Performance Analysis of AF Relaying with Selection Combining in Nakagami-$m$ Fading

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Abstract—This paper investigates performance analysis of a selection combining scheme, which utilizes a variable gain amplify and forward (AF) relay over a Nakagami-$m$ fading channel. A selection combiner at a destination node chooses the better link between a relay channel and a direct channel. We derived exact closed-form expressions for moments of signal to noise ratio (SNR), ergodic capacity and average symbol error probability (SEP). Simulation examples confirm that our exact formulas offer a more accurate analysis tool for selection combining than other prevailing approximations without extra complexity. The derived expressions serve as a useful tool for system design due to their validity for any SNR and arbitrary system parameters.

Index Terms—selection combining, AF relaying, outage probability, Nakagami-$m$ fading, symbol error probability

I. INTRODUCTION

Internet of things covers many interdisciplinary issues, such as environmental monitoring, control of industrial processes, smart spaces and so on. As a complex technological innovation, internet of things confirms that future wireless communications are highly dense and heterogeneous. Dense networks make it possible for relay transmission, such as two-hop and multihop networks [1]–[3]. A relay node may forward a signal with either an amplify and forward (AF) or a decode and forward (DF) protocol. These two protocols have been well studied. For example, an approximate bit error probability was derived in [4] for a Rake receiver at relays and destination over multipath Nakagami-$m$ fading. A Turbo code was applied in [5] for asymptotic outage probability in relay selection networks. The distributed relay processing, ideal centralized maximal ratio combining and centralized maximal ratio combining relay processing were employed in [6], which introduced Nakagami and Gamma distribution for approximate bit error rate of binary phase shift keying. Incremental DF and AF relaying were considered in [7] for analyzing the diversity multiplexing tradeoff. Orthogonal space time block coding was assumed in [8] for deriving closed formula of higher moments of end-to-end signal to noise ratio (SNR).

Diversity technique aims at a performance improvement of a wireless system. Among all different diversity schemes, selection combining may be the simplest one. The importance of selection combining has motivated numerous researches.

Selection combining of direct and relayed paths in space shift keying was analyzed in [9]. A bit error rate based selection combining was proposed in [10], which calculated bit error rate of each branch and selected the branch with the minimum bit error rate. A single threshold was employed to select retransmitting relays in [11]. Exact bit error rate formulas of digital modulation was derived in [12] when an arbitrary number of relays used selection combining. In [13], selection combining was employed in cyclic prefixed single carrier DF relaying protocol and the transmit antenna selection and receive selection combining was investigated in [14]. An arbitrary fading parameter $m$ was considered in [15], [16] for DF relaying systems while Rayleigh fading was studied in [17]–[19] for AF relaying.

Performance analysis of selection combining in a Nakagami channel was recently reported but mostly for the case of integer $m$ [13], [14], [20]. When non integer $m$ is encountered, infinite series expansion has to be exploited for numerical evaluation, whose exact analytical evaluation appears to be difficult [16]. Some researchers only provided a loose lower or upper bound by simplification [21]. Infinite series always requires truncated partial summation, whose numbers of terms rely on a precision threshold. For comparison, the previous works are summarized in Tab.I.

