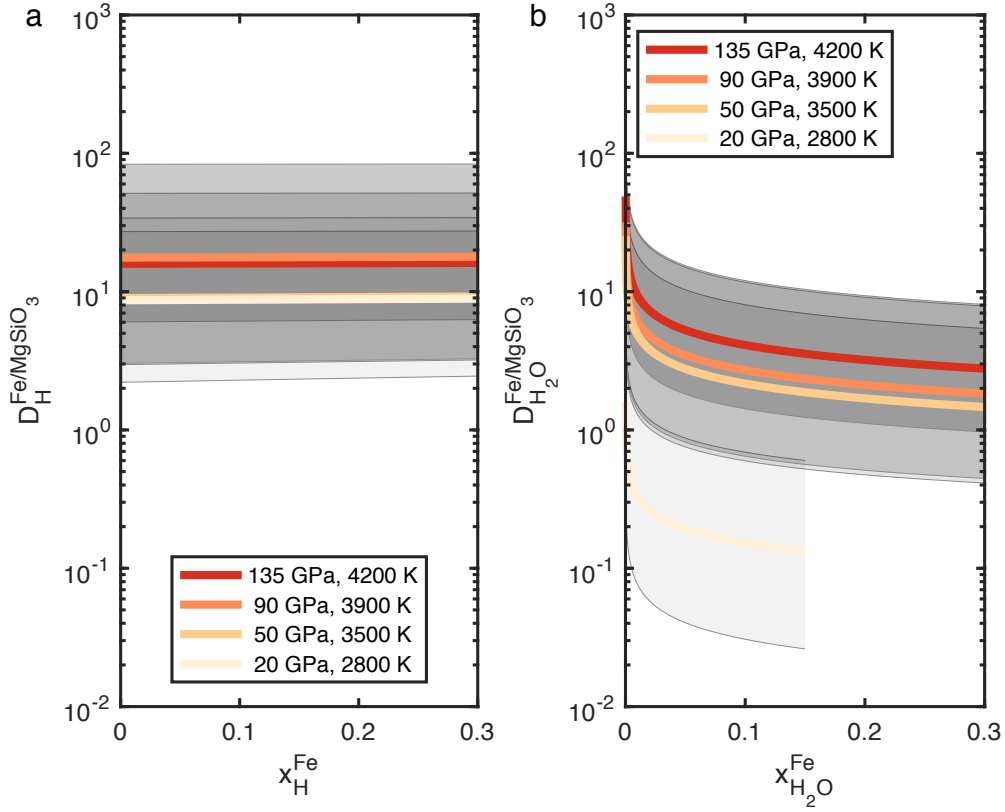


Figure 2: **Partition coefficient.** Derived partition coefficient between the iron and silicate melts as a function of concentration in iron for **a)** H and **b)** H₂O. Shaded regions are uncertainties. See **Supplementary Information** for a better view with uncertainties.

Partitioning coefficients

With the obtained free energies, we calculated the partition coefficient of H between iron and silicate melts (denoted by $D_{\text{H}}^{\text{Fe/MgSiO}_3}$) by equating the chemical potentials of H ($\mu_{\text{H}}(p, T, x)$) in both iron and silicate. As can be seen in **Fig. 2a**, $D_{\text{H}}^{\text{Fe/MgSiO}_3}$ does not show a visible dependence on x_{H}^{Fe} . $D_{\text{H}}^{\text{Fe/MgSiO}_3}$ is over 1 for all the examined pressures and compositions, showing a siderophile nature of H. The calculated partition coefficient of H₂O between iron and silicate melts $D_{\text{H}_2\text{O}}^{\text{Fe/MgSiO}_3}$ is shown in **Fig. 2b**. Generally speaking, H₂O is also siderophile except for at 20 GPa

95 where H₂O is slightly lithophile. $D_{\text{H}_2\text{O}}^{\text{Fe/MgSiO}_3}$ shows a sharp increase approaching the concentration
96 limit of $x_{\text{H}_2\text{O}}^{\text{Fe}}$, and such a behaviour is due to the entropy difference.

97 We did not include FeO in silicate melts nor O in the metal. The MgSiO₃ silicate is a good
98 approximation to the lower mantle⁹. According to the estimated O budget in the outer core and
99 FeO partition calculations¹⁰, the content of FeO in liquid MgSiO₃ should not be significant.
100 Furthermore, H atoms mainly pair with Fe and do not prefer an O-H bonding in liquid iron (see
101 **Supplementary Information**). Therefore, the presence of FeO in equilibrated iron and silicate
102 melts will have negligible effects on the siderophile character of hydrogen. The presence of ferric
103 iron in the silicate melt has also not been considered as the amount of ferric iron present during
104 core formation is likely to be very small¹¹. But regardless, the presence of ferric Fe₂O₃ should not
105 also change the siderophile behaviour of hydrogen as Fe₂O₃ in the silicate melt would be subjected
106 to the reaction: Fe₂O₃+2H=2FeO+H₂O, and this transformation (H to H₂O) basically does not
107 change the siderophile nature of hydrogen.