To improve performance evaluation accuracy and reduce the calculation complexity, this paper investigates performance analysis of an AF relay system with selection combining over Nakagami-$m$ fading channel, where $m$ is a positive number or a non negative number plus one half. Although maximal ratio combining is the optimal combining technique, it requires computing the optimal weight for each branch. Selection combining may be the simplest combining scheme, which selects the signal with the largest SNR out of multiple branches and ignores the remaining branches. The decision variable is computed between the direct link and the relaying link and the one with a larger magnitude is chosen for selection combining. In practice, the selection combining technology has been used in many scenarios, such as the internet of things domain [3] and power line communications [22]. The exact higher order moments of the end to end SNR, ergodic capacity and average symbol error probability (SEP) formulas are obtained. Different from the additive white Gaussian noise (AWGN) assumption in most studies, our problem formulation is also extended to an additive white generalized Gaussian noise (AWGNN) environment, which is a more general type of noise model. The exact SEP formula subject to AWGNN implies that one can obtain the error performance in a more general scenario, such as Laplace noise and uniformly distributed.
Consider a relay system consisting of a source node $S$, an AF relay node $R$, and a destination node $D$, as shown in Fig.1. $S$ transmits information to $D$ directly or via $R$ during two phases. In the first phase, $S$ sends its signals while $R$ and $D$ listen. In the second phase, $S$ stays silent while $R$ forwards the amplified signals to $D$ if the relay link is beneficial. We assume that all channels experience independent Nakagami-$m$ fading, where $m$ is a positive number or a non-negative number plus one half. Let $p_s$ and $p_r$ be the transmit powers of $S$ and $R$, respectively. Denote by $h_s$, $h_r$, and $h_d$ the channel coefficients of the $S\rightarrow R$, $R\rightarrow D$ and $S\rightarrow D$ links, respectively. In addition, $\sigma^2_r$ and $\sigma^2_d$ represent noise variances at $R$ and $D$, respectively. Thus, the instantaneous SNR of the direct link and the SNR of the relay link are, respectively, given by [20]

$$\gamma_1 = \frac{p_s |h_d|^2}{\sigma^2_d} + p_r |h_r|^2$$

$$\gamma_2 = \frac{\sigma^2_r^2}{\sigma^2_s^2} + 1$$

Assuming that $D$ combines the received signals from the $S\rightarrow D$ and $S\rightarrow R\rightarrow D$ links by selection combining, the end to end SNR at $D$ is given by [20]

$$\gamma = \max(\gamma_1, \gamma_2)$$

The corresponding cumulative distribution function (CDF) $F_\gamma(z)$ is given by [20]

$$F_\gamma(z) = F_{\gamma_1}(z) F_{\gamma_2}(z)$$

### III. PERFORMANCE ANALYSIS

#### A. Outage Probability

1) $m$ is a positive number: Since $h_s$, $h_r$ and $h_d$ are modeled as Nakagami-$m$ random variables, the CDFs of $\gamma_s$ and $\gamma_r$ are, respectively, given by [20]

$$F_{\gamma_1}(x) = 1 - \frac{\Gamma(m_d, \beta_d x)}{\Gamma(m_d)}$$

$$F_{\gamma_2}(y) = 1 - \frac{2 e^{-(\beta_s + \beta_d) y}}{\Gamma(m_r)} \sum_{l_1=0}^{m_s-1} \sum_{l_2=0}^{m_r-1} C_{m_s-1}^{l_1} C_{m_r-1}^{l_2}$$

$$\times \frac{1}{l_1! + \frac{1}{2} \frac{1-k+l_1}{2} \beta_s^m r_{m_r}^{-1-k+l_2} y l_1 + m_r}$$

$$\times K_{k-1-l_2} \left(2 \sqrt{1/3} \beta_r y \right)$$

where $\beta_s$ and $\beta_r$ are the channel gains of the $S\rightarrow R$ and $R\rightarrow D$ links, respectively.
where $m_s$, $m_r$ and $m_d$ are the shape parameters of channel coefficients $h_s$, $h_r$ and $h_d$, respectively. Moreover, $\beta_s = m_s \sigma_s^2/\left[ p_s E \left( h_s^2 \right) \right]$, $\beta_r = m_r \sigma_r^2/\left[ p_r E \left( h_r^2 \right) \right]$ and $\beta_d = m_d \sigma_d^2/\left[ p_d E \left( h_d^2 \right) \right]$ denote the corresponding scale parameters, where $E(\cdot)$ is the expectation operator, $C_z$ stands for the binomial coefficient and $K_\nu(\cdot)$ is the $\nu$th order modified Bessel function of the second kind [23, eq.(8.432.1)]. Furthermore, $\Gamma(\cdot)$ is the gamma function [23, eq.(8.310.1)] and $\Gamma(\cdot,\cdot)$ is the upper incomplete gamma function [23, eq.(8.350.2)].

2) $m$ is a non negative number plus one half: The CDF of $\gamma_1$ is the same as eq.(5) but the CDF of $\gamma_2$ is written as follows [24]

$$F_{\gamma_2}(y) = 1 - \sqrt{\pi}e^{-(\sqrt{\beta_s} + \sqrt{\beta_r})^2 y} \left( \sqrt{\beta_s} + \sqrt{\beta_r} \right) \sum_{k_1=0}^{m_s} \sum_{k_2=0}^{m_r} \frac{(m_s + k_1)! (m_r + k_2)! \beta_s^{m_s - k_1} \beta_r^{m_r - k_2}}{4^{k_1+k_2} k_1! k_2! (m_s - k_1)! (m_r - k_2)!} \times y^{m_s-k_1+m_r-k_2} \Psi \left( \frac{3}{2}; \frac{3}{2}; \frac{1}{2} \right) \left( \sqrt{\beta_s} + \sqrt{\beta_r} \right)^2 \right) \frac{y^3}{2}$$

(7)

where $[\cdot]$ is the floor function and $\Psi(\cdot;\cdot;\cdot)$ is the confluent hypergeometric function defined in [23, eq.(9.210.2)].

Then, the outage probability of the end to end SNR $\gamma$ is given by

$$P_{out} = Pr(\gamma \leq \gamma_{th}) = F_{\gamma}(\gamma_{th})$$

(8)

where $\gamma_{th}$ is a preset threshold. Substituting the corresponding $F_{\gamma_1}(x)$ and $F_{\gamma_2}(y)$ into eq.(4) yields the exact outage probability $P_{out}$.

B. Moments of SNR

In selection combining, the destination chooses a larger magnitude as the decision variable between the direct link and the indirect link. Again, we consider the following two cases:

1) $m$ is a positive number: In order to calculate the higher order moment, the CDF of the equivalent SNR $\gamma$ is rewritten as

$$F_{\gamma}(z) = F_{\gamma_1}(z) F_{\gamma_2}(z) = 1 - \bar{F}_{\gamma_1}(z) - \bar{F}_{\gamma_2}(z) + \bar{F}_{\gamma_1}(z) \bar{F}_{\gamma_2}(z)$$

where $\bar{F}(\cdot) = 1 - F(\cdot)$ is the complementary CDF. Taking the expectation of $\gamma^n$ over the distribution of $F_{\gamma}(z)$ via integration by parts, the higher order moment is obtained as

$$E(\gamma^n) = \int_{0}^{\infty} n \left[ 1 - F_{\gamma}(z) \right] z^{n-1} dz$$

$$= \int_{0}^{\infty} n \left[ \bar{F}_{\gamma_1}(z) + \bar{F}_{\gamma_2}(z) - \bar{F}_{\gamma_1}(z) \bar{F}_{\gamma_2}(z) \right] \times z^{n-1} dz$$

(9)

The integral of the first two terms in (9) can be obtained from the integral table identity [23, eq.(6.655)]. Since the fading parameter is a positive number, one can expand $\bar{F}_{\gamma_1}(z)$ using the series identity [23, eq.(8.352.2)]. By substituting the three terms in (9), the moments of the SNR $\gamma$ are given by (10), where $\frac{d}{dz} F_{\gamma}(\alpha_1, \ldots, \alpha_p; \beta_1, \ldots, \beta_q; z)$ is called a generalized hypergeometric series [23, eq.(9.14)].

2) $m$ is a non negative number plus one half: Likewise, the higher-order moments are computed by integration by parts. The second and third terms of (9) involve the integral of the confluent hypergeometric function, which can be solved using [23, eq.(7.621.6)]. The moments of the SNR $\gamma$ are given by (11).