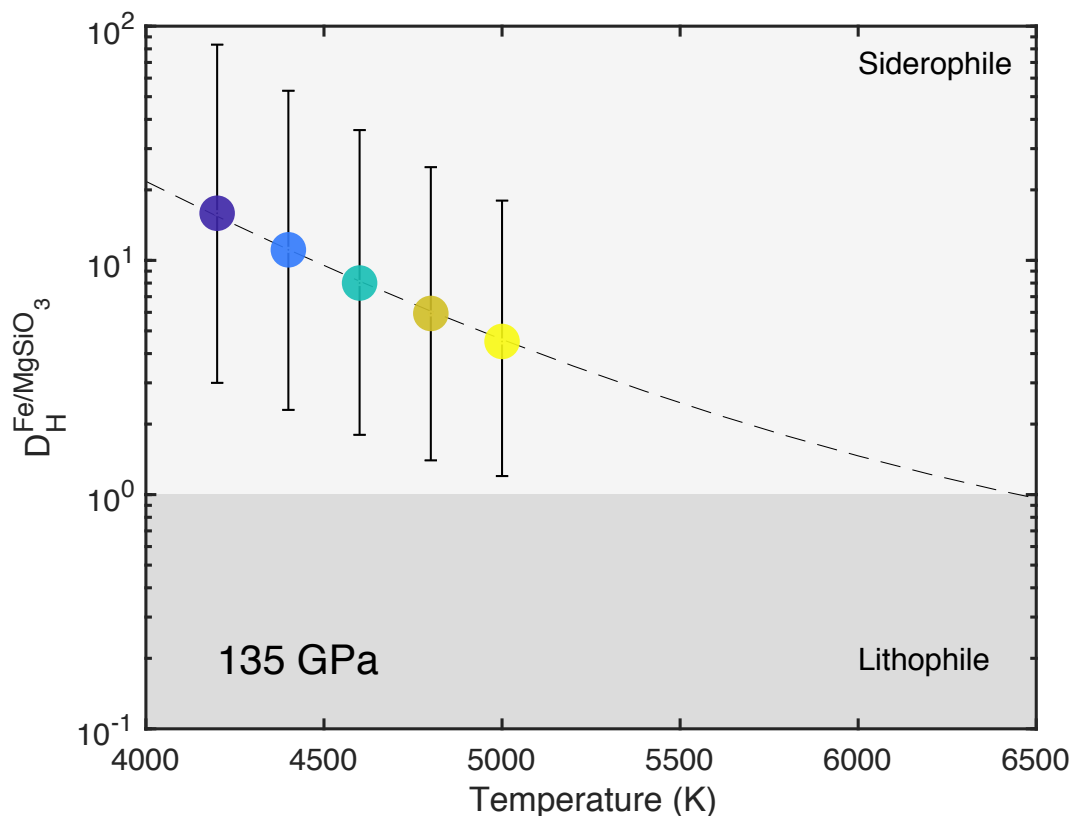


Figure 3: **Temperature dependence of H partitioning.** Calculated partition coefficient $D_H^{\text{Fe/MgSiO}_3}$ between iron and silicate melts as a function of temperature at 135 GPa. $D_H^{\text{Fe/MgSiO}_3}$ has little dependency on hydrogen concentration.

We have also explored the temperature dependence of H partitioning at 135 GPa – conditions appropriate to the core-mantle boundary (CMB) today. Gibbs free energies at temperatures from 4200 to 5000 K were obtained by integrating the Gibbs–Helmholtz equation based on the calculated temperature-dependent enthalpies (see **Extended Data Table 2**) and assuming the same concentration dependence of Gibbs free energy to 4200 K. As shown in **Fig. 3**, $D_H^{\text{Fe/MgSiO}_3}$ decreases with increasing temperature and is significantly lowered over the range from 4200 to 5000 K. By extrapolating our data, we found that the temperature would need to reach over ~6500 K for H to become lithophile.

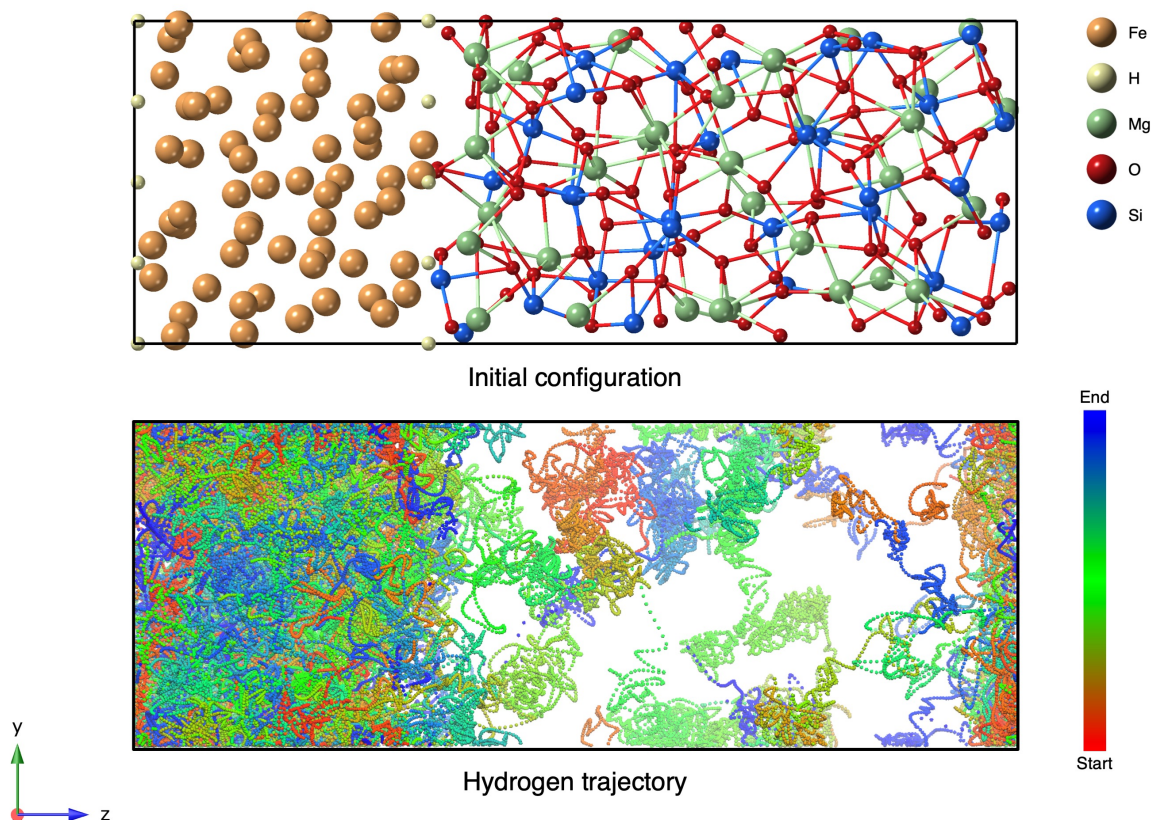


Figure 4: **Empirical counting of H partitioning**. Top panel: initial configuration of 12 hydrogen atoms sandwiched by 64 iron atoms and 32 formulas of MgSiO_3 for a NVT run of 10 *ps* at ~50 GPa and 3500 K. Both iron and silicate are in melt state during the calculation. Bottom panel: Plot of the trajectories of the 12 hydrogen atoms.

In addition to the free energy calculations, we performed another calculation using the empirical-counting strategy to verify the findings above (see **Methods**). We built one supercell that contains a melt of 64 Fe atoms, a melt of 32 formula of MgSiO_3 and 12 H atoms sandwiched between the two melts; the system size was chosen to minimise surface area while maintaining computational efficiency. The calculation was run at ~50 GPa and 3500 K for 10 *ps*. **Fig. 4** shows the initial setting and AIMD trajectories (also see the **Supplementary Information** for the Movie). It can be seen that H atoms mostly reside in the Fe side during the run, showing the siderophile

nature of H. We counted the average number of H atoms at each side and obtained $D_{\text{H}}^{\text{Fe/MgSiO}_3} = 3.1 \pm 0.3$, which is lower than our free energy calculation result that gives $D_{\text{H}}^{\text{Fe/MgSiO}_3} = 9.1_{-6}^{+18}$. It should be noted, however, that H diffuses much slower in silicate melt than in iron, so we might overcount the residence chance of H in silicate and obtain a $D_{\text{H}}^{\text{Fe/MgSiO}_3}$ smaller than its true value. The data from empirical counting may be improved with a longer run, bigger supercells and multiple independent simulations. As well as H, some Si and O atoms also entered the iron region which might also act to provide a slightly different $D_{\text{H}}^{\text{Fe/MgSiO}_3}$ compared to the free energy calculations. Nevertheless, these simulations agree qualitatively with the free energy results. It should be pointed out that Zhang and Yin⁴ obtained $D_{\text{H}}^{\text{Fe/MgSiO}_3} = 0.7 \pm 0.1$ using a similar two-phase model at 40 GPa and 3200 K, which is lower than our value. The discrepancy is likely from the setting of the two-phase model. They used a 44 iron atom cluster surrounded by silicate melt. Such a small cluster has a large surface-to-volume ratio and a significant fraction of interface atoms, and so probably does not represent the true partitioning between the bulk phases.

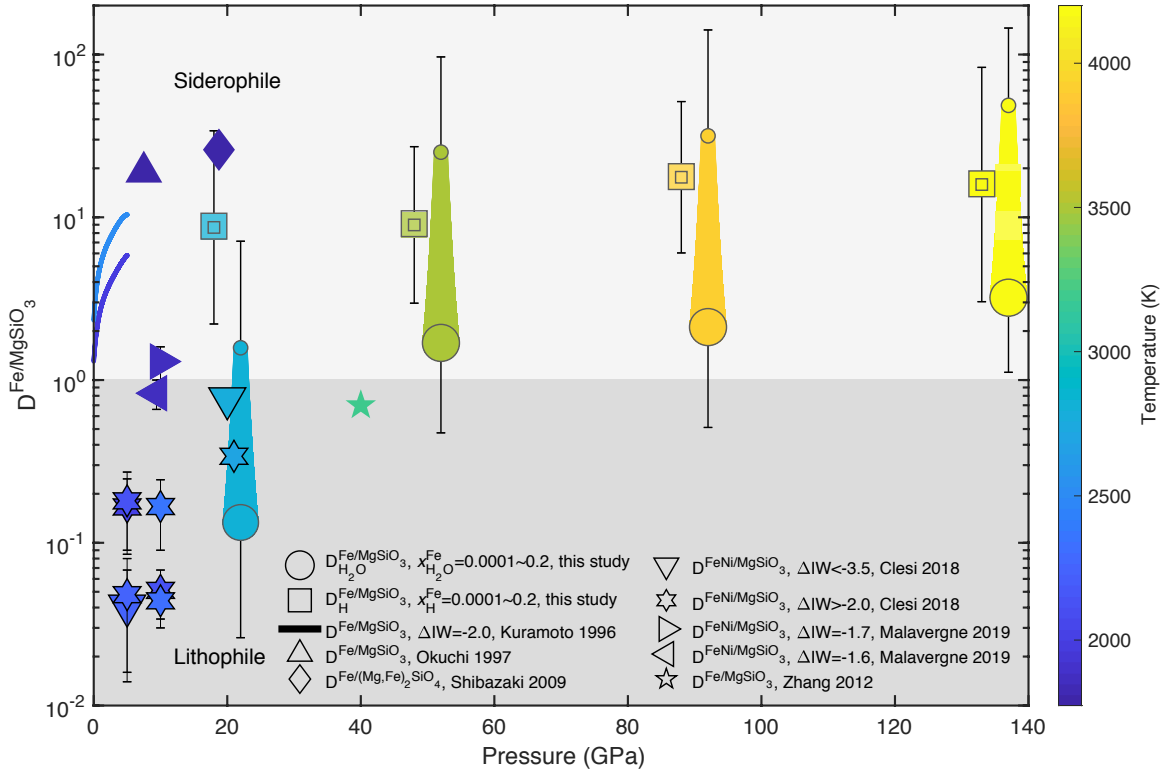


Figure 5: Comparison of partition coefficients with the literature. Compiled literature data in comparison with our partition coefficients of H and H₂O between iron and silicate melts calculated at 20, 50, 90 and 135 GPa, corresponding to 2800, 3500, 3900 and 4200 K. The partition coefficients of H and H₂O from this study were slightly shifted to lower and higher pressures, respectively, to facilitate a better view. The small and big squares (circles) indicate the partition coefficients of H (H₂O) at $x_{\text{H}/\text{H}_2\text{O}}^{\text{Fe}}=0.0001$ and 0.2, respectively.