C. Ergodic Capacity

1) $m$ is a positive number: If the magnitude of the received signal in the relay link is greater, then the destination instructs the relay to participate in cooperation, otherwise it does not. Using the rule of integration by parts, the ergodic capacity is written as

$$E \left[ \frac{1}{2} \log_2 (1 + \gamma) \right] = \int_{0}^{\infty} \frac{1 - F_{\gamma}(z)}{2 \ln 2} dz$$

$$= \int_{0}^{\infty} \bar{F}_{\gamma_1}(z) + \bar{F}_{\gamma_2}(z) dz - \int_{0}^{\infty} \bar{F}_{\gamma_1}(z) \bar{F}_{\gamma_2}(z) dz$$

(12)

When the first term of (12) is tackled, one kind of integral appears as

$$J_1 = \int_{0}^{\infty} \frac{\Gamma(m_d, \beta_d x)}{1 + x} dx$$

(13)

Here, some constant coefficients are omitted. Next, we rewrite the Gamma and fractional functions in terms of Meijer’s $G$ function as follows

$$\Gamma(m_d, \beta_d x) = G_{1,2}^{2,0} \left[ \beta_d x \right]_{m_d, 0}^{1,0}$$

$$\frac{1}{1 + x} = G_{1,1}^{1,1} \left[ 0 \right]_{0, 0}^{0, 0}$$

(14)

(15)

where $G(\cdot)$ is the Meijer’s $G$ function [23, eq.(9.301)]. Using [23, eq.(7.811.1)], $J_1$ is expressed as a Meijer’s $G$ function. When the second term of (12) is tackled, one kind of integral appears as

$$J_2 = \int_{0}^{\infty} e^{-(\beta_d + \beta_d) x} dx \left[ (1 + m_r) K_{k-1-t_2} \left( 2 \sqrt{\beta_d} x \right) \right]$$

(16)

Likewise, the exponential function is rewritten as

$$e^{-(\beta_d + \beta_d) x} = H_{0,1}^{1,0} \left[ (\beta_d + \beta_d) x \right]_{0, 0}^{0, 1}$$

(17)

where $H(\cdot)$ is the Fox’s $H$ function [25, eqs.(2.9.4),(1.1.1)]. Using [26, eq.(2.6.4)] yields the result $J_2$ in (16). Adding the constant coefficients and combining $J_1$ and $J_2$, the ergodic capacity is given by (18), where $H(x, y)$ is the bivariate Fox’s function [26, eq.(2.2.1)].

2) $m$ is a non negative number plus one half: Similarly, based on the bivariate Meijer’s function, when $m$ is a non negative number plus one half, the ergodic capacity is given by (19).
\[
E(\gamma^n) = \frac{\Gamma(m_d + n)}{\Gamma(m_d) \beta_d^m} + \frac{8n\sqrt{\pi} \beta_r}{\Gamma(m_r)} \sum_{l_1=0}^{m_s-1} \sum_{k=0}^{m_r-1} \frac{C_{l_1}^{C_{m_r-1}} l_1^{l_1-4} l_2^{k-\beta_1 l_1+1-k+l_2}}{l_1! \Gamma\left(\frac{1}{2} + l_1 + n + m_r\right)}
\times \Gamma\left(k - l_2 + l_1 + n + m_r\right) \left(\sqrt{\beta_s} + \sqrt{\beta_r}\right)^{2(k - l_2 - l_1 - n - m_r)}
\times 2F_1 \left[\frac{3}{2} - k + l_2, 1 + l_2 - k + l_1 + n + m_r; \frac{1}{2} + l_1 + n + m_r; \left(\frac{\sqrt{\beta_s} - \sqrt{\beta_r}}{\sqrt{\beta_s} + \sqrt{\beta_r}}\right)^2\right]
\times \frac{\sqrt{\pi} n}{2\Gamma(m_r)} \sum_{l_1=0}^{m_s-1} \sum_{l_2=0}^{m_r-1} \sum_{l_3=0}^{m_d-1} \frac{C_{l_1}^{C_{l_2}^{C_{m_r-1}} l_1^{l_1-4} l_2^{l_2-1} l_3^{l_3-1} \sqrt{\beta_s} + \sqrt{\beta_r}}}{l_1! l_2! (\beta_s + \beta_r + \beta_d + 2\sqrt{\beta_s \beta_r})^{l_1 + m_r + n + l_3 + k - 1 - l_2}}
\times \Gamma\left(l_1 + m_r + n + l_3 + k - 1 + l_2\right)
\times 2F_1 \left[l_1 + m_r + n + l_3 + k - 1 - l_2, k - l_2 - \frac{1}{2}; l_1 + n + m_r + l_3 + \frac{1}{2}; \left(\frac{\sqrt{\beta_s} - \sqrt{\beta_r}}{\sqrt{\beta_s} + \sqrt{\beta_r}}\right)^2 + \beta_d\right]^{(10)}
\]