Pressure and temperature dependence of water partitioning

In **Fig. 5**, we plot our partitioning coefficients of H and H₂O to compare with the literature. Our results agree with the findings of Kuramoto and Matsui¹, Okuchi² and Shibazaki *et al.*³, who determined the H concentration in iron via indirect methods. In contrast, Clesi *et al.*⁵ and Malavergne *et al.*⁶ found a more lithophile behaviour of hydrogen via direct methods. We note that H concentration is high in Okuchi's² experiments ($x_{\text{H}}^{\text{Fe}}>0.4$) and experiments of Shibazaki *et*

158 *al.*³ ($x_{\text{H}}^{\text{Fe}} > 0.5$), and is low in experiments of Clesi *et al.*⁵ and Malavergne *et al.*⁶ ($x_{\text{H}}^{\text{Fe}} < 0.03$). Our
159 results show that H is always siderophile at all possible ranges, and the difference between
160 experiments cannot be explained by the concentration difference. Experiments on the Fe-H system
161 show that hydrogen is nearly insoluble in both solid and liquid iron below 1 GPa^{12,13}, which
162 suggests that the hydrogen originally partitioned into iron at high pressure may have escaped upon
163 depressurisation, resulting in low concentrations in the Fe melt phase. In addition, Okuchi² found
164 that there is a minimum H₂O/MgSiO₃ molar ratio ($m \geq 1.0$) needed to keep P_{H_2} in the experiment
165 capsules, and in his experiments he used brucite, silicic acid and liquid H₂O to introduce hydrogen
166 in the system. While, in the experiments of Clesi *et al.*⁵ and Malavergne *et al.*⁶, hydrogen was
167 introduced into the system by adding Al(OH)₃ and brucite, and the H₂O/MgSiO₃ molar ratio is far
168 less than that in Okuchi's experiments². It is speculated that P_{H_2} is low in experiments of Clesi *et*
169 *al.*⁵ and Malavergne *et al.*⁶, and the actual condition could be more like our oxidising case
170 $P_{\text{H}_2\text{O}}/P_{\text{H}_2+\text{H}_2\text{O}} = 1$. Their partition coefficients also match ours at oxidising conditions.

171 Our H₂O partitioning coefficient strongly increases from 20 GPa to 50 GPa. The data of Clesi
172 *et al.*⁵ and Malavergne *et al.*⁶ at more oxidising conditions also show a similar trend from low
173 pressures to ~20 GPa. Unfortunately, their data do not extend to 50 GPa and so cannot be used to
174 confirm our high-pressure results, but the overlap at 20 GPa between our results and the
175 experimental results is reassuring. As for the temperature effect, Kuramoto and Matsui's¹ result
176 suggests that the increase of temperature strengthens the siderophile behaviour of H by using
177 extrapolated temperature-dependent molar volumes and solubilities in their thermodynamic model.
178 However, our free energy calculations clearly show the weakening of siderophile behaviour with
179 increasing temperature. We ran another empirical-counting simulation at ~50 GPa and 4000 K and
180 obtained $D_{\text{H}}^{\text{Fe}/\text{MgSiO}_3} = 2.1 \pm 0.3$, lower than that at ~50 GPa and 3500 K. This confirms that

$D_{\text{H}}^{\text{Fe/MgSiO}_3}$ decreases with increasing temperature. Apart from the pressure and temperature effects, there is a strong difference in the absolute value of hydrogen partitioning depending on whether it is H_2 or H_2O ; nevertheless, both species show siderophile behavior at high pressures relevant to the core-mantle differentiation (CMD) and CMB conditions.

Water in the deep Earth

The calculated hydrogen partition coefficients imply that the Earth's core can potentially act as a large reservoir of water. How much water is in the core depends on the amount of water dissolved in the silicate melt during core-formation, which is related to the Earth accretion process, the CMD process and the extent of equilibrium. If we assume a homogeneous accretion model of water to the Earth and a single-stage core-forming process at 50 GPa and 3500 K, over 76% of hydrogen will be partitioned into the core either at reducing conditions ($P_{\text{H}_2}/P_{\text{H}_2+\text{H}_2\text{O}}=1$) or under oxidising conditions ($P_{\text{H}_2\text{O}}/P_{\text{H}_2+\text{H}_2\text{O}}=1$). This means that if the one ocean of water we see at the Earth's surface was degassed from the mantle during or just after core-formation, then the core should contain a minimum of five oceans of water. Alternatively, in the case of a late veneer scenario, the Earth is almost free of water during the differentiation process and there would hardly be any water in the core.

Interestingly, our results show that at current CMB conditions, H_2 and H_2O are both more compatible in the core than in silicate melts. This means that any water held in a long lived deep basal magma ocean¹⁴ would tend to partition strongly into the core, suggesting that deep mantle anomalies resulting from a basal magma ocean (such as ULVZs and LLSVPs) should be relatively dry. In addition, any water added to the deepest mantle via subduction will also have a tendency to partition into the core now, either directly entering the core or reacting with liquid iron to form

iron oxide and release H₂ into the core¹⁵. Regardless of which or any of these processes are occurring, the chemistry of the core should be subject to a constant change.

A recent model to explain the low D/H ratio of the Earth suggests a combination of chondritic water and ingassing of nebular hydrogen, with four to five oceans of water are sequestered into the core¹⁶. This was based on high hydrogen solubility at high pressures and mantle hydrogen isotope fractionation. Our results are consistent with this model in that the core can be a reservoir of water. Recent noble gas isotope studies¹⁷⁻¹⁹ and early-Earth ingassing modelling²⁰ also provide strong evidence for the capture of nebular hydrogen during Earth' accretion. According to our partitioning results, the core at present, therefore, could hold a significant amount of water.