\[
E(\gamma^n) = \frac{\Gamma(m_d + n)}{\Gamma(m_d) \beta_d^m} + \frac{\sqrt{\pi}}{\Gamma(m_r) \Gamma(m_r) (n - 1)!} \sum_{k_1=0}^{m_s} \sum_{k_2=0}^{m_r} \left(\frac{m_s}{k_2 + k_2}\right) \beta_s^{k_2} \frac{\beta_r^{k_2}}{4} \left[\frac{(m_s + k_1)! (m_r + k_2)!}{\beta_s^{k_2} \beta_r^{k_2}} - \frac{(m_s + k_1)! (m_r + k_2)!}{\beta_s^{k_2} \beta_r^{k_2}}\right]
\times \left(\sqrt{\beta_s} + \sqrt{\beta_r}\right)^{1 - m_s + k_1 - m_r + k_2 - 2n}
\times \frac{\Gamma\left(m_s - k_1 + m_r - k_2\right)}{2} + n\right) \Gamma\left(m_s - k_1 + m_r - k_2 - 1\right) + n + m_d,

\]

\[
\frac{m_s + m_r - k_1 - k_2}{2} + n + m_d, 1 + m_d, 1 + m_d + n; \frac{-\beta_d}{\sqrt{\beta_s} + \sqrt{\beta_r}} \right]^{(11)}
\]

\[
E\left[\frac{1}{2} \log_2 (1 + \gamma)\right] = \frac{1}{2 \ln 2\Gamma(m_d)} G^{C_{3,2}, \beta_d} \left(\beta_d, 0, 1, l_{m_d, 0, 0}\right) + \frac{1}{\ln 2\Gamma(m_r)} \sum_{l_1=0}^{m_s-1} \sum_{k=0}^{m_r-1} \frac{C_{l_1}^{C_{m_r-1}} l_1^{l_1-4} l_2^{k-\beta_1 l_1+1-k+l_2}}{l_1! \beta_s^{l_1 + k_2 - \beta_1 l_2 - 1} \beta_r^{l_1 + k_2 - \beta_1 l_2 - 1}}
\times H^{2,0,1,1,1}_{2,0,1,1,0,1,1}\left[\beta_s + \beta_r, 0, 0, 0, 0, 0; \left(l_1 + m_r + k_2 + l_2 - 1\right), \left(l_1 + m_r + k_2 + l_2 + 1, 1\right)\right]
\times \left(0, 2\right) - \left(0, 2\right)
\times H^{2,0,1,1,1}_{2,0,1,1,0,1,1}\left[\beta_s + \beta_r, 0, 0, 0, 0, 0; \left(l_1 + m_r + k_2 + l_2 - 1\right), \left(l_1 + m_r + k_2 + l_2 + 1, 1\right)\right]
\times \left(0, 2\right) - \left(0, 2\right) \right]^{(18)}
\]
D. Average SEP

1) \( m \) is a positive number: The average SEP conditioned on the instantaneous SNR is given by

\[
P_e = E \left[ aQ \left( \sqrt{b\gamma} \right) - cQ^2 \left( \sqrt{b\gamma} \right) \right]
\]