The presence of abundant hydrogen in the core may change its seismic, electric and thermal properties. Currently, core composition is still debated with an unexplained density deficit and low seismic velocities²¹⁻²³. Umemoto and Hirose²⁴ show that ~1 wt.% H in the outer core can match the compressional sound velocity and density, and suggest that hydrogen could be a primary light element in the core. A core with 1 wt% hydrogen is equivalent to the hydrogen content of ~130 oceans of water. Even with our highest partition coefficients at 50 GPa and 3500 K, a core with that much water would result in a mantle content of some 23 oceans of water. With one ocean at the surface now, this implies that the current mantle should have 22 oceans of water, which is above even the most optimistic saturation limits for the mantle²⁵, unless bridgmanite is able to incorporate far more water than is currently expected²⁶. Furthermore, hydrogen should also be able to partition into solid iron since the local environment of H in both solid and liquid iron is very similar, and the possibility of H in the inner core may also improve our current understanding about the inner core²⁷, for which only the multiple light elements model with carbon can explain its seismic properties²⁸.

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Methods

Chemical potential of H/H₂O

The chemical potential of H/H₂O in iron/silicate melt, $\mu_{\text{H}/\text{H}_2\text{O}}$, is the partial molar Gibbs free energy of H or H₂O:

$$\mu_{\text{H}/\text{H}_2\text{O}}(p, T, x) = \left(\frac{\partial G}{\partial n_{\text{H}/\text{H}_2\text{O}}} \right)_{p, T, n_{\text{Fe}/\text{MgSiO}_3}} \quad (1)$$

which is the free energy change when adding H or H₂O to the melts with all other conditions unchanged. We express the system Gibbs free energy by

$$G(p, T, x) = \bar{G}(p, T, x) - TS_{\text{mix}} \quad (2)$$

where S_{mix} is the ideal mixing entropy, and $\bar{G}(p, T, x)$ is the pure component free energy and equal to the sum of pure component of chemical potentials $\sum_{i=1}^n x_i \bar{\mu}_i$. The chemical potential also has two contributions, namely, the pure component and the mixing, and is written as

$$\mu(p, T, x) = \bar{\mu}(p, T, x) - TS_{\text{mix}} \quad (3)$$

We performed statistical tests on the calculated data $\bar{G}(p, T, x)$ per formula for the Fe_{1-x}H_x, (MgSiO₃)_{1-x}H_x, Fe_{1-x}(H₂O)_x and (MgSiO₃)_{1-x}(H₂O)_x systems, and the tests justify a linear model — the use of higher order polynomials is statistically invalid. Therefore, we fitted the calculated $\bar{G}(p, T, x)$ with

$$\bar{G}(p, T, x) = a + bx \quad (4)$$

where a and b are coefficients. We used a weighted fitting with the weight as $(\sum_{i=1}^n \sigma_{x_i})/\sigma_{x_1}$, where x_i is the i^{th} concentration and σ is the uncertainty of \bar{G} . $\bar{\mu}(p, T, x)$ for H and H₂O can be directly obtained, namely^{10,29},

$$\bar{\mu}_{\text{H}/\text{H}_2\text{O}}(p, T, x) = \bar{G}(p, T, x) + (1 - x) \frac{\partial \bar{G}(p, T, x)}{\partial x} = a + b \quad (5)$$

The ideal mixing entropy for the Fe_{1-x}H_x, (MgSiO₃)_{1-x}H_x, Fe_{1-x}(H₂O)_x and (MgSiO₃)_{1-x}(H₂O)_x systems are

$$S_{\text{mix}}^{\text{Fe}_{1-x}\text{H}_x} = -k_B T (x \ln x + (1 - x) \ln(1 - x)) \quad (6.1)$$

$$S_{\text{mix}}^{(\text{MgSiO}_3)_{1-x}\text{H}_x} = -k_B T \left(x \ln \left(\frac{x}{5-4x} \right) + (1 - x) \left(2 \ln \left(\frac{1-x}{5-4x} \right) + 3 \ln \left(\frac{3-3x}{5-4x} \right) \right) \right) \quad (6.2)$$

$$S_{\text{mix}}^{\text{Fe}_{1-x}(\text{H}_2\text{O})_x} = -k_B T \left(x \left(2 \ln \left(\frac{2x}{1+2x} \right) + \ln \left(\frac{x}{1+2x} \right) \right) + (1 - x) \ln \left(\frac{1-x}{1+2x} \right) \right) \quad (6.3)$$

$$S_{\text{mix}}^{(\text{MgSiO}_3)_{1-x}(\text{H}_2\text{O})_x} = -k_B T \left(x \left(2 \ln \left(\frac{2x}{5-2x} \right) + \ln \left(\frac{3-2x}{5-2x} \right) \right) + (1 - x) \left(2 \ln \left(\frac{1-x}{5-2x} \right) + 3 \ln \left(\frac{3-2x}{5-2x} \right) \right) \right) \quad (6.4)$$

respectively. k_B is the Boltzmann constant. Similarly, S_{mix}^{H/H_2O} can be calculated as $S_{mix}^{system} + (1-x)\frac{\partial S_{mix}^{system}}{\partial x}$. In equilibrium between iron and silicate melts, the chemical potential $\mu_{H/H_2O}(p, T, x)$ in iron is equal to that in silicate melt

$$\bar{\mu}_H^{Fe}(p, T, x) - T \left(S_{mix}^{Fe_{1-x}H_x} + (1-x) \frac{\partial S_{mix}^{Fe_{1-x}H_x}}{\partial x} \right) = \bar{\mu}_H^{MgSiO_3}(p, T, y) - T \left(S_{mix}^{(MgSiO_3)_{1-y}H_y} + (1-y) \frac{\partial S_{mix}^{(MgSiO_3)_{1-y}H_y}}{\partial y} \right) \quad (7.1)$$

$$\bar{\mu}_{H_2O}^{Fe}(p, T, x) - T \left(S_{mix}^{Fe_{1-x}(H_2O)_x} + (1-x) \frac{\partial S_{mix}^{Fe_{1-x}(H_2O)_x}}{\partial x} \right) = \bar{\mu}_{H_2O}^{MgSiO_3}(p, T, y) - T \left(S_{mix}^{(MgSiO_3)_{1-y}(H_2O)_y} + (1-y) \frac{\partial S_{mix}^{(MgSiO_3)_{1-y}(H_2O)_y}}{\partial y} \right) \quad (7.2)$$

where y is the concentration of H/H₂O in silicate. At each x , we can obtain y and $D_{H/H_2O}^{Fe/MgSiO_3} = x/y$ by solving equations 7.1/7.2 analytically. Hence, the solute concentration in silicate $x_{H/H_2O}^{MgSiO_3}$ can be easily derived for each solute fraction in iron x_{H/H_2O}^{Fe} based on chemical potential functions, and the partition coefficient can also be determined.

***Ab initio* molecular dynamics**

The Born–Oppenheimer AIMD calculations were performed with the density functional theory (DFT). The projector augmented wave (PAW) method^{30,31} implemented in the VASP code^{32,33} was employed to treat ion-electron interactions within the frozen-core approximation. Exchange-correlation effects were treated in the generalized gradient approximation (GGA) parameterised by Perdew, Burke and Ernzerhof³⁴. The Fermi–Dirac statistics were used to populate single particle orbitals. The plane-wave basis was generated with valence configurations of Fe- $3p^6 3d^7 4s^1$, Mg- $2p^6 3s^2$, Si- $3s^2 3p^2$, O- $2s^2 2p^4$, and H- $1s^1$. There is a high-to-low spin transition in liquid iron, but the density difference between magnetic calculation and non-magnetic calculation at 20 GPa and 2000 K is no more than 0.9%³⁵, and magnetism mainly shifts the volume/pressure without bringing apparent structural changes³⁶. The change to the chemical potential of H/H₂O by including magnetism is no more than 16/82 meV at 20 GPa. As discussed in the main text, the pressure effect on hydrogen partitioning is mainly due to the rapid increase of the hydrogen chemical potential in the silicate, which changes much slower in iron. Thus, including magnetism basically does not change our conclusions and all calculations were performed without spin polarisation.

We modeled the iron melt with a supercell of 64 Fe atoms obtained by melting *hcp*-Fe, and used a supercell containing 32 formulas of MgSiO_3 for the silicate melt obtained by melting perovskite. Then we added H_2 or H_2O into the supercells. The examined compositions can be seen in **Extended Data Table 1**. A plane-wave energy cutoff of 600 eV and 800 eV for the iron melts and silicate melts, respectively, was able to converge the energy within 1 meV/atom and pressure within 0.15 GPa together with a $2 \times 2 \times 2$ Monkhorst-Pack k-mesh. To save computer time, we first run the calculations using a single Gamma point and an energy cutoff of 400 eV and 600 eV for the iron and silicate melts, respectively. We then made corrections to 600 eV and 800 eV with a $2 \times 2 \times 2$ Monkhorst-Pack k-mesh, respectively, by doing free energy perturbation and thermodynamic integration^{37,38}.

The iron and silicate melts were first relaxed at target pressures of 20, 50, 90 and 135 GPa, corresponding to temperatures of 2800, 3500, 3900 and 4200 K (roughly above the solidus of silicate melt⁸). The relaxation was done with constrained NPT (constant number of atoms N , pressure P and temperature T) calculations that maintained the cubic supercell. A time step of 1 fs was used for all NPT runs. NPT calculations were run for over 10 ps and the lattice parameters were extracted from the last eight picoseconds. When shifting to different P-T conditions, the melt structures were allowed to relax long enough as approaching the new PT condition step-by-step. These derived lattice parameters were then used for NVT (constant number of atoms N , volume V and temperature T) calculations, which normally last over several picoseconds; the first picoseconds were discarded for free energy calculations.

Thermodynamic integration

Gibbs free energy of melts was calculated by performing thermodynamic integration (TI) to the Weeks-Chandler-Andersen (WCA) gas system, which has established thermodynamics and no liquid-gas transition^{39,40}. The efficiency of this approach has been recently demonstrated in calculating the melting curve of elemental systems³⁷. In this study we extend this method to the free energy calculation of mixtures. The WCA system is a truncated repulsive Lennard-Jones (rLJ) system characterized by the energy parameter ε and length parameter σ , for which the potential ϕ_{WCA} is defined as

$$\phi_{\text{WCA}}(r) = \begin{cases} 4\varepsilon \left[\left(\frac{\sigma}{r} \right)^{12} - \left(\frac{\sigma}{r} \right)^6 \right] + \varepsilon, & r \leq 2^{1/6}\sigma \\ 0, & r > 2^{1/6}\sigma \end{cases} \quad (8)$$

The potential during the transition from the *ab initio* system to the WCA system can be denoted as $\phi_\lambda = \phi_{\text{WCA}} + \lambda\phi$, where λ is the coupling parameter and ϕ is the electronic free energy from *ab initio* calculation. ϕ_λ smoothly shifts from the *ab initio* to the WCA potential as $\lambda \rightarrow 0$ when we set $2^{1/6}\sigma$ to be less than the minimal bond length

in the *ab initio* system. Gibbs free energy is calculated as $G = F(V) + P_0 V$, where $F(V)$ is the Helmholtz free energy and P_0 is the target pressure. $F(V)$ can be determined via TI as

$$F(V) = F_{\text{WCA}} + \frac{1}{N} \int_0^1 \langle \phi_\lambda \rangle d\lambda = F_{\text{WCA}} + \frac{1}{Nm} \int_0^1 \frac{\langle \phi_\lambda \rangle}{\lambda^{m-1}} d\lambda^m \quad (9)$$

Where N is the number of atoms in the system and F_{WCA} is the documented free energy of the WCA gas^{39,40}. We followed the previous study to transform λ to λ^m in order to ensure the integrand can be expressed in low-order polynomials³⁷. A six-point Gaussian-Legendre quadrature was sufficient to converge the integral. F_{WCA} was calculated by $F_{\text{WCA}} = F_{\text{ig}} + F'_{\text{WCA}}$, where F_{ig} is the ideal gas free energy and F'_{WCA} is the free energy difference between the ideal gas and the WCA system, and

$$F_{\text{ig}} = -k_B T \sum_{i=1}^n \ln Z_i = -k_B T \sum_{i=1}^n n \ln \left(\frac{\Omega}{N_i \Lambda_i^3} \right) = k_B T \sum_{i=1}^n \left[\ln \frac{\Lambda_i^3}{V} - 1 \right] \quad (10)$$

for the multicomponent system, where Ω is the system volume, V is the volume per atom, n is the number of elements, and Z_i , N_i and Λ_i are the partition function, number of atoms and thermal wavelength for element i , respectively. $\Lambda_i = h / \sqrt{2\pi m_i k_B T}$, where h is the Planck constant, m_i is the mass of element i .