(20)

where \( a, b \) and \( c \) are constants dependent on the modulation type and \( Q(\cdot) \) is the Gauss Q function. Applying the rule of integration by parts, \( P_e \) can be rewritten as

\[
P_e = \int_0^\infty \frac{a}{2\sqrt{\pi x}} e^{-\frac{bx^2}{2}} F_\gamma(x) \, dx
- \int_0^\infty \frac{c}{2\sqrt{\pi x}} e^{-\frac{bx^2}{2}} erfc \left( \frac{\sqrt{b\gamma}}{2} \right) F_\gamma(x) \, dx
\]

(21)

where \( erfc(\cdot) \) is the complementary error function. The first and second terms of (21) are denoted by \( P_{e1} \) and \( P_{e2} \), respectively. Let us check \( P_{e1} \) first. Using [23, eq.(6.455.1)], the average SEP \( P_{e1} \) is given by (22).

Analyzing \( P_{e2} \) is challenging due to the complex nature of the complementary error function. One type of integral \( J_3 \) appears as

\[
J_3 = \int_0^\infty \left( e^{-\frac{bx^2}{2}} \right) \, dx
\]

(24)

In (24), some constant coefficients are omitted. To simplify the calculation, we resort to Fox’s \( H \) function. Based on [25, eqs.(2.9.4),(2.9.21)], the complementary error function and the exponential function can be rewritten in terms of Fox’s \( H \) function as

\[
e^{-\left( \frac{b}{2} + \beta_s + \beta_r \right)x} = H^{0,1}_{1,0} \left[ \left( \frac{b}{2} + \beta_s + \beta_r \right) x \right] (0,1)
\]

(25)

Then using [26, eq.(2.6.4)], \( J_3 \) can be expressed in terms of the bivariate Fox’s function. The average SEP \( P_{e2} \) is given by (26). Finally, combining (22) and (26) yields the average SEP \( P_e = P_{e1} - P_{e2} \). This applies to the scenario where the effect of \( Q^2(x) \) is not be ignored, as in quadrature amplitude modulation (QAM). If the quadratic term is not taken into account, \( c = 0 \) will be substituted in (26).

In some special scenarios, AWGN perhaps is not an ideal choice. In [27], AWGGN was proposed for wireless sensor networks and underwater communications due to its versatility in providing a good match to various empirically obtained measurement data. The generalized Gauss distribution is more accurate in describing the noise probability distribution than the traditional Gauss distribution in these scenarios. Therefore, more universal is the analysis of SEP subject to AWGGN, which is given by

\[
P_e = E \left[ aQ_\alpha \left( \sqrt{b\gamma} \right) \right]
\]

(27)

where \( Q_\alpha(\cdot) \) is the generalized Q function defined as

\[
Q_\alpha(x) = \frac{\Gamma \left( 1/\alpha, |\Lambda_0 x|^\alpha \right)}{2\Gamma(1/\alpha)}
\]

(28)

where \( \Lambda_0 = \sqrt{\Gamma(3/\alpha)}/\Gamma(1/\alpha) \). It is easily seen that \( Q_\alpha(x) \) reduces to the traditional Q function when \( \alpha = 2 \). Some common noise types are summarized in [28] with different \( \alpha \) values. Applying integration by parts, the SEP subject to AWGGN is given by (29). As a double check, when \( \alpha = 2 \), (29) becomes (22) through some identities, which proves the correctness of the formula.

2) \( m \) is a non negative number plus one half: Due to mathematical tractability, we only tackle average SEP when \( c = 0 \) with non negative number \( m \). Likewise, using [26, eq.(2.6.2)], the average SEP is given by (30).

Likewise, to analyze the SEP subject to AWGGN, the exact closed form formula is given by (31). Similarly, the SEP expression helps us to accurately assess the joint impact of the noise distribution and channel fading.

Before closing this section, we point out that higher order moments of SNR, ergodic capacity and average SEP are all expressed in exact closed form. All these important performance metrics help us understand the AF relaying system.