The uncertainties of $\langle \phi_\lambda \rangle$ were obtained by using blocking method and integrated to obtain the uncertainty of \bar{G} . The uncertainties of $\bar{\mu}_{\text{H}/\text{H}_2\text{O}}$ were derived following the error propagation rule.

Empirical-counting strategy

At 50 GPa and 3500 K, we first relaxed both the iron (64 Fe atoms) and silicate (32 formulas of MgSiO_3) melt structures into a rectangular supercell with a square x - y plane of $9 \times 9 \text{ \AA}^2$. Then, we combined the two supercells into one with some space between the two parts in order to place 12 hydrogen atoms. Six hydrogen atoms were inserted at each of the two Fe/ MgSiO_3 interfaces. The integrated supercell was equilibrated within NVT ensemble for 10 ps at 3500 K. For each MD step, we calculated the bond length for every hydrogen atom, which was tagged as a residence in the iron if its nearest neighbor atom is Fe apart from hydrogen. Finally, we obtained a partition coefficient $D_{\text{H}}^{\text{Fe}/\text{MgSiO}_3} = 3.1 \pm 0.3$.

Data availability

The raw outputs can be accessed in the UK National Geoscience Data Centre (NGDC) (<https://dx.doi.org/10.5285/d0677edf-c987-497d-aae8-23bf22ef774d>). Any additional data can be requested by e-mailing the corresponding author.

Code availability

The Vienna *Ab Initio* Simulation Package (VASP) is a proprietary software available for purchase at <https://www.vasp.at/>.

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Author Contributions

Y.L. carried out the simulations and analysis. L.V. and J.B supervised the project. All authors contributed to data analysis and writing the paper.

Competing interests

The authors declare no competing interests.

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Figure Captions

Figure 1: Calculated free energies. **a, b, e and f)** Calculated Gibbs free energies $\bar{G}(p, T, x)$ (points) and their fits (curves) for $\text{Fe}_{1-x}\text{H}_x$, $(\text{MgSiO}_3)_{1-x}\text{H}_x$, $\text{Fe}_{1-x}(\text{H}_2\text{O})_x$ and $(\text{MgSiO}_3)_{1-x}(\text{H}_2\text{O})_x$ melts, respectively. **c, d, g and h)** Derived $\bar{\mu}_{\text{H}/\text{H}_2\text{O}}(p, T, x)$ quantities in iron and silicate melts. Shaded regions indicate uncertainties. See **Extended Data Table 1** for the raw data and **Supplementary Information** for a better view with uncertainties.

Figure 2: Partition coefficient. Derived partition coefficient between the iron and silicate melts as a function of concentration in iron for **a)** H and **b)** H_2O . Shaded regions are uncertainties. See **Supplementary Information** for a better view with uncertainties.

Figure 3: Temperature dependence of H partitioning. Calculated partition coefficient $D_{\text{H}}^{\text{Fe}/\text{MgSiO}_3}$ between iron and silicate melts as a function of temperature at 135 GPa. $D_{\text{H}}^{\text{Fe}/\text{MgSiO}_3}$ has little dependency on hydrogen concentration.

Figure 4: Empirical counting of H partitioning. Top panel: initial configuration of 12 hydrogen atoms sandwiched by 64 iron atoms and 32 formulas of MgSiO_3 for a NVT run of 10 ps at ~50 GPa and 3500 K. Both iron and silicate are in melt state during the calculation. Bottom panel: Plot of the trajectories of the 12 hydrogen atoms.

Figure 5: Comparison of partition coefficients with the literature. Compiled literature data in comparison with our partition coefficients of H and H_2O between iron and silicate melts calculated at 20, 50, 90 and 135 GPa, corresponding to 2800, 3500, 3900 and 4200 K. The partition coefficients of H and H_2O from this study were slightly shifted to lower and higher pressures,

respectively, to facilitate a better view. The small and big squares (circles) indicate the partition coefficients of H (H₂O) at $x_{\text{H}/\text{H}_2\text{O}}^{\text{Fe}}=0.0001$ and 0.2, respectively.

Extended Data Table 1 | Calculated free energies. Calculated volumes and Gibbs free energies $\bar{G}(p, T, x)$ of iron and silicate melts with H and H₂O at 20, 50, 90, and 135 GPa, corresponding to temperatures of 2800, 3500, 3900 and 4200 K, respectively.