IV. Simulation Results

The correctness of all formulas is checked by computer simulation in this section. According to the location of S, R and D with respect to each other and channel qualities, two typical scenarios are considered: all channel gains are
\[ P_{c1} = E\left[aQ \left(\sqrt{b}\right)\right] = \frac{a}{2} - \frac{av b}{2\sqrt{2\pi} \beta d \Gamma(m_d)} \left[ \frac{1}{2} \Gamma \left(\frac{1}{2}; m_d + 1\right) \right] - \frac{av b}{2\sqrt{2\pi} \beta d \Gamma(m_r)} \sum_{l_1=0}^{m_r-1} \sum_{l_2=0}^{m_r-1} \frac{C_{l_1}^k C_{l_2}^{m_r-1}}{l_1!} \] 

\[ \times (\beta_r - 1 + l_2) \Gamma (l_1 + m_r + l_2 - 1) \Gamma (l_1 + m_r + l_2 - 1) \] 

\[ + \frac{av b}{2\sqrt{2\pi} \beta d \Gamma(m_r)} \sum_{l_1=0}^{m_r-1} \sum_{l_2=0}^{m_r-1} \sum_{l_3=0}^{m_r-1} \frac{C_{l_1}^k C_{l_2}^{m_r-1} C_{l_3}^l}{l_1!} \left( \frac{l_1 + m_r + l_2 + l_3 + k - l_2 - \frac{3}{2}}{\Gamma(l_1 + m_r + l_3 + k + l_2 - \frac{3}{2})} \times 2F_1 \left[ l_1 + m_r + l_3 + k - l_2 - \frac{1}{2}, l_1 + m_r + l_3 + 1; \frac{\sqrt{b} - \sqrt{b} - \frac{b}{2}}{\sqrt{b} + \sqrt{b} + \frac{b}{2}} l_1 ! l_3 ! \right] \right) \] 

(22)

\[ P_{c2} = E\left[Q^2 \left(\sqrt{b}\right)\right] = \frac{c}{4} - \frac{c}{4 \sqrt{\pi}} \sum_{l=0}^{m_d-1} \frac{\beta d^2 \Gamma(2l_3 + 1)}{l_3!} \left( \frac{1}{2} l_3 + 1; l_3 + 3; 1 - 2b + b \right) \] 

\[ - \sqrt{b} \frac{c}{\sqrt{2\pi} \Gamma(m_r)} \sum_{l_1=0}^{m_r-1} \sum_{l_2=0}^{m_r-1} \sum_{l_3=0}^{m_r-1} \frac{C_{l_1}^k C_{l_2}^{m_r-1} C_{l_3}^l}{l_1!} \left( \frac{l_1 + m_r + l_2 + \frac{3}{2}}{\Gamma(l_1 + m_r + l_3 + \frac{3}{2})} \right) \] 

\[ + \sqrt{b} \frac{c}{\sqrt{2\pi} \Gamma(m_r)} \sum_{l_1=0}^{m_r-1} \sum_{l_2=0}^{m_r-1} \sum_{l_3=0}^{m_r-1} \left[ \frac{\beta d^2 \Gamma(2l_3 + 1)}{l_3!} \right] \] 

(26)

\[ P_c = E\left[aQ_\alpha \left(\sqrt{b}\right)\right] = \int_0^\infty \frac{aa \Lambda_0 \sqrt{b}}{4 \Gamma(1/\alpha) \sqrt{2}} e^{-\left(\sqrt{b} \Lambda_0 \alpha \right)^\alpha} F_\gamma (z) dz = \frac{a}{2} - \frac{av b \Lambda_0}{4 \Gamma(1/\alpha) \sqrt{2}} \Gamma(m_d) \] 

\[ \times \frac{\beta d^2 \Gamma(1/\alpha)}{\Gamma(1/\alpha) \Gamma(m_r)} \sum_{l_1=0}^{m_r-1} \sum_{l_2=0}^{m_r-1} \sum_{l_3=0}^{m_r-1} \frac{C_{l_1}^k C_{l_2}^{m_r-1} C_{l_3}^l}{l_1!} \left( \frac{l_1 + m_r + l_3 + k - l_2 - \frac{4}{2} + \frac{1}{2} l_1 + m_r + l_3 + 1; \beta_r \right) \] 