Material	P (GPa)	T (K)	V (Å ³ /atom)	\bar{G} (eV/atom)
Fe ₆₄	20	2800	10.798	-8.665±0.008
	50	3500	9.999	-7.472±0.009
	90	3900	9.148	-5.527±0.011
	135	4200	8.509	-3.385±0.016
Fe ₆₄ H ₂	20	2800	10.578	-8.481±0.011
	50	3500	9.751	-7.315±0.013
	90	3900	8.934	-5.416±0.014
	135	4200	8.312	-3.048±0.013
Fe ₆₄ H ₄	20	2800	10.372	-8.320±0.009
	50	3500	9.544	-7.186±0.011
	90	3900	8.756	-5.342±0.013
	135	4200	8.125	-3.270±0.017
Fe ₆₄ H ₈	20	2800	9.936	-8.047±0.010
	50	3500	9.132	-6.951±0.011
	90	3900	8.372	-5.175±0.013
	135	4200	7.766	-3.202±0.013
Fe ₆₄ H ₁₂	20	2800	9.557	-7.798±0.007
	50	3500	8.776	-6.742±0.011
	90	3900	8.045	-5.048±0.013
	135	4200	7.449	-3.150±0.014
Fe ₆₄ H ₂₄	20	2800	8.662	-7.178±0.008
	50	3500	7.913	-6.271±0.011
	90	3900	7.222	-4.726±0.011
	135	4200	6.687	-3.048±0.013
Fe ₆₂ (H ₂ O) ₁	20	2800	10.515	-8.240±0.008
	50	3500	9.693	-7.127±0.014
	90	3900	8.880	-5.284±0.012
	135	4200	8.245	-3.246±0.014
Fe ₆₂ (H ₂ O) ₂	20	2800	10.263	-8.240±0.008
	50	3500	9.429	-7.127±0.014
	90	3900	8.640	-5.284±0.012
	135	4200	8.031	-3.246±0.014
Fe ₆₂ (H ₂ O) ₄	20	2800	9.799	-7.912±0.007
	50	3500	8.986	-6.840±0.012
	90	3900	8.202	-5.067±0.012
	135	4200	7.618	-3.158±0.014
Fe ₆₂ (H ₂ O) ₆	20	2800	9.380	-7.618±0.008
	50	3500	8.604	-6.619±0.013
	90	3900	7.846	-4.919±0.012

	135	4200	7.263	-3.092±0.013
Fe ₆₂ (H ₂ O) ₁₂	20	2800	8.513	-7.032±0.008
	50	3500	7.744	-6.114±0.012
	90	3900	7.021	-4.621±0.010
	135	4200	6.484	-2.978±0.013
(MgSiO ₃) ₃₂	20	2800	9.984	-6.618±0.006
	50	3500	8.277	-5.373±0.008
	90	3900	7.281	-3.680±0.007
	135	4200	6.617	-1.915±0.008
(MgSiO ₃) ₃₂ H ₄	20	2800	9.763	-6.509±0.008
	50	3500	8.182	-5.267±0.008
	90	3900	7.199	-3.624±0.010
	135	4200	6.505	-1.850±0.010
(MgSiO ₃) ₃₂ H ₈	20	2800	9.639	-6.410±0.008
	50	3500	8.115	-5.191±0.009
	90	3900	7.089	-3.551±0.010
	135	4200	6.424	-1.826±0.010
(MgSiO ₃) ₃₂ H ₁₂	20	2800	9.522	-6.320±0.008
	50	3500	8.017	-5.174±0.009
	90	3900	6.986	-3.493±0.010
	135	4200	6.338	-1.814±0.010
(MgSiO ₃) ₃₂ H ₂₄	20	2800	9.272	-6.086±0.008
	50	3500	7.744	-4.900±0.009
	90	3900	6.743	-3.347±0.010
	135	4200	6.091	-1.783±0.010
(MgSiO ₃) ₃₁ (H ₂ O) ₁	20	2800	9.821	-6.584±0.008
	50	3500	8.210	-5.337±0.008
	90	3900	7.216	-3.667±0.011
	135	4200	6.539	-1.924±0.010
(MgSiO ₃) ₃₁ (H ₂ O) ₂	20	2800	9.758	-6.528±0.008
	50	3500	8.155	-5.293±0.008
	90	3900	7.154	-3.637±0.008
	135	4200	6.483	-1.911±0.010
(MgSiO ₃) ₃₁ (H ₂ O) ₃	20	2800	9.680	-6.503±0.007
	50	3500	8.072	-5.276±0.008
	90	3900	7.099	-3.621±0.008
	135	4200	6.437	-1.925±0.010
(MgSiO ₃) ₃₁ (H ₂ O) ₆	20	2800	9.416	-6.383±0.010
	50	3500	7.894	-5.173±0.008
	90	3900	6.931	-3.587±0.010
	135	4200	6.270	-1.910±0.010
(MgSiO ₃) ₃₁ (H ₂ O) ₁₂	20	2800	9.038	-6.212±0.010
	50	3500	7.570	-5.064±0.013
	90	3900	6.631	-3.543±0.010
	135	4200	6.002	-1.925±0.010
(MgSiO ₃) ₃₁ (H ₂ O) ₁₆	135	4200	5.841	-1.937±0.010

Extended Data Table 2 | Temperature dependence of free energies. Calculated volumes, enthalpies and Gibbs free energies $\bar{G}(p, T, x)$ of Fe₆₄, Fe₆₄H₄, (MgSiO₃)₃₂ and (MgSiO₃)₃₂H₈ at temperatures from 4200 to 5000 K under 135 GPa.

Material	T (K)	V ($\text{\AA}^3/\text{atom}$)	H (eV/atom)	\bar{G} (eV/atom)
Fe ₆₄	4200	8.509	1.150	-3.385
	4400	8.529	1.222	-3.603
	4600	8.568	1.313	-3.824
	4800	8.601	1.407	-4.050
	5000	8.627	1.497	-4.279
Fe ₆₄ H ₄	4200	8.125	1.052	-3.270
	4400	8.162	1.122	-3.477
	4600	8.197	1.209	-3.688
	4800	8.219	1.307	-3.903
	5000	8.249	1.387	-4.122
(MgSiO ₃) ₃₂	4200	6.617	0.600	-1.915
	4400	6.642	0.684	-2.037
	4600	6.677	0.754	-2.162
	4800	6.687	0.868	-2.291
	5000	6.716	0.943	-2.424
(MgSiO ₃) ₃₂ H ₈	4200	6.424	0.641	-1.826
	4400	6.453	0.730	-1.946
	4600	6.473	0.794	-2.069
	4800	6.511	0.909	-2.196
	5000	6.534	0.972	-2.326