(29)
normalized to unity; the channel gains of the S→R and R→D links are normalized to unity while the channel gain of the S→D link is only one tenth, referred to as weak SD. This corresponds to a scenario where the destination node is far from the source node or the user is at the cell edge. The noise variances of all receivers are equal $\sigma^2 = \sigma^2_d = \sigma^2_a$. The source node and the relay use the same transmission power $P_s = P_r$. The average SNR per hop is defined as $P_s/\sigma^2$.

Figs.2 and 3 show that the first order moment of SNR is consistently growing. The simulated and computed curves agree very well, validating the accuracy of our analysis. As can be seen from both figures, there is always a gap between a strong SD channel and a weak SD channel. Other higher order moments can be similarly drawn using eqs.10 and 11. Using the first and second moment, the amount of fading can easily be evaluated by $E(\gamma^2)/E^2(\gamma) - 1$.

The variation of the ergodic capacity with average SNR per hop is shown in Figs.4 and 5, where theoretical results are consistent with simulated curves. The larger fading parameter offers performance improvement over the smaller ones. When $m_s = m_r = m_d = 0.5$, in high SNR region, the capacity is 4.1912 at 28dB and 4.5204 at 30dB. This implies that the multiplexing gain for a non negative integer $m$ is

$$\frac{10 \times \lg 2 \times (4.5204 - 4.1912)}{30 - 28} = 0.4955 \approx \frac{1}{2}$$

While for $m_s = m_r = 0.5, m_d = 1.5$, the capacity is 4.4736
The first order moment

ergodic capacity (bps/Hz)

\[ m_s = 1, m_r = 1, m_d = 2 \]
\[ m_s = 1, m_r = 1, m_d = 2, \text{weak SD} \]
\[ m_s = 1, m_r = 2, m_d = 1 \]
\[ m_s = 1, m_r = 2, m_d = 1, \text{weak SD} \]

\[ m_s = 0.5, m_r = 0.5, m_d = 0.5, \text{weak SD} \]
\[ m_s = 0.5, m_r = 0.5, m_d = 1.5, \text{weak SD} \]
\[ m_s = 1.5, m_r = 0.5, m_d = 0.5, \text{weak SD} \]
\[ m_s = 1.5, m_r = 1.5, m_d = 0.5, \text{weak SD} \]

While for negative integer \( m \) is [29]

\[
10 \log \left( \frac{0.0037466}{0.0023726} \right) \quad \text{at } 30\text{dB} \approx 0.9921 \approx \min (m_s, m_r) + m_d
\] (34)

A similar phenomenon is observed in Fig.7 when \( m \) is a positive integer. Therefore, a key conclusion is reached: the diversity gain for a selection combining relaying system in Nakagami fading channel is \( \min (m_s, m_r) + m_d \). The reason is that the error probability of the S→R and R→D links is limited to the smaller channel quality due to the inherent

\[ 10 \log \left( \frac{7.5603}{3.0259} \right) \quad \text{at } 30\text{dB} \approx 1.9884 \approx \min (m_s, m_r) + m_d
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\] (35)
property of relay technology, while the whole error probability of $S \rightarrow R \rightarrow D$ and $S \rightarrow D$ links is limited to the largest channel quality because of the decision characteristic of selection combining.

V. CONCLUSION

Due to low complexity of selection combining, we analyzed its performance in an AF relaying system over a Nakagami-$m$ channel. All derived exact formulas are expressed in closed form using special functions. In addition, the AWGN case is extended to AWGNN, whose practical importance is often overlooked. We analyzed the multiplexing gain and diversity gain which can approximately predict the asymptotic behavior in the high SNR regime. Simulation results for various fading parameters and channel qualities confirm the accuracy of the analysis.

REFERENCES